

5,141,656

Aug. 25, 1992

United States Patent [19]

Rountree

[54] PROCESS FOR COATING MACHINE PARTS AND COATED MACHINE PARTS PRODUCED THEREBY

- [76] Inventor: Philip L. Rountree, 7364 Hayward Rd., Hudson, Ohio 44136
- [21] Appl. No.: 498,780
- [22] Filed: Mar. 26, 1990
- [51] Int. Cl.⁵ C10M 103/06
- [52] U.S. Cl. 252/25; 252/58;
- 427/290 [58] Field of Search 252/25, 58; 427/290

[56]

References Cited

U.S. PATENT DOCUMENTS

1,658,173	2/1928	Perks .
3.715,790	2/1973	Reinberger .
3,728.776	4/1973	DeFazio .
4.091,518	5/1978	Rutherford .
4.238,575	12/1980	Kleiner et al.

[45] **Date of Patent:**

Patent Number:

4,292,723 10/1981 Rauscher . 4,724.819 2/1988 Fleri .

[11]

OTHER PUBLICATIONS

Modern Plastics Encyclopedia, 1984-1985, pp. 14, 22-26, 30, 32, 36, 38 and 74-78. DOD-P-16232F. TRW Publication (undated).

Primary Examiner—Jacqueline Howard Attorney, Agent, or Firm—Rothwell, Figg, Ernst & Kurz

[57] ABSTRACT

A process for coating a machine part surface wherein the surface is cleaned, abraded and treated so as to render the surface directly bondable to a resin-bonded lubricant coating. A resin-bonded lubricant coating then is directly applied to the treated machine part surface and cured so as to cross-link the resin.

25 Claims, 1 Drawing Sheet



U.S. Patent



PROCESS FOR COATING MACHINE PARTS AND COATED MACHINE PARTS PRODUCED THEREBY

BACKGROUND OF THE INVENTION

1. Field of the Invention

The present invention relates to the field of reconditioning machine parts, particularly automotive parts.

2. Description of the Backcround Art

Most automobiles manufactured in the world today utilize rack and pinion steering systems. In recent years, hydraulic power assist has been added to rack and pinion steering systems which utilize a control valve assembly and a hydraulic cylinder thereof attached di-¹⁵ rectly to the rack. With hydraulic power assist, hydraulic pressure is applied to one side or the other of the rack piston proportional to the movement of the steering column so as to move the rack in the desired direction and thereby steer the vehicle.

In rack and pinion steering systems with hydraulic power assist, the rack piston is sealed against the hydraulic cylinder with a face seal. The rack shaft, which transmits the force of the piston to the tie rods, serves as a seal face at opposite ends of the hydraulic cylinder. ²⁵ All of these seals are subject to wear due to the nature of the finish of the rack shaft and the cylinder surfaces. When the seals begin to leak, protective boots extending between the tie rods and the ends of the cylinder, which protect the ends of the cylinder from contact with con- 30 taminants and debris, begin to fill with hydraulic fluid. Output from the hydraulic pump of the power assist system can thereby be reduced or interrupted and malfunctions may occur.

The natural progression of wear on rack and pinion 35 systems can be accelerated by the introduction of foreign matter in the hydraulic reservoir, or by puncture or failure of one or both of the protective boots, thereby exposing the ends of the hydraulic cylinder. Once this occurs, the progression of malfunction is accelerated 40 when the rack shaft and/or cylinder bore becomes pitted or scored, and leakage becomes a major problem. Similar problems can occur within the pinion housing, causing wear of bearing surfaces therein.

There are various known methods for reconditioning 45 or refurbishing worn machine parts. For example, U.S. Pat. No. 4,724,819 to Fleri discloses a cylinder liner reconditioning process wherein the internal wall of a cylinder liner is cleaned and grit-blasted. A bond coat then is applied to the cylinder wall, followed by steel 50 coating and then coating with Teflon. The thus coated liner then is placed in an oven so as to permanently bond the Teflon thereto.

Other methods for reconditioning machine parts are disclosed in U.S. Pat. Nos. 1,658,173, 3,715,790, 55 3,728,776, 4,091,518 and 4,292,723, as well as Soviet Patent Publication Nos. 564,136 and 98/00105.

Despite the numerous proposals for reconditioning machine parts known in the art, there remains a need for reconditioning processes for machine parts such as 60 those utilized in rack and pinion steering systems.

SUMMARY OF THE INVENTION

In accordance with the present invention, a process for coating a machine part surface includes the steps of 65 these areas is too rough, the seal leaks at the outset. cleaning the machine part surface and abrading the cleaned machine part surface so as to roughen the surface. The roughened surface then is treated so as to

render the surface directly bondable to a resinbonded lubricant coating. A resin-bonded lubricant coating then is directly applied to the thus treated machine part surface. The coating then is cured so as to cross link the 5 resin.

BRIEF DESCRIPTION OF THE DRAWING

The sole figure is a schematic illustration of a rack and pinion steering system with hydraulic power assist, ¹⁰ to which the present invention is applicable.

DESCRIPTION OF THE PREFERRED **EMBODIMENTS**

The present invention provides a process for coating a machine part surface which can be applied to new parts so as to render the new parts more resistant to damage, and which also can be utilized to recondition used machine parts. According to one embodiment, the inventive process is applied to working surfaces of a 20 rack and pinion steering system with hydraulic power assist. Such a system is schematically shown in the drawing, and includes a rack shaft 10 having a rack gear 12 which cooperatively interacts with a pinion gear 14 attached to a steering column 16.

The pinion is a worm gear that is mechanically linked to a steering wheel (not shown) by means of the steering column 16. As the steering wheel turns the pinion gear 14, the teeth of the pinion gear mesh with the rack gear 12 to provide steering direction for the vehicle. The steering direction initiated by the pinion and rack gears is transmitted to the front wheels (not shown) of the vehicle through inner socket assemblies 26 and 28 connected to respective tie rods 30 and 32, and finally to steering arms (not shown) connected to the front wheels. Protective boots 34 and 36 in the form of rubber or plastic bellows, surround the inner socket assemblies 26 and 28, respectively, so as to prevent contaminants from entering the internal mechanism and destroying the gear assembly.

For hydraulic power assist, the rack shaft 10 is surrounded by a hydraulic cylinder 18 which contains a hydraulic piston 20 attached directly to the rack shaft 10. Piston 20 includes an o-ring seal 22, forming a fluidtight interface with the cylinder wall 24.

Hydraulic cylinder 18 is a double-acting cylinder. As hydraulic pressure is applied to either side of piston 20 via respective lines 40 and 42, shaft 10 will move away from the pressurized chamber. Since shaft 10 is a mechanical link to the tie rods and steering, movement of shaft 10 directs the vehicle.

The hydraulic power assist system is controlled by a control valve assembly 38 which is actuated by the turning of steering column 16.

Pressure is applied in the hydraulic power assist system by means of a hydraulic pump 44 in communication with a hydraulic fluid reservoir 46.

Seal surface areas 48 and 50 of rack shaft 10 serve as the seal faces at respective ends 52 and 54 of cylinder 18. The rack shaft 10 typically is made of hardened steel having sufficient surface roughness to provide a lubricated seal in areas 48 and 50 of the rack shaft. If the finish in these areas is too smooth, lubricant starvation occurs and the seals wear prematurely. If the finish in

By the process of the present invention, the seal areas of the rack are protected against random and incipient failure during normal operation, and the mating seal surfaces are protected against wear, corrosion, pitting and abrasion when foreign matter is introduced into the system. In addition to protecting such mating surfaces, the invention may be used to repair working surfaces which suffer minor damage, and may be used in con- 5 junction with other known techniques to repair severely damaged elements. For example, a machine part such as a rack which has been severely damaged, can be metalized or plated by various well-known techniques to a size greater than its original size, and ground back 10 precisely to its original dimension prior to subjecting the part to the process of the present invention.

The present invention will be further described with reference to coating of the working surfaces of a steel rack shaft 10, which may either be a new rack shaft, or 15 ture for about 120 hours. a used rack shaft to be reconditioned.

The rack shaft 10 is initially cleaned by degreasing the rack in any suitable manner. For example, the rack can be degreased by immersion in a hot caustic soap solution, or utilizing a vapor degreaser with a degreas- 20 ing solvent.

When degreasing by immersion in a hot caustic soap solution, the solution can contain various additives, including surfactants, foaming agents, and the like.

Vapor degreasing can be accomplished in a vented 25 vessel containing a solvent chamber above which is located a vapor condensing chamber in fluid communication with the solvent chamber. The solvent chamber contains a degreasing solvent such as 1:1:1 chloroethane, in which heating elements are immersed. The rack 30 is positioned in the condensing chamber, which is surrounded by a cooled condensing jacket. The solvent is vaporized by the heating elements immersed therein, and condenses on the rack in the condensing chamber so as to bathe the rack in hot, chemically pure solvent. 35 The grease is carried away with the condensed solvent as it drips from the rack and returns to the solvent chamber.

After degreasing, any surfaces which are not to be treated according to the inventive process are suitably 40 masked. One such surface of rack 10 is the seal groove of piston 20, which can be masked by placing an o-ring in the seal groove.

The cleaned and masked rack 10 then is abraded so as to roughen the surface. The rack can be abraded by 45 grit-blasting with an abrasive media such as aluminum oxide, silica sand, silican carbide, metal shot, and the like. The grit grade may vary from about 20 grit to about 120 grit, depending on the desired surface, with 80 grit being typically used. The rack is gritblasted 50 using air pressure within the range of from about 40 psi to about 100 psi, depending on the hardness of the steel being treated, with increased air pressure being utilized with harder steels. Grit adhering to the rack is blown 55 off under pressurized air after blasting is completed.

The grit-roughened surface then is treated so as to render the surface directly bondable to a resin-based lubricant coating. When applying the inventive process to a steel rack shaft 10, the grit-roughened surface is treated with a phosphatizing agent, with surface areas 60 not to be treated, such as the o-ring groove of piston 20, being masked. Suitable phosphatizing agents include zinc phosphate and manganese phosphate. Zinc phosphate is preferable for use in applications where corrosion is a problem, whereas manganese phosphate pro- 65 vides better wear characteristics. The coating thickness may also vary depending on the degree of corrosion or abrasion resistance versus the surface roughness de-

sired. The thickness of the phosphate coating may vary from about 0.0002 inch to 0.0010 inch in thickness depending on whether a fine grain phosphate formulation is used or whether a heavy grain phosphate formulation is used. In preferred embodiments, a thickness of about 0.0003 inch is obtained by use of a microcrystaline phosphate formulation.

If the part being processed, such as rack 10, has been heat treated to a Rockwell hardness in excess of about 39, resulting hydrogen embrittlement must be relieved. This can be accomplished by baking the rack in an oven at about 350° F. for about 4 hours, or the hydrogen can be allowed to dissipate from the rack to reduce the brittleness thereof by normal attrition at room tempera-

After phosphatizing the part and any necessary hydrogen dissipation, a resin-bonded lubricant is applied to the working surfaces to a thickness of from about 0.0005 inch to about 0.004 inch, with a preferred thickness of about 0.001 inch. The resin-bonded lubricant can be water based or non-aqueous solvent based, and can be applied to the working surfaces by any known technique, such as conventional spray techniques well known in the art. Examples of organic based solvents are methyl ethyl ketone, low molecular weight alcohol, toulene, benzene and standard organic solvent, which is usually a composite solvent. A water based diluent is preferred.

The resin-bonded lubricant includes a resin capable of withstanding the working temperatures of the part and having good adhesive qualities, low friction, excellent strength, wear resistance, chemical resistance, ductility, stress crack resistance, flex strength, low absorption and good application properties. Suitable resins are included in the following group: phenolics, epoxies, polyimides, polyamide-imides, polyesters, acrylics, polyphenylene sulfides, polybutylenes, furans, polyolefins such as polyethylenes, polypropylenes etc., polymethylpentenes, and the like. Preferred resins are polyimide, polyamidimide, phenolics and expoxies.

s friction, abrasion and wear. Suitable lubricant components include fluoropolymers such as polytetrafluoroethylene (Teflon (R)), fluorinated ethylene-propylene copolymer, perfluoroalkoxy resin, ethylene-tetrafluoroethylene copolymer, polyvinylidene fluoride, polychlorotrifluoroethylene, ethylenechlorotrifluoroethylene copolymer and polyvinyl fluoride, as well as tungsten disulfide, molybdenum disulfide, and titanium disulfide. Most preferred is polytetrafluoroethylene. The ratio of solids in a typical dispersion varies from about 15% to about 40% by weight depending upon the properties desired, i.e., corrosion resistance vs. friction and wear. When coating rack shafts, the amount of solids in the dispersion is preferably about 25% by weight.

After application of the resin-bonded lubricant to the working surfaces of the machine part, the coating is cured so as to cross-link the resin. Typically, the coating is cured at a temperature within the range of from about 250° F. to about 700° F. for from about 5 minutes to about 2 hours according to a schedule which is determined by the type of resin used and the amount of catalyst present. A typical schedule is as follows:

Curing Time (min.)	Part Temperature °F.
15	700
20	600
25	450

-continued				
Curing Time (min.)	Part Temperature °F.			
30	350			
60	250			

For coating rack shafts, a curing time of about 30 minutes at about 350° F. is preferred.

For aluminum machine part surfaces, the process is modified in the preparation of the substrate. The alumi- 10 num surface is cleaned in a non-silicated neutral cleaning solution such as ALUMA-K by Kleen-Corps Inc., or vapor degreased as described above. The part then is dried and grit-blasted at pressures toward the lower end of the pressure range set forth above with silica sand or 15 aluminum oxide so as to roughen the surface. The roughened surface then is hardened by anodizing the surface or by chemical conversion such as chromate conversion. Alternatively, the roughened surface is hard coated to provide a suitable base for applying the 20 lubricant is applied to said surface by spraying. resin-bonded lubricant. The resin-bonded lubricant then is applied to the surface as described above and cured.

By coating machine part surfaces with resin-bonded lubricant in accordance with the present invention, discontinuities of the surface are filled and the coating 25 burnishes in a short period of time to a smooth, frictionless surface providing non-leaking seals. Furthermore, such seals wear at a rate considerably less than when utilizing conventional steel working surfaces. The coating process of the present invention protects seals against random and incipient failure during normal operation, and protects mating surfaces against wear, corrosion, pitting and abrasion when foreign matter is introduced into the system.

Since modifications, variations and changes in detail may be made to the described embodiments, it is in-³⁵ tended that all matter in the foregoing description and shown in the accompanying drawing be interpreted as illustrative and not in a limiting sense.

What is claimed is:

1. A process for coating a machine part surface com- 40prising cleaning the machine part surface, abrading the cleaned machine part surface so as to roughen the surface, treating the roughened surface so as to render the roughened surface directly bondable to a resin-bonded lubricant coating, then applying a resin-bonded lubri- 45 cleaned with a non-silicated neutral cleaning solution. cant coating directly to the roughened machine part surface, and curing the coating so as to cross-link the resin.

2. The process of claim 1 wherein the machine part surface is steel, and wherein the treating step comprises 50 treating the roughened surface with a phosphatizing agent so as to render the surface directly bondable to the resin-bonded lubricant coating.

3. The process of claim 2 wherein the phosphatizing agent is selected from the group consisting of zinc phos- 55 phate and manganese phosphate.

4. The process of claim 2 wherein, after treatment with said phosphatizing agent, hydrogen is dissipated from the machine part so as to reduce brittleness thereof prior to application of the resin-bonded lubricant.

5. The process of claim 1 wherein the machine part surface is aluminum, and wherein said roughened surface is hardened prior to application of the resin-bonded lubricant coating thereto.

6. The process of claim 5 wherein said roughened 65 surface is anodized or chemically converted to harden said roughened surface prior to application of the resinbonded lubricant coating thereto.

7. The process of claim 1 wherein said cleaning comprises degreasing said machine part surface.

8. The process of claim 7 wherein said surface is degreased by immersion in a degreasing solution.

9. The process of claim 8 wherein said degreasing solution is a hot caustic soap solution.

10. The process of claim 7 wherein said machine part surface is degreased in a vapor degreaser with a degreasing solvent.

11. The process of claim 1 wherein said cleaned machine part surface is abraded by grit-blasting.

12. The process of claim 11 wherein said grit-blasting is with an abrasive media having a grade within the range of from about 20 grit to about 120 grit using air pressure within the range of from about 40 psi to about 100 psi.

13. The process of claim 1 wherein after grit-blasting, abrasive media is blown off the surface prior to application of said resin-bonded lubricant.

14. The process of claim 1 wherein said resin-bonded

15. The process of claim 1 wherein said resin-bonded lubricant is applied to said surface in water or in a nonaqueous solvent.

16. The process of claim 1 wherein said resin-bonded lubricant is applied to said surface to a thickness of from about 0.0005 to about 0.004 inch.

17. The process of claim 16 wherein said resin-based lubricant is applied to said surface to a thickness of about 0.001 inch.

18. The process of claim 1 wherein said lubricant is selected from the group consisting of fluoropolymers, tungsten disulfide, molybdenum disulfide and titanium disulfide.

19. The process of claim 1 wherein said resin is selected from the group consisting of phenolics, epoxies, polyimides, polyamide-imides, polyesters, acrylics, polyphenylene sulfides, polybutylenes, furans, polyolefins and polymethylpentenes.

20. The process of claim 19 wherein said resin is selected from the group consisting of phenolics, polyamide-imides, polyimides and epoxies.

21. The process of claim 1 wherein said coating is cured at a temperature within the range of from about 250° F. to about 700° F.

22. The process of claim 5 wherein said surface is

23. A machine part having a working surface comprising an abraded, phosphatized machine part surface directly bonded to an outer surface layer formed of cured, resin-bonded lubricant.

24. A process for coating a working surface of a steel rack shaft for a rack and pinion steering system, comprising cleaning the working surface, abrading the cleaned surface so as to roughen the surface, phosphatizing the roughened surface so as to render the surface directly bondable to a resin-bonded lubricant coating, applying a resin-bonded lubricant coating directly to the phosphatized surface, and curing the coating so as to cross-link the resin.

25. A process for coating an aluminum working surface of a rack shaft for a rack and pinion steering system, comprising cleaning the aluminum rack shaft surface, abrading the cleaned rack shaft surface so as to roughen the rack shaft surface, hard-coating the roughened rack shaft surface so as to render the rack shaft surface directly bondable to a resin-bonded lubricant coating, applying a resin-bonded lubricant coating directly to the hard-coated rack shaft surface, and curing the coating so as to cross-link the resin.

* *

UNITED STATES PATENT AND TRADEMARK OFFICE **CERTIFICATE OF CORRECTION**

PATENT NO. : 5,141,656

: August 25, 1992 DATED

INVENTOR(S) : Philip L. Rountree

It is certified that error appears in the above-identified patent and that said Letters Patent is hereby corrected as shown below:

Column 2, line 1, delete "resinbonded" and insert --resinbonded--.

Column 3, line 50, delete "gritblasted", and insert --grit-blasted--.

Column 4, line 42, delete "s", and insert -- A lubricant is dispersed in the resin, which minimizes ---.

Signed and Sealed this

Twelfth Day of October, 1993

Attest:

Attesting Officer

ince Tehman

BRUCE LEHMAN Commissioner of Patents and Trademarks