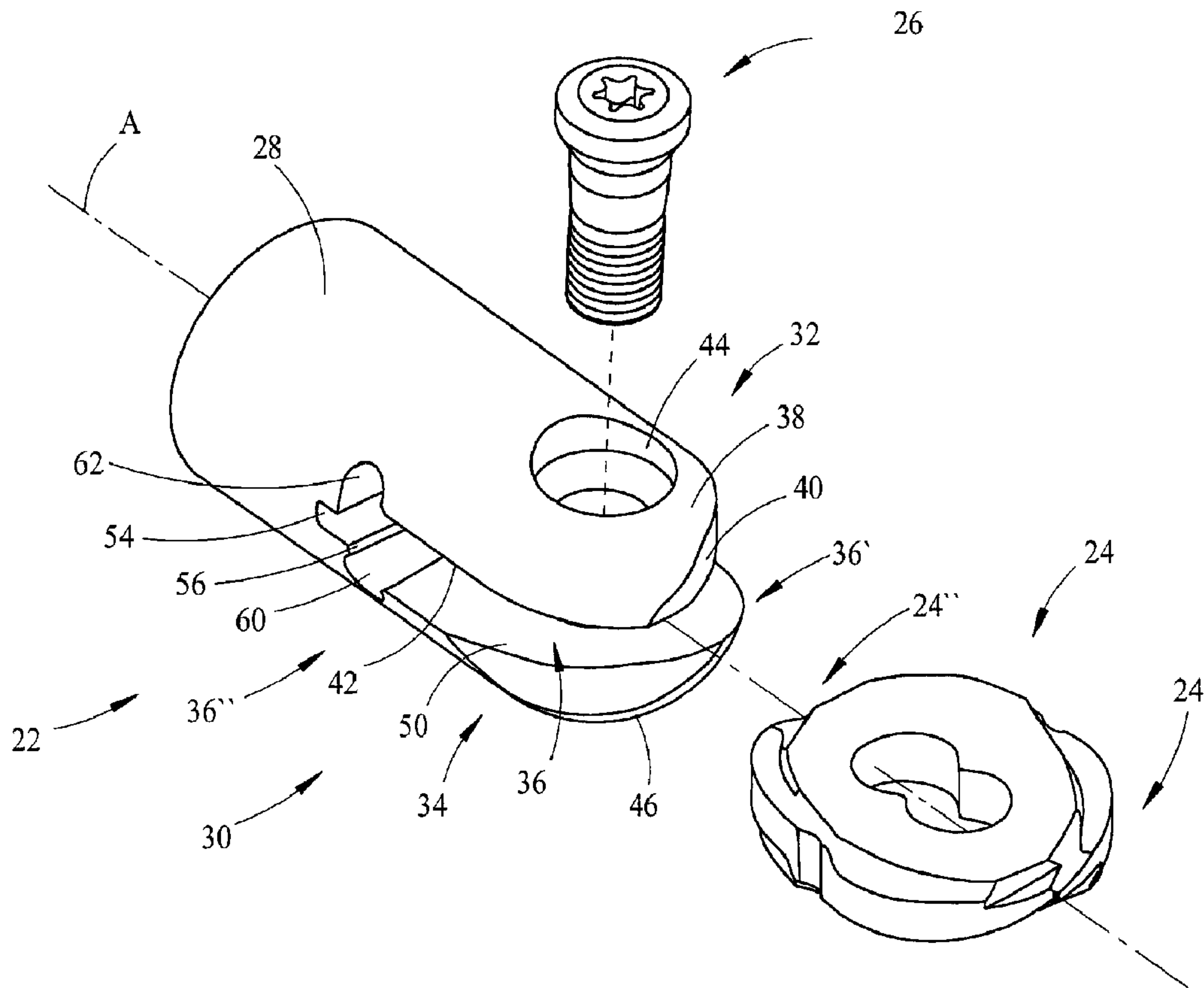




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(57) Abrégé/Abstract:

A cutting tool assembly (20), for example ball nose end mill, having a single replaceable cutting insert (24, 100, 106) clamped between two clamping jaws (34, 32) having clamping surfaces (50, 42) with geometries complementary to those of the clamping

(57) Abrégé(suite)/Abstract(continued):

surfaces (66, 64) of the cutting insert. In an end view of the cutting tool assembly, the clamping surfaces (50, 42) of the clamping jaws (34, 32) are at least partially convex and the insert clamping surfaces (66, 64) are concave. The cutting insert is secured in position by means of a clamping screw (26) that passes through through bores (44, 118) in the clamping jaws and in the cutting insert. When the cutting insert is clamped between the clamping jaws the side cutting edges of the cutting insert are provided with adequate support and are accurately radially located.

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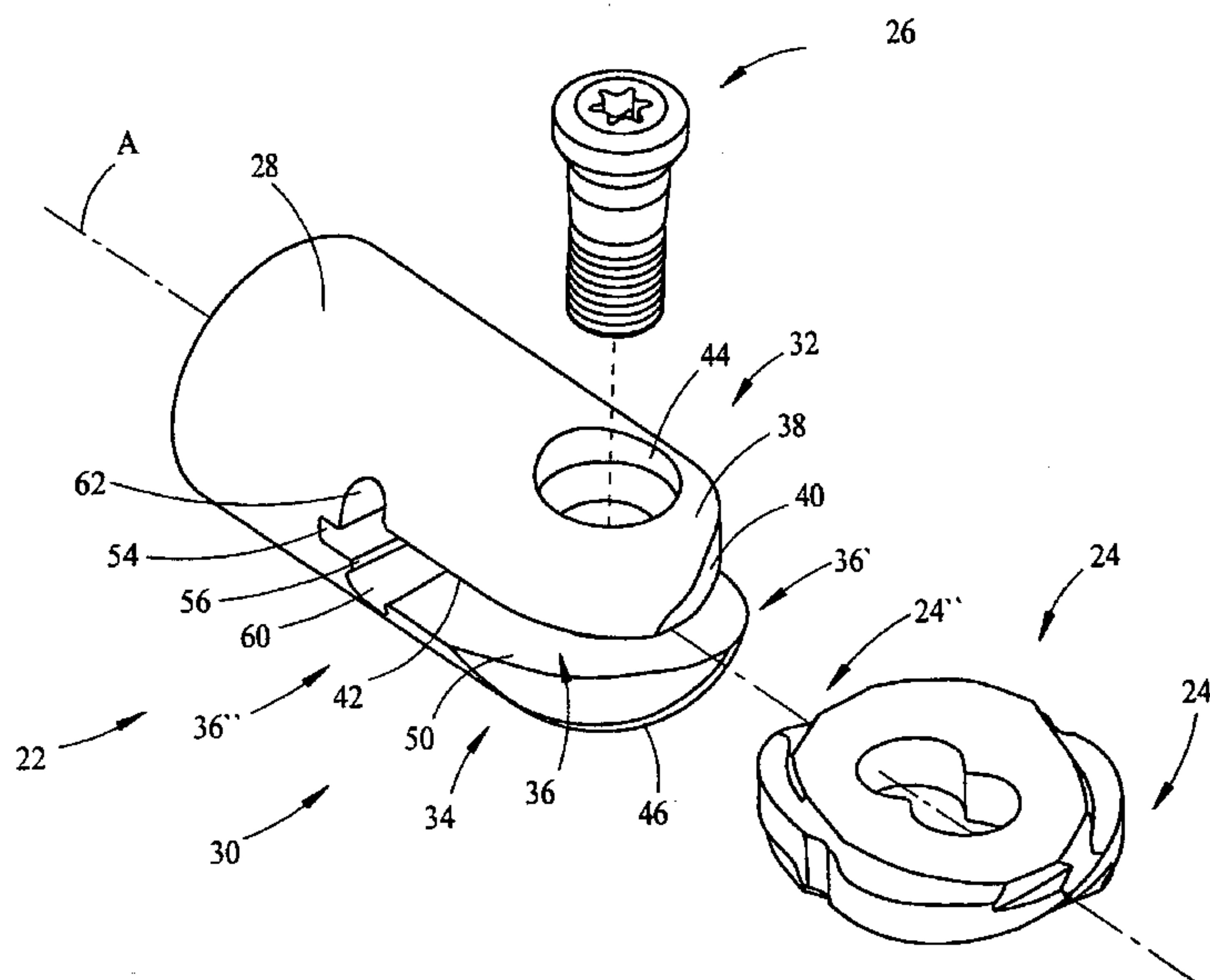
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(54) Title: MILLING CUTTER AND CUTTING INSERT THEREFOR



(57) Abstract: A cutting tool assembly (20), for example ball nose end mill, having a single replaceable cutting insert (24, 100, 106) clamped between two clamping jaws (34, 32) having clamping surfaces (50, 42) with geometries complementary to those of the clamping surfaces (66, 64) of the cutting insert. In an end view of the cutting tool assembly, the clamping surfaces (50, 42) of the clamping jaws (34, 32) are at least partially convex and the insert clamping surfaces (66, 64) are concave. The cutting insert is secured in position by means of a clamping screw (26) that passes through through bores (44, 118) in the clamping jaws and in the cutting insert. When the cutting insert is clamped between the clamping jaws the side cutting edges of the cutting insert are provided with adequate support and are accurately radially located.

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MILLING CUTTER AND CUTTING INSERT THEREFOR

FIELD OF THE INVENTION

This invention relates generally to milling cutters and more particularly to a ball nose end mill having a single replaceable cutting insert retained between clamping jaws, for use in high precision milling operations.

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BACKGROUND OF THE INVENTION

Milling cutters are commonly used for profile and cavity milling in the auto, aircraft, die and mold industries. In order to achieve high accuracy and good surface quality in the work products produced by the milling cutters to which the present invention relates, the cutting insert should be retained in the milling cutter with a high degree of locational precision.

A problem with prior art milling cutters utilizing replaceable cutting inserts is that the latter are either flat plate-like or generally prismatic in shape and are clamped between two clamping jaws having clamping surfaces with geometries complementary to those of the surfaces of the cutting insert being clamped, i.e., flat or prismatic, respectively. The cutting insert is secured in position by means of a clamping screw that passes through through bores in the clamping jaws and in the cutting insert. Due to manufacturing tolerances it is difficult to ensure that the cutting insert is on a true centerline when retained in the milling cutter. Such manufacturing

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tolerances include, for example, the diameter of the clamping screw, the diameter of the through bores and the location of the through bores. That is, for cutting tools such as end mills having a single replaceable cutting insert retained between clamping jaws the radial location of two diametrically opposite cutting edges of the cutting insert can be ascertained only to within the total manufacturing tolerances. This being the case, the points on the cutting edges of the cutting insert will not necessarily lie precisely on a flight circle concentric with the axis of rotation of the milling cutter. For milling cutters having flat plate-like cutting inserts, manufacturing tolerances of the clamping screw and the through bore in the milling cutter and in the cutting insert are the main contributing factors to the radial location imprecision of the cutting insert. The radial location precision can be improved by using inserts that have generally prismatic abutting surfaces clamped in clamping jaws having complementary shaped clamping surfaces. However, even in this case radial location imprecision of the cutting insert will exist. The main contribution to the radial location imprecision coming from geometrical factors such as the tolerance of manufacture of the angle between adjacent surfaces comprising the prismatic abutting surfaces.

In EP 0 417 862 B1 a cutting tool assembly is described which ensures effective clamping of a cutting insert in an insert holder so that the cutting insert is effectively retained against displacement under cutting forces, and so that the relative position of the cutting insert with respect to the cutting insert holder is maintained substantially invariant, both during cutting operations and also when inserts have to be replaced. In the embodiment shown in Fig. 3 of '862, effective retention of the cutting insert is obtained between ribs of the clamping jaws of the cutting insert holder and the cutting insert along discrete axially directed locations which are symmetrically disposed with respect to, and spaced from, a longitudinally directed median plane. In the embodiment shown in Fig. 4 of '862, instead of effective retention along discrete axially directed locations, the retention is along

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narrow axially directed intermediate curved portions.

In both the embodiments described in '862 the ribs of the clamping jaws are formed with a clamping surface of substantially circular cross-sectional shape and the clamping contact between the clamping surfaces of the clamping jaws and the cutting insert is designed to take place along predetermined axial locations by forming the clamping surfaces of the cutting insert with side curved portions having a larger radius of curvature than that of the clamping surface of the clamping jaw and a central curved portion have a smaller radius of curvature than that of the clamping surface of the clamping jaw.

It should be noted that in both embodiments described in EP '862 the clamping surfaces of the cutting insert are of a non-uniform cross section and that in both embodiments the side portions of the clamping surfaces of the cutting inserts do not abut the clamping surfaces of the clamping jaws. A disadvantage of such a clamping arrangement is that it cannot be applied to cutting tool assemblies such as end mills comprising a single replaceable cutting insert retained between a pair of clamping jaws. The cutting inserts of such cutting tool assemblies have a width, measured between the side cutting edges, which is much greater than their thickness, measured between the clamping surfaces of the cutting insert, and the clamping arrangement described in EP '862 would not provide adequate support for the side cutting edges of the cutting insert.

It is therefore an object of the present invention to overcome the aforementioned disadvantage and to provide a milling cutter that will ensure accurate radial location of replaceable cutting inserts when clamped in the milling cutter whilst providing adequate support for the side cutting edges of the cutting insert.

It is a further object of the present invention to provide an indexable cutting insert for such a milling cutter.

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SUMMARY OF THE INVENTION

In accordance with the present invention, there is provided a cutting tool assembly (20) comprising a cutting insert holder (22), a cutting insert (24) and a clamping screw (26), the cutting insert holder (22) comprising a clamping portion (30) connected to a body portion (28);

the clamping portion (30) comprising:

a lower clamping jaw (34) having a lower peripheral surface (46) and an upper clamping surface (50);

an upper clamping jaw (32) resiliently connected to the lower clamping jaw (34), the upper clamping jaw (32) having a lower clamping surface (42) and an upper peripheral surface (38);

a through bore (44) passing through the upper and lower clamping jaws, the through bore being threaded in one of the upper or lower clamping jaws;

an insert receiving slot (36) defined between the upper and lower clamping surfaces (50, 42);

the cutting insert (24) comprising:

an insert upper clamping surface (64) bounded by an upper edge (70);

an insert lower clamping surface (66) bounded by a lower edge (72);

a peripheral side surface (68) between the insert upper clamping surface (64) and the insert lower clamping surface (66);

at least one cutting edge associated with the peripheral side surface;

at least one through hole (118) passing through the cutting insert (24) between the insert upper and lower clamping surfaces;

wherein:

the insert upper clamping surface (64) conforms with a portion of a first cylindrical surface having a first radius of curvature, r_1 , and a first cylinder axis;

the insert lower clamping surface (66) conforms with a portion of a

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second cylindrical surface having a second radius of curvature, r_2 , and a second cylinder axis;

the upper clamping surface (50) of the lower clamping jaw (34) at least partially conforms with a portion of a third cylindrical surface having a third radius of curvature, R_2 , and a third cylinder axis;

the lower clamping surface (42) of the upper clamping jaw (32) at least partially conforms with a portion of a fourth cylindrical surface having a fourth radius of curvature, R_1 , and a fourth cylinder axis;

in a front view of the cutting tool assembly, the upper and lower clamping surfaces (50, 42) of the lower and upper clamping jaws (34, 32), respectively, are at least partially convex, and the insert lower and upper clamping surfaces (66, 64) are concave;

the cutting insert (24) is retained in the insert receiving slot (36) in a retained position by means of the clamping screw (26) which passes through the through bore (44) in the upper and lower clamping jaws of the cutting insert holder and through the at least one through hole (118) in the cutting insert (24) and is screwed into the threaded through bore in one of the upper or lower clamping jaws;

the lower clamping surface (42) of the upper clamping jaw (32) engages the insert upper clamping surface (64) at at least one upper region of contact (64') and the upper clamping surface (50) of the lower clamping jaw (34) engages the insert lower surface (66) at at least one lower region of contact (66');

characterized in that:

the at least one upper region of contact comprises at least two outer regions (64') of the insert upper clamping surface (64) and the at least one lower region of contact comprises at least two outer regions (66') of the insert lower clamping surface (66).

Preferably, the cutting insert holder (22) has an axis of rotation (A) and the cutting insert (24) has a longitudinal axis of rotational symmetry

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(B) and a center (128) through which the longitudinal axis of rotational symmetry (B) passes, the longitudinal axis of rotational symmetry (B) constituting an axis of rotation of the cutting insert about which the cutting insert has 180° rotational symmetry.

5 In accordance with a specific application, the first radius of curvature and the second radius of curvature are equal in magnitude, $r_1=r_2$, defining a radius of curvature, r , of the cutting insert clamping surfaces, and the third radius of curvature and the fourth radius of curvature are equal in magnitude, $R_1=R_2$, defining a radius of curvature, R , of the clamping jaws' clamping surfaces.

In accordance with the present invention, the radius of curvature, R , of the clamping jaws' clamping surfaces is greater than the radius of curvature, r , of the cutting insert clamping surfaces.

15 In accordance with one specific application, $r = 16$ mm and $R = 16.2$ mm.

In accordance with the present invention, the cutting insert has a width, W , which is greater than a thickness, T , where the width and thickness are measured in a front view of the cutting insert as, respectively, the distance between opposing portions of the peripheral side surface, and a maximum distance between the insert upper and lower clamping surfaces.

Generally, W/T lies in the range 2.5 to 4.0.

In accordance with a specific application, W/T is equal to 3.3.

25 Further in accordance with the present invention, the cutting insert has a width, W , which is greater than a thickness, t , where the width and thickness are measured in a front view of the cutting insert as, respectively, the distance between opposing portions of the peripheral side surface, and a minimum distance between the insert upper and lower clamping surfaces.

Generally, W/t lies in the range 4.0 to 6.0.

30 In accordance with a specific application, W/t is equal to 5.3.

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Yet further in accordance with a specific application the radius of curvature, r , of the cutting insert clamping surfaces is approximately equal to W , and the radius of curvature, R , of the clamping jaw's clamping surfaces is approximately equal to W .

5 Generally, the insert receiving slot (36) has a forward end (36') for receiving a cutting insert and a rear end (36'') at which the upper clamping jaw is resiliently connected to the lower clamping jaw.

Preferably, the rear end (36'') of the insert receiving slot (36) is provided with at least one insert axial location surface (56, 58) transverse to
10 the axis of rotation (A) of the cutting insert holder (22).

Still further preferably, the rear end (36'') of the insert receiving slot (36) is provided with at least one generally cylindrical groove (60, 62) transverse to the axis of rotation (A) of the cutting insert holder (22) and adjacent the at least one insert axial location surface (56, 58).

15 Still yet further preferably, the cutting insert (24) has two end portions (24', 24'') adjacent the axis of rotation (B) of the cutting insert (24), at least one of the two end portions (24', 24'') being provided with axial abutment surfaces (88a, 88b, 90a, 90b) transverse to the axis of rotation (B) of the cutting insert (24).

20 Preferably, the axial abutment surfaces (88a, 88b, 90a, 90b) are ground.

In accordance with a first specific application, the at least one through hole (118) in the cutting insert (100) is implemented as a circular bore (102) having a bore axis (104) located substantially at the center of the
25 cutting insert in a top view of the cutting insert, the bore axis being perpendicular to the axis of rotation (B) of the cutting insert.

In accordance with a second specific application, the at least one through hole (118) in the cutting insert (106) is implemented as two circular bores (108, 110), each circular bore having a bore axis (112, 114) and a bore
30 diameter ($D1$, $D2$), the bore diameter of each circular bore being substantially

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equal in magnitude ($D1=D2=D$), each bore axis being located at substantially the same distance ($X1=X2=X$) from the center (116) of the cutting insert (106) in a top view of the cutting insert, the bore axes being perpendicular to the axis of rotation (B) of the cutting insert (106) and the distance (2X) between the two bore axes (112, 114) being greater than the bore diameter (D).

In accordance with a third specific application of the present invention, the at least one through hole (118) is implemented by two intersecting circular bores (120, 122), each circular bore having a bore axis (124, 126) and a bore diameter ($D1, D2$), the bore diameter of each circular bore being substantially equal in magnitude ($D1=D2=D$), each bore axis being located at substantially the same distance from the center (128) of the cutting insert (24) in a top view of the cutting insert, each bore axis being perpendicular to the axis of rotation (B) of the cutting insert and the distance (Y) between the two bore axes being less than the bore diameter (D).

In accordance with the second specific application of the present invention, the cutting insert (106) is retained in the insert receiving slot (36) in a retained position by means of a clamping screw (26) which passes through the through bore in the upper and lower clamping jaws of the cutting insert holder and through the circular bore in the cutting insert closest the forward end (36') of the insert receiving slot (36) and is screwed into the threaded through bore (52) in one of the upper or lower clamping jaws.

In accordance with the third specific application of the present invention, the cutting insert (24) is retained in the insert receiving slot (36) in a retained position by means of a clamping screw (26) which passes through the through bore in the upper and lower clamping jaws of the cutting insert holder and through the circular bore (120) in the cutting insert (24) closest the forward end (36') of the insert receiving slot (36) and is screwed into the threaded through bore (52) in one of the upper or lower

clamping jaws.

In accordance with a specific application of the invention, the peripheral side surface (68) of the cutting insert (24, 100, 106) is provided with two diametrically opposite pairs of cutting edges (74a, 74b; 76a, 76b) so that when the cutting insert is retained in the insert receiving slot, one pair of cutting edges (74a, 74b) is located closer to the forward end (36') of the insert receiving slot (36) and constitutes a pair of operative cutting edges and the other pair of cutting edges (76a, 76b) is located closer to the rear end (36'') of the insert receiving slot and constitutes a pair of inoperative cutting edges.

Preferably, the peripheral side surface is provided with two diametrically opposite notches (78', 78'') which are located on a first transverse axis of rotational symmetry (T1) and which separate between the diametrically opposite sets of cutting edges (74a, 74b; 76a, 76b), the first transverse axis of rotational symmetry (T1) passing through the peripheral side surface (68) and perpendicular to the longitudinal axis of rotational symmetry (B), the cutting insert having 180° rotational symmetry about the first transverse axis of rotational symmetry (T1).

Typically, each pair of cutting edges (74a, 74b; 76a, 76b) comprises one cutting edge (74b; 76b) which extends from a region close to where the longitudinal axis of rotational symmetry (B) passes through the peripheral side surface (68) upwards towards a notch whilst the other cutting edge (74a; 76a) extends from the same region close to where the longitudinal axis of rotational symmetry passes through the peripheral side surface downwards towards the diametrically opposite notch.

Generally, each cutting edge is provided with a relief surface (80) and a rake surface (82).

There is further provided in accordance with the present invention, a cutting insert (24) having a longitudinal axis of rotation (B) and a center (128) through which the longitudinal axis (B) passes, the

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longitudinal axis (B) constituting an axis of rotation of the cutting insert, the cutting insert (24) comprising:

an insert upper clamping surface (64) bounded by an upper edge (70);

an insert lower clamping surface (66) bounded by a lower edge (72);

5 a peripheral side surface (68) between the insert upper clamping surface (64) and the insert lower clamping surface (60);

at least one cutting edge associated with the peripheral side surface;

at least one through hole (118) passing through the cutting insert (24) between the insert upper and lower clamping surfaces;

10 wherein:

the insert upper clamping surface (64) conforms with a portion of a first cylindrical surface having a first radius of curvature, r_1 , and a first cylinder axis;

15 the insert lower clamping surface (66) conforms with a portion of a second cylindrical surface having a second radius of curvature, r_2 , and a second cylinder axis.

In accordance with a specific application, the first radius of curvature and the second radius of curvature are equal in magnitude, $r_1=r_2$, defining a radius of curvature, r , of the cutting insert clamping surfaces.

20 Further in accordance with a specific application, longitudinal axis (B) constitutes an axis of rotational symmetry of the cutting insert about which the cutting insert has 180° rotational symmetry.

In accordance with the present invention, the cutting insert has a width, W , which is greater than a thickness, T , where the width and
25 thickness are measured in a front view of the cutting insert as, respectively, the distance between opposing portions of the peripheral side surface, and a maximum distance between the insert upper and lower clamping surfaces.

Generally, W/T lies in the range 2.5 to 4.0.

In accordance with a specific application W/T is equal to 3.3.

30 Further in accordance with the present invention, the cutting

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insert has a width, W , which is greater than a thickness, t , where the width and thickness are measured in an end view of the cutting insert as, respectively, the distance between opposing portions of the peripheral side surface, and a minimum distance between the insert upper and lower
5 clamping surfaces.

Generally, W/t lies in the range 4.0 to 6.0.

In accordance with a specific application, W/t is equal to 5.3.

Still yet further preferably, the cutting insert (24) has two end portions (24', 24'') adjacent the axis of rotation (B) of the cutting insert (24),
10 at least one of the two end portions (24', 24'') being provided with axial abutment surfaces (88a, 88b, 90a, 90b) transverse to the axis of rotation (B) of the cutting insert (24).

Preferably, the axial abutment surfaces (88a, 88b, 90a, 90b) are ground.

15 In accordance with a first specific application, the at least one through hole (118) in the cutting insert (100) is implemented as a circular bore (102) having a bore axis (104) located substantially at the center of the cutting insert in a top view of the cutting insert, the bore axis being perpendicular to the axis of rotation (B) of the cutting insert.

20 In accordance with a second specific application, the at least one through hole (118) in the cutting insert (106) is implemented as two circular bores (108, 110), each circular bore having a bore axis (112, 114) and a bore diameter (D_1 , D_2), the bore diameter of each circular bore being substantially equal in magnitude ($D_1=D_2=D$), each bore axis being located at substantially
25 the same distance ($X_1=X_2=X$) from the center (116) of the cutting insert (106) in a top view of the cutting insert, the bore axes being perpendicular to the axis of rotation (B) of the cutting insert (106) and the distance ($2X$) between the two bore axes (112, 114) being greater than the bore diameter (D).

30 In accordance with a third specific application of the present

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invention, the at least one through hole (118) is implemented by two intersecting circular bores (120, 122), each circular bore having a bore axis (124, 126) and a bore diameter (D1, D2), the bore diameter of each circular bore being substantially equal in magnitude ($D1=D2=D$), each bore axis
5 being located at substantially the same distance from the center (128) of the cutting insert (24) in a top view of the cutting insert, the bore axes being perpendicular to the axis of rotation (B) of the cutting insert and the distance (Y) between the two bore axes being less than the bore diameter (D).

There is yet further provided in accordance with the present
10 invention, a cutting insert holder (22) having an axis of rotation A and comprising a clamping portion (30) connected to a body portion (28); the clamping portion (30) comprising:

a lower clamping jaw (34) having a lower peripheral surface (46) and an upper clamping surface (50);

15 an upper clamping jaw (32) resiliently connected to the lower clamping jaw (34), the upper clamping jaw (32) having a lower clamping surface (42) and an upper peripheral surface (38);

a through bore (44) passing through the upper and lower clamping jaws, the through bore being threaded in one of the upper or lower clamping
20 jaws; and

an insert receiving slot (36) defined between the upper and lower clamping surfaces (50, 42);

wherein:

the upper clamping surface (50) of the lower clamping jaw (34) at
25 least partially conforms with a portion of a third cylindrical surface having a third radius of curvature, R2, and a third cylinder axis;

the lower clamping surface (42) of the upper clamping jaw (32) at least partially conforms with a portion of a fourth cylindrical surface having a fourth radius of curvature, R1, and a fourth cylinder axis; and

30 in a front view of the cutting tool assembly, the upper and lower

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clamping surfaces (50, 42) of the lower and upper clamping jaws (34, 32), respectively, are at least partially convex.

In accordance with a specific application, the third radius of curvature and the fourth radius of curvature are equal in magnitude, $R_1=R_2$,
5 defining a radius of curvature, R , of the clamping jaws' clamping surfaces.

Generally, the insert receiving slot (36) has a forward end (36') for receiving a cutting insert and a rear end (36'') at which the upper clamping jaw is resiliently connected to the lower clamping jaw.

Preferably, the rear end (36'') of the insert receiving slot (36) is
10 provided with at least one insert axial location surface (56, 58) transverse to the axis of rotation (A) of the cutting insert holder (22).

Still further preferably, the rear end (36'') of the insert receiving slot (36) is provided with at least one generally cylindrical groove (60, 62) transverse to the axis of rotation (A) of the cutting insert holder (22) and
15 adjacent the at least one insert axial location surface (56, 58).

In accordance with one embodiment, the lower clamping surface (42) of the upper clamping jaw (32) is divided into three regions, two substantially identical outer regions (42') having a first radius of curvature and a central region (42'') having a second radius of curvature and the
20 upper clamping surface (50) of the lower clamping jaw (34) is divided into three regions, two substantially identical outer regions (50') having a first radius of curvature and a central region (50'') having a second radius of curvature.

Preferably, the second radius of curvature is larger than the first
25 radius of curvature.

There is still yet further provided in accordance with the present invention, a clamping screw (26) having a screw axis C and comprising:

- an upper portion (140);
- a central portion (142); and
- 30 a lower portion (144);

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the upper portion (140) comprises an upper cylindrical portion (146) and an upper frusto-conical portion (148), the upper frusto-conical portion (148) tapers downwardly and inwardly from the upper cylindrical portion (146) towards the central portion (142), the clamping screw upper portion (140) is provided with a socket (149), for receiving a wrench for tightening or loosening the clamping screw (26), the clamping screw central portion (142) has a central cylindrical portion (150) connected at its upper end to the upper frusto-conical portion (148) and at its lower end to a central frusto-conical portion (152), the central frusto-conical portion (152) tapers downwardly and inwardly from the upper end thereof, to the lower end thereof, at the lower end thereof the central frusto-conical portion (152) is connected, via a narrow neck portion (154), to the clamping screw lower portion (144), the clamping screw lower portion (144) comprises a threaded portion (156) of the clamping screw (26), the central frusto-conical portion (152) tapers at an angle θ to the screw axis C.

BRIEF DESCRIPTION OF THE DRAWINGS

For a better understanding the invention will now be described, by way of example only, with reference to the accompanying drawings in which:

Fig. 1 is a perspective view of a cutting tool assembly according to the present invention;

Fig. 2 is an exploded view of the cutting tool assembly of Fig. 1;

Fig. 3a is a bottom perspective view of the cutting insert holder shown in Fig. 2 with the lower clamping jaw removed for the purpose of clarification;

Fig. 3b is a top perspective view of the cutting insert holder shown in Fig. 2 with the upper clamping jaw removed for the purpose of clarification;

Fig. 4a is similar to Fig. 3a but for a cutting insert holder with the lower clamping surface of the upper clamping jaw divided into three regions;

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Fig. 4b is similar to Fig. 3b but for a cutting insert holder with the upper clamping surface of the lower clamping jaw divided into three regions;

Fig. 5a is a front view of the cutting insert holder according to the present invention;

Fig. 5b is similar to Fig 5a but for a cutting insert holder with the clamping surfaces of the clamping jaws divided into three regions;

Fig. 6 is a front view of the cutting insert according to the present invention;

Fig. 7 is an enlarged view of the cutting insert shown in Fig. 2;

Fig. 8 is a top view of the cutting insert shown in Fig. 7;

Fig. 9 is a top view of a cutting insert in accordance with the present invention with one circular through bore;

Fig. 10 is a top view of a cutting insert in accordance with the present invention with two non-overlapping circular through bores;

Fig. 11 is a side view of a clamping screw used for clamping a cutting insert in a cutting insert holder in accordance with the present invention;

Fig. 12 is a side cross sectional view, in a longitudinal median plane, of the cutting tool assembly of Fig. 1 showing the clamping screw in an initial position before engaging the upper clamping jaw of the cutting insert holder;

Fig. 13 is a side cross sectional view, in a longitudinal median plane, of the cutting tool assembly of Fig. 1 showing the clamping screw in an initial position engaging the upper clamping jaw of the cutting insert holder but prior to applying force to the clamping jaws;

Fig. 14 is a front view of the cutting tool assembly showing the location of the insert clamping surfaces relative to the clamping surfaces of the clamping jaws for both Figs. 12 and 13;

Fig. 15 is a side cross sectional view, in a longitudinal median plane, of the cutting tool assembly of Fig. 1 showing the clamping jaws engaging

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the insert clamping surfaces but prior to the final tightening of the clamping screw;

Fig. 16 is a side cross sectional view, in a longitudinal median plane, of the cutting tool assembly of Fig. 1 showing the axial abutment surfaces at the rear of the cutting insert engaging the insert axial location surfaces at the rear of the insert receiving slot, after the final tightening of the clamping screw;

Fig. 17 is a front view of the cutting tool assembly in accordance with Fig. 16; and

Fig. 18 is a front view of the cutting tool assembly having a cutting insert holder with the clamping surfaces of the clamping jaws divided into three regions, showing the situation after the final tightening of the clamping screw.

15 DETAILED DESCRIPTION OF THE INVENTION

Attention is first drawn to Figs. 1, 2, 3a, 3b and 5a. As shown, a cutting tool assembly **20** comprises a cutting insert holder **22** having an axis of rotation **A**, a cutting insert **24** and a clamping screw **26** for securing the cutting insert in the cutting insert holder. The cutting insert holder **22** comprises an elongated cylindrical body portion **28** and a clamping portion **30** in a front portion thereof. The clamping portion **30** consists of an upper clamping jaw **32** separated from a lower clamping jaw **34** by an insert receiving slot **36**. The upper clamping jaw **32** has an upper peripheral surface **38** having a chip evacuation recess **40** in a front portion thereof, a lower clamping surface **42** and a through bore **44** transverse to the axis of rotation **A**. The lower clamping jaw **34** has a lower peripheral surface **46** having a chip evacuation recess **48** in a front portion thereof, an upper clamping surface **50** and a threaded bore **52** transverse to the axis of rotation **A** and aligned with the through bore **44** in the upper clamping jaw. The terms “upper”, “lower”, “forward” and “rear” are used herein with reference

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to the orientation of the cutting insert holder **22** and the cutting insert **24** as shown in Figs. 1 and 2. Hence, the cutting insert **24** has a forward end **24'** and a rear end **24''**. Similarly, the insert receiving slot **36** has a forward end **36'** and a rear end **36''**.

5 The upper clamping jaw is resiliently connected to the lower clamping jaw at the rear end of the insert receiving slot via a slot **54** transverse to the axis of rotation **A**. Adjacent the slot **54** are two insert axial location surfaces transverse to the axis of rotation **A**, a lower insert axial location surface **56** and an upper insert axial location surface **58**. A lower
10 generally cylindrical groove **60**, transverse to the axis of rotation **A**, is located between the lower insert axial location surface **56** and the upper clamping surface **50** of the lower clamping jaw **34**. An upper generally cylindrical groove **62**, transverse to the axis of rotation **A**, is located between the upper insert axial location surface **58** and the lower clamping surface **42** of the
15 upper clamping jaw **32**.

In accordance with a first embodiment of the cutting insert holder **22**, the lower clamping surface **42** of the upper clamping jaw **32** conforms with a portion of a cylindrical surface having a radius of curvature **R1** and a cylinder axis generally parallel to the axis of rotation **A**, so that in
20 an end view of the cutting insert holder **22** the lower clamping surface of the upper clamping jaw is convex (see Figs. 3a and 5a). The upper clamping surface **50** of the lower clamping jaw **34** conforms with a portion of a cylindrical surface having a radius of curvature **R2** and a cylinder axis generally parallel to the axis of rotation **A**, so that in an end view of the
25 cutting insert holder **22** the upper clamping surface of the lower clamping jaw is convex (see Figs. 3b and 5a). Generally, the radii of curvature **R1**, **R2** of the lower and upper clamping surfaces **42**, **50** do not have to be identical.

Figs. 4a, 4b and 5b show a second embodiment of the cutting

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insert holder **22**. In accordance with this embodiment, which is a preferred embodiment of the present invention, the lower clamping surface **42** of the upper clamping jaw **32** is divided into three regions, two substantially identical outer regions **42'** on either side of a central region **42''**. The term
5 “substantially identical” in this context is used to indicate that the two outer regions **42'** are identical to within manufacturing tolerances. Each of the two outer regions conforms with a portion of a common cylindrical surface having a radius of curvature **R1** and a cylinder axis generally parallel to the axis of rotation **A**, whereas the central region **42''** is either planar, or
10 conforms with a portion of a cylindrical surface having a radius of curvature **R1'** larger than the radius of curvature **R1** of the outer regions **42'**. Therefore, in accordance with this embodiment, the lower clamping surface **42** of the upper clamping jaw **32** at least partially conforms with a portion of a cylindrical surface. Similarly, the upper clamping surface **50** of the lower
15 clamping jaw **34** can be formed to at least partially conform with a portion of a cylindrical surface by dividing it into three regions, two substantially identical outer regions **50'** on either side of a central region **50''**. Each of the two outer regions **50'** conforms with a portion of a common cylindrical surface having a radius of curvature **R2** and a cylinder axis generally
20 parallel to the axis of rotation **A**, whereas the central region **50''** is either planar, or conforms with a portion of a cylindrical surface having a radius of curvature **R2'** larger than the radius of curvature **R2** of the outer regions **50'**.

Attention is now drawn to Figs. 6 to 8. The cutting insert **24**
25 comprises an insert upper clamping surface **64**, an insert lower clamping surface **66** and a peripheral side surface **68** between the insert upper clamping surface and the insert lower clamping surface. The insert upper clamping surface **64** intersects the peripheral side surface **68** at an upper edge **70** and the insert lower clamping surface **66** intersects the peripheral

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side surface **68** at a lower edge **72**. The upper edge **70** constitutes a peripheral boundary of the insert upper clamping surface **64**, similarly the lower edge **72** constitutes a peripheral boundary of the insert lower clamping surface **66**. The cutting insert **24** has a longitudinal axis of rotation **B**. In accordance with a preferred embodiment, the axis of rotation **B**, constitutes an axis of rotational symmetry of the cutting insert, about which the cutting insert has 180° rotational symmetry and the lower edge **72** is equivalent in form to the upper edge **70**, due to the 180° rotational symmetry of the cutting insert about the axis of rotational symmetry **B**.

The cutting insert **24** is indexable and therefore the peripheral side surface **68** of the cutting insert is provided with two diametrically opposite pairs of cutting edges, a front pair of cutting edges **74a**, **74b** and a rear pair of cutting edges **76a**, **76b**. When the cutting insert **24** is retained in the insert receiving slot **36**, the front pair of cutting edges **74a**, **74b** is located closer to the front end of the insert receiving pocket and constitute a pair of operative cutting edges and the rear pair of cutting edges **76a**, **76b** is located closer to the rear end of the insert receiving pocket and constitute a pair of inoperative cutting edges.

The cutting insert has a first transverse axis **T1** passing through the peripheral side surface **68** and perpendicular to the longitudinal axis of rotation **B**. The cutting insert has a second transverse axis **T2** perpendicular to the longitudinal axis of rotation **B** and to the first transverse axis **T1**, the cutting insert having 180° rotational symmetry about the second transverse axis of rotational symmetry **T2**.

The peripheral side surface is provided with two diametrically opposite notches **78'**, **78''** which are located on the first transverse axis **T1** and which separate between the diametrically opposite pairs of cutting edges, that is, between the front pair **74a**, **74b** and the rear pair of cutting edges **76a**, **76b**.

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For the front pair of cutting edges, cutting edge **74a** extends from a region close to where the longitudinal axis of rotational symmetry **B** passes through the peripheral side surface **68** downwards and rearwards towards the notch **78'** whilst the other cutting edge **74b** extends from the same region close to where the longitudinal axis of rotational symmetry **B** passes through the peripheral side surface **68** upwards and rearwards towards the diametrically opposite notch **78''**. Due to the symmetrical nature of the cutting insert, the rear pair of cutting edges are identical to the front pair of cutting edges. Each cutting edge is provided with a relief surface **80** and a rake surface **82**.

The insert upper clamping surface **64** conforms with a portion of a cylindrical surface having a radius of curvature **r1** and a cylinder axis generally parallel to the longitudinal axis of rotational symmetry **B**. Similarly, the insert lower clamping surface **66** conforms with a portion of a cylindrical surface having a radius of curvature **r2** and a cylinder axis generally parallel to the longitudinal axis of rotational symmetry **B**. Hence, in an end view of the cutting insert **24** the insert's upper and lower clamping surfaces are concave (see Fig. 6). Generally, the radii of curvature **r1**, **r2** of the insert upper and lower clamping surfaces do not have to be identical.

In accordance with a preferred embodiment of the present invention, the radii of curvature **r1**, **r2** of the insert upper and lower clamping surfaces are substantially equal in magnitude, $r1=r2=r$, defining a single value **r** for the radius of curvature for each of the cutting insert clamping surfaces. The cylinder axis of the lower clamping surface is parallel to the cylinder axis of the upper clamping surface and both the cylinder axes lie in a vertical longitudinal median plane of the cutting insert which includes the axes **T2** and **B**. In accordance with this preferred embodiment, the longitudinal axis of rotation **B** and the first transverse axis **T1** are axes of rotational symmetry. The cutting insert **24** having 180°

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rotational symmetry about each of these axes. In this embodiment the lower clamping surface **66** is identical in form to the upper clamping surface **64** and the lower edge **72** is identical in form to the upper edge **70**.

In Fig. 6, three dimensions, **W**, **T** and **t** defining the basic linear dimensions of the cutting insert in an end view are shown. The width, **W**, of the cutting insert is defined as the distance between opposing portions of the peripheral side surface. The maximum thickness, **T**, of the cutting insert is defined as the maximum distance between the insert upper and lower clamping surfaces as measured in an end view. The minimum thickness, **t**, of the cutting insert is defined as the minimum distance between the insert upper and lower clamping surfaces as measured in an end view.

Generally, W/T lies in the range 2.5 to 4.0 and W/t lies in the range 4.0 to 6.0. In accordance with a specific application, W/T is equal to 3.3 and W/t is equal to 5.3.

In accordance with a preferred embodiment of the present invention, the radii of curvature **R1**, **R2** of the lower and upper clamping surfaces of the clamping jaws are substantially equal in magnitude, $R1=R2=R$, defining a single value for the radius of curvature **R** for each of the clamping surfaces of the clamping jaws. The cylinder axes of the lower and upper clamping surfaces of the clamping jaws are parallel and lie in the vertical median plane of the cutting insert, when the cutting insert is retained in the cutting insert holder.

In accordance with the present invention the radius of curvature of the clamping jaw's clamping surfaces **R** is greater than the radius of curvature **r** of the cutting insert clamping surfaces. That is, for the general case, the value of **R1** is greater than the value of **r1** and the value of **R2** is greater than the value of **r2**. In accordance with a preferred embodiment $R1=R2=R$ and $r1=r2=r$ and the value of **R** is greater than the value of **r**. Symbolically, this can be expressed as $R=r+\delta$, where δ , is a positive number.

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In accordance with one specific application, $r = 16$ mm and $R = 16.2$ mm.

The cutting insert **24** is provided with two axial abutment surfaces **88a**, **88b** at its front end **24'** and two axial abutment surfaces **90a**, **90b** at its rear end **24''**. The axial abutment surfaces are transverse to the axis of rotation **B** of the cutting insert. When the cutting insert **24** is retained in the insert retaining slot **36**, as shown in Fig.1, the upper rear abutment surface **90b** abuts the upper insert axial location surface **58**, and the lower rear abutment surface **90a** (not seen in the figures) abuts the lower insert axial location surface **56**, thereby fixing the axial location of the cutting insert in the cutting insert holder. The axial abutment surfaces **88a**, **88b**; **90a**, **90b** are preferably ground in order to increase the accuracy of the axial location of the cutting insert in the cutting insert holder.

Attention is now drawn to Figs. 7 to 10. In order to securely clamp the cutting insert in the cutting insert holder the cutting insert is provided with at least one through hole passing through the cutting insert between the insert upper and lower clamping surfaces. In general, a cutting insert for clamping in the insert holder shown in Fig. 1 will have either one or two through holes, depending on the length of the cutting insert. The reason for this being that the through bore **44** in the upper clamping jaw **32** and the associated threaded bore **52** in the lower clamping jaw **34** are preferably located as close as possible to the front end of the cutting insert holder in order to ensure that the front end portions of the clamping jaws close tightly on the retained cutting insert.

Figs. 8 to 10 show cutting inserts of different lengths. The length of a cutting insert in accordance with the present invention is measured along the axis of rotation **B** from one end of the cutting insert to the other. For example, in Fig. 8, the length of the cutting insert **24** is measured along the axis **B** from its front end **24'** to its rear end **24''**.

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Typically, in accordance with the present invention, insert lengths can vary from very short, having a length of approximately $0.5W$ to very long, having a length of approximately $2W$. The cutting insert **100** shown in Fig. 9 is relatively short, and is provided with a single through hole, namely a circular bore **102** having a bore axis **104** located substantially at the center of the cutting insert in a top view of the cutting insert. The bore axis **104** is perpendicular to the axis of rotation **B** of the cutting insert and lies in a vertical longitudinal median plane of the cutting insert. The cutting insert **100** is provided with two axial abutment surfaces **88a**, **88b** at its front end **100'** and two axial abutment surfaces **90a**, **90b** at its rear end **100''** (only one front axial abutment surface **88b** and one rear axial abutment surface **90b** are seen in Fig. 9. However, the arrangement of the abutment surfaces is the same as that of the abutment surfaces for the medium length cutting insert **24** shown in the perspective view in Fig. 7). The axial abutment surfaces are transverse to the axis of rotation **B** of the cutting insert. The cutting insert **106** shown in Fig. 10 is relatively long and is provided with two circular bores, a forward circular bore **108** and a rear circular bore **110** having bore axes **112** and **114**, respectively. The bore diameter **D1**, **D2** of each of the two circular bores are of substantially equal magnitude $D1=D2=D$ and each bore axis is located at substantially the same distance $X1=X2=X$ from the center of the cutting insert **116** in a top view of the cutting insert. The distance between the two bore axes $X+X=2X$ is greater than a bore diameter **D**. The bore axes **112**, **114** are perpendicular to the axis of rotation **B** of the cutting insert and lie in a vertical longitudinal median plane of the cutting insert.

The cutting insert **24** shown in Figs. 7 and 8 is of an intermediate length its length being typically of the order of $1.5W$, and is provided with a single through hole **118** formed from two intersecting circular bores, a forward circular bore **120** and a rear circular bore **122** having bore axes **124** and **126**, respectively. The bore diameter of the forward circular bore **120** is

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substantially equal in magnitude to the bore diameter of the rear circular bore 122 and, in a top view of the cutting insert 24, each bore axis is located at substantially the same distance from the center 128 of the cutting insert 24. The distance between the two bore axes is less than a bore diameter and therefore the two bores overlap. The bore axes 124, 126 are perpendicular to the axis of rotation B of the cutting insert and lie in a vertical longitudinal median plane of the cutting insert.

The two dotted lines in Fig. 7 divide the insert upper clamping surface 64 into three regions, two substantially identical outer regions 64' separated by a central region 64". This division into three regions is not a physical division, since all portions of the insert upper clamping surface 64 lie on the same concave surface. However, when the cutting insert is clamped in the cutting insert holder 22 of the embodiment shown in Figs. 4a, 4b and 5b (as will be described in greater detail below, with respect to Fig. 18), the outer regions 42' of the lower clamping surface 42 of the upper clamping jaw 32 abut the insert upper clamping surface 64 along the outer regions 64' thereof. Hence, the outer regions 64' of the insert upper clamping surface 64 are regions that correspond to the outer regions 42' of the lower clamping surface 42 of the upper clamping jaw 32. Similarly, the insert lower clamping surface 66 is divided into three regions, two substantially identical outer regions 66' separated by a central region 66". The two outer regions 66' correspond to the two outer regions 50' of the upper clamping surface 50 of the lower clamping jaw 34.

It should be noted that the outer regions 64' of the insert upper clamping surface 64 extend to the upper edge 70 thereof. Similarly, the outer regions 66' of the insert lower clamping surface 66 extend to the upper edge 72 thereof. In a similar manner, the clamping surfaces of the cutting inserts 100, 106 shown in Figs. 9 and 10 are divided into three regions.

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Attention is now drawn to Fig. 11. The clamping screw **26** of the present invention has a screw axis **C** and comprises generally three portions; an upper portion **140**, a central portion **142** and a lower portion **144**. The upper portion **140** comprises an upper cylindrical portion **146** and an upper frusto-conical portion **148**. The upper frusto-conical portion **148** tapers downwardly and inwardly from the upper cylindrical portion **146** toward the central portion **142**. The clamping screw upper portion **140** is provided with a socket **149** such as a Torx or hexagonal socket, for receiving a wrench for tightening or loosening the clamping screw **26**. The clamping screw central portion **142** has a central cylindrical portion **150** connected at its upper end to the upper frusto-conical portion **148** and at its lower end to a central frusto-conical portion **152**. The central frusto-conical portion **152** tapers downwardly and inwardly from its upper end, where it is connected to the central cylindrical portion **150**, to its lower end where it is connected, via a narrow neck portion **154**, to the clamping screw lower portion **144**. The clamping screw lower portion **144** comprises a threaded portion **156** of the clamping screw **26**. The central frusto-conical portion **152** tapers at an angle θ to the screw axis **C**. This angle will be referred to herein as the angle of taper of the central frusto-conical portion **152**.

Attention is now drawn to Figs. 12 to 16, illustrating the principle stages involved in clamping the cutting insert in the cutting insert holder **22**. For illustrative purposes the cutting insert holder **22** shown in Figs. 12 to 16 is in accordance with the first embodiment wherein, in an end view of the cutting insert holder **22** the lower clamping surface **42** of the upper clamping jaw **32** and the upper clamping surface **50** of the lower clamping jaw **34** and are both uniformly convex. The cutting insert shown in these figures is a cutting insert **100** with a single circular through bore **102**. Furthermore, for simplicity of illustration the case $R1=R2=R$ and $r1=r2=r$ is considered. The gaps between the cutting insert **100** and the

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cutting insert holder **22**, between the clamping screw **26** and the cutting insert holder **22**, and between the clamping screw **26** and the cutting insert **100** are not to scale and have been exaggerated for illustrative purposes.

Figs. 12 and 14 show the initial arrangement after the cutting insert **100** has been placed in the insert receiving slot **36** and the clamping screw **26** has been positioned in the cutting insert holder **22**, so that it passes through the bore **44** in the upper clamping jaw **32**, through the through bore **102** in the cutting insert **100** and is received in the threaded bore **52** in the lower clamping jaw **34**. In this position, due to the fact that $R=r+\delta$, the insert lower clamping surface **66** rests on the upper clamping surface **50** of the lower clamping jaw **34** with the outer regions **66'** of the insert lower clamping surface **66** engaging the upper clamping surface **50** of the lower clamping jaw **34** and with a maximum clearance **d** between the central region **66''** of the insert lower clamping surface **66** and the central region **50''** of the upper clamping surface **50** of the lower clamping jaw **34**. In accordance with a specific application the clearance **d** is typically of the order of 0.005 mm to 0.02 mm. There is also a clearance **h** between the insert upper clamping surface **64** and the lower clamping surface **42** of the upper clamping jaw **32**.

The through bore **44** in the upper clamping jaw **32** and the threaded bore **52** in the lower clamping jaw **34** have a common longitudinal bore axis **E**. The screw axis **C** coincides with the longitudinal bore axis **E** and makes an angle ϕ with a normal **N** to the axis of rotation **A** of the cutting insert holder **22**. The angle ϕ is chosen to be equal to the angle of taper θ of the central frusto-conical portion **152**. With this choice of the angle ϕ , the rearmost generator **153''** (i.e., rearmost longitudinally directed straight line on the central frusto-conical portion **152**) of the central frusto-conical portion **152** is parallel to the normal **N** to the axis of rotation **A**.

Fig. 13 shows the situation after the clamping screw **26** has been

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tightened until the upper frusto-conical portion **148** of the clamping screw **26** engages a corresponding frusto-conical bore **158** that constitutes part of the through bore **44** in the upper clamping jaw **32**. It is pointed out that due to the fact that the rearmost generator **153''** of the central frusto-conical portion **152** is parallel to the normal **N**, that as the clamping screw **26** is tightened the rearmost generator of the central frusto-conical portion **152** moves parallel to itself and therefore is always parallel to the normal **N** to the axis of rotation **A**. In a non-binding example, for the position shown in Fig. 13, the clearance **h** between the insert upper clamping surface **64** and the lower clamping surface **42** of the upper clamping jaw **32** is approximately 0.1 mm. There is a clearance **x**, of approximately 0.035 mm, between the rearmost generator **153''** of the central frusto-conical portion **152** and the rear portion **102''** of the circular bore **102** of the cutting insert **100**.

Fig. 15 shows the situation after further tightening of the clamping screw **26**. During the tightening of the clamping screw **26** the clearance **h** between the insert upper clamping surface **64** and the lower clamping surface **42** of the upper clamping jaw **32** is gradually reduced and a force is exerted by the clamping jaws on the insert clamping surfaces causing the cutting insert **100** to become longitudinally aligned in the cutting insert holder **22** so that the longitudinal axis of rotational symmetry **B** of the cutting insert becomes aligned with the axis of rotation **A** of the cutting insert holder **22**. In passing from the situation shown in Fig. 13 to that shown in Fig. 15, the clamping screw **26** has moved a vertical distance of approximately 0.1 mm and a corresponding horizontal distance of 0.005 mm, reducing the clearance **x** between the rearmost generator **153''** of the central frusto-conical portion **152** and the rear portion **102''** of the circular bore **102** of the cutting insert **100** to approximately 0.03 mm

As the clamping screw **26** is further tightened, the rearmost

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generator **153**" of the central frusto-conical portion **152** engages the rear portion **102**" of the circular bore **102** of the cutting insert **100** and urges the cutting insert rearwardly until the clearance between the axial abutment surfaces **90a**, **90b** at the rear **100**" of the cutting insert **100** and the insert axial location surfaces **56**, **58** at the rear **36**" of the insert receiving slot **36** is completely closed and the axial abutment surfaces **90a**, **90b** engage the insert axial location surfaces **56**, **58**. As shown in Figs. 16 and 17, the cutting insert **100** is now firmly clamped, both radially and longitudinally, in the insert receiving slot **36** of the cutting insert holder **22**.

10 For the relatively long cutting insert **106**, the procedure for clamping the cutting insert in the cutting insert holder is similar to that described above for the short cutting insert **100**. Clearly, the axial dimension of the insert receiving slot **36** will be longer in this case. Furthermore, the cutting insert holder is preferably designed so that the clamping screw **26** is received in the forward circular bore **108** and during the clamping of the cutting insert **106** the clamping screw **26** engages a rear portion **108**" of the circular bore **108**.

For the cutting insert **24** of intermediate length, the cutting insert holder is preferably designed so that the clamping screw **26** is received in the forward circular bore **120**. However, in contrast to the relatively short cutting insert **100** and the relatively long cutting insert **106**, in the case of the cutting insert **24** of intermediate length the forward circular bore **120** intersects the rear circular bore **122** and therefore the forward circular bore **120** has no rear portion (see Fig. 8). Hence, during the clamping process, the central frusto-conical portion **152** of the clamping screw **26** engages the forward circular bore **120** at two rear side portions **120**", close to the intersection of the forward and rear circular bores **120**, **122** and lying on either side of the longitudinal median plane **M** the axis of rotation **B** and through the second transverse axis of rotational symmetry **T2** of the cutting

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insert **24**. The forward circular bore **120** is engaged by the clamping screw **26** at the two rear side portions of the central frusto-conical portion **152** corresponding to the rear side portions **120''** of the forward circular bore **120**. Each of the two rear side portions of the central frusto-conical portion **152** is located in a region of a portion of a rear side generator **153'** of the central frusto-conical portion **152** of the clamping screw **26**. A rear side generator **153'** is shown in Fig. 11 by a dashed line. In Fig. 11, only one of the two rear side generators **153'** is seen, the other one being on the side of the central frusto-conical portion **152** not seen in the figure, parallel to and "directly behind" the rear side generator **153'** that is seen. In order to increase the areas of engagement between the two rear side portions of the central frusto-conical portion of the clamping screw and the two the rear side portions **120''** of the forward circular bore **120**, the design of the through hole **118** can be suitably altered in the regions of the two the rear side portions **120''**, as will be apparent to a person skilled in the art.

Fig. 18 shows the situation after the final tightening of the clamping screw **26**, for a cutting tool assembly having a cutting insert holder **22** with the clamping surfaces of the clamping jaws divided into three regions (as shown in Fig. 5b), in accordance with a preferred embodiment of the present invention. As can be seen, the regions of abutment between the upper surface of the cutting insert and the lower clamping surface of the upper clamping jaw **32** is restricted to the outer regions **64'** of the clamping surfaces of the cutting insert and the corresponding outer regions **42'** of the lower clamping surface of the upper clamping jaw **32**. Since the central region **42''** of the lower clamping surface **42** has a larger radius of curvature than that of the outer regions **42'**, a clearance is formed between the central region **42''** of the lower clamping surface **42** and the central region **64''** of the insert upper clamping surface **64**. Therefore, in accordance with the embodiment of the cutting

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insert holder with the clamping surfaces of the clamping jaws divided into three regions, the central region 42'' of the lower clamping surface 42 becomes a clearance surface and does not engage the central region 64'' of the insert upper clamping surface 64. Similarly, the regions of abutment between the insert lower clamping surface 66 and the upper clamping surface 50 of the lower clamping jaw 34 are restricted to the outer regions 66' of the insert lower clamping surface 66 and the corresponding outer regions 50' of the upper clamping surface 50 of the lower clamping jaw 34. Therefore, in accordance with the embodiment of the cutting insert holder with the clamping surfaces of the clamping jaws divided into three regions, the central region 50'' of the upper clamping surface 50 becomes a clearance surface and does not engage the central region 66'' of the insert lower clamping surface 66. This arrangement assures that the clamping forces applied by the clamping jaws of the cutting insert holder on the clamping surfaces of the cutting insert are applied to the outer (or, side) regions of the clamping surfaces, thereby giving support to the cutting edges extending along the sides of the cutting insert from the front of the cutting insert to the rear of the cutting insert.

It should be noted, that in accordance with the present invention, the insert upper clamping surface 64 engages the lower clamping surface 42 of the upper clamping jaw 32 and the insert lower clamping surface 66 engages the upper clamping surface 50 of the lower clamping jaw 34. Furthermore, in accordance with the preferred embodiment of the present invention, the central region 42'' of the lower clamping surface 42 does not engage the central region 64'' of the insert upper clamping surface 64 and the central region 50'' of the upper clamping surface 50 does not engage the central region 66'' of the insert lower clamping surface 66, hence only the outer regions 64', 66' of the cutting insert engage the clamping surfaces 42, 50 of the clamping jaws. This is in complete contrast with the situation in

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EP 0 417 862 B1, wherein the side portions (numbered **16a**, **16b** and **16' a**, **16' b** therein) of the cutting insert described therein do not engage the clamping surfaces of the clamping jaws.

In Fig. 18 two angles $\alpha 1$ and $\alpha 2$ are defined relative to the center of curvature **O** of the lower clamping surface **42** of the upper clamping jaw **32**. The angles $\alpha 1$ and $\alpha 2$ are defined in a plane perpendicular to the axis of rotation **A** of the cutting insert holder **22**. Hence, the dashed lines and the points **O**, **P1** and **P2** are all located in the same plane perpendicular to the axis of rotation **A**. The angle $\alpha 1$ defines the angular location of the innermost point of contact **P1** between an outer region **42'** of the lower clamping surface **42** of the upper clamping jaw **32** and the insert upper clamping surface **64**. The angle $\alpha 2$ defines the angular location of the outermost point of contact **P2** between an outer region **42'** of the lower clamping surface **42** of the upper clamping jaw **32** and the insert upper clamping surface **64**. Since $\alpha 2$ is greater than $\alpha 1$, and since the clamping force on the cutting insert is applied in a direction parallel to the longitudinal vertical median plane **M** of the cutting insert, which coincides with a longitudinal vertical median plane of the cutting tool assembly when the cutting insert is retained in the cutting insert holder, the condition for sliding contact between the insert upper clamping surface **64** and the lower clamping surface **42** of the upper clamping jaw **32** is that $\alpha 1$ be greater than the angle of friction. In accordance with a specific application the cutting insert holder **22** is made of steel and the cutting insert **24**, **100**, **106** is made of cemented carbide. In accordance with this specific application $\alpha 1$ should be greater than 10° . Preferably, $\alpha 2$ is approximately 30° .

Although the present invention has been described to a certain degree of particularity, it should be understood that various alterations and modifications can be made without departing from the spirit or scope of the invention as hereinafter claimed. In particular, the invention has been

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demonstrated with respect to a ball nose end mill having a single replaceable cutting insert retained between the clamping jaws of the ball nose end mill. It will be appreciated that the invention does not relate to a specific type of milling cutter but relates to any milling cutter having a single replaceable
5 cutting insert retained between the clamping jaws of the milling cutter, provided that the clamping surfaces of the clamping jaws are at least partially convex and the insert clamping surfaces are concave and that the radius of curvature of the clamping surfaces of the clamping jaws is larger than the radius of curvature of the insert clamping surfaces.

We claim:

1. A cutting tool assembly comprising a cutting insert holder, a cutting insert and a clamping screw, the cutting insert holder comprising a clamping portion connected to a body portion;

the clamping portion comprising:

a lower clamping jaw having a lower peripheral surface and an upper clamping surface;

an upper clamping jaw resiliently connected to the lower clamping jaw, the upper clamping jaw having a lower clamping surface and an upper peripheral surface;

a through bore passing through the upper and lower clamping jaws, the through bore being threaded in one of the upper or lower clamping jaws;

an insert receiving slot defined between the upper and lower clamping surfaces;

the cutting insert comprising:

an insert upper clamping surface bounded by an upper edge;

an insert lower clamping surface bounded by a lower edge;

a peripheral side surface between the insert upper clamping surface and the insert lower clamping surface;

at least one cutting edge associated with the peripheral side surface;

at least one through hole passing through the cutting insert between the insert upper and lower clamping surfaces;

wherein:

in a front view of the cutting tool assembly, the upper and lower clamping surfaces of the lower and upper clamping jaws, respectively, are partially convex, and the insert lower and upper clamping surfaces are concave;

the cutting insert is retained in the insert receiving slot in a retained position by means of the clamping screw which passes through the through bore in the upper and lower clamping jaws of the cutting insert holder and through the at least one through hole in the cutting insert and is screwed into the threaded through bore in one of the upper or lower clamping jaws;

the lower clamping surface of the upper clamping jaw engages the insert upper clamping surface at least one upper region of contact and the upper clamping surface of the lower clamping jaw engages the insert lower surface at least one lower region of contact;

wherein:

at least a portion of the insert upper clamping surface conforms with a portion of a first cylindrical surface having a first radius of curvature, r_1 , and a first cylinder axis;

at least a portion of the insert lower clamping surface conforms with a portion of a second cylindrical surface having a second radius of curvature, r_2 , and a second cylinder axis;

the upper clamping surface of the lower clamping jaw partially conforms with a third cylindrical surface having a third radius of curvature, R_2 , and a third cylinder axis;

the lower clamping surface of the upper clamping jaw partially conforms with a fourth cylindrical surface having a fourth radius of curvature, R_1 , and a fourth cylinder axis;

the fourth radius of curvature, R_1 , is greater than the first radius of curvature, r_1 , the third radius of curvature, R_2 , is greater than the second radius of curvature, r_2 .

2. The cutting tool assembly according to claim 1, wherein the cutting insert holder has an axis of rotation (A) and the cutting insert has a longitudinal axis of rotational symmetry (B) and a center through which the longitudinal axis of rotational symmetry (B) passes, the longitudinal axis of rotational symmetry (B) constituting an axis of rotation of the cutting insert about which the cutting insert has 180 degree rotational symmetry.
3. The cutting tool assembly according to claim 2, wherein the first radius of curvature and the second radius of curvature are equal in magnitude, $r_1=r_2$, defining a radius of curvature, r , of the cutting insert clamping surfaces, and the third radius of curvature and the fourth radius of curvature are equal in magnitude, $R_1=R_2$, defining a radius of curvature, R , of the clamping jaw's clamping surfaces.
4. The cutting tool assembly according to claim 3, wherein the at least one upper region of contact comprises at least two outer regions of the insert upper clamping surface and the at least one lower region of contact comprises at least two outer regions of the insert lower clamping surface.
5. The cutting tool assembly according to claim 4, wherein $r \leq 16$ mm and $R \leq 16.2$ mm.
6. The cutting tool assembly according to claim 4, wherein the cutting insert has a width, W , which is greater than a first thickness, T , where the width and first thickness are measured in a front view of the cutting insert as, respectively, the distance between opposing portions of the peripheral side surface, and a maximum distance between the insert upper and lower clamping surfaces.
7. The cutting tool assembly according to claim 6, wherein W/T lies in the range 2.5 to 4.0.
8. The cutting tool assembly according to claim 6, wherein W/T is equal to 3.3.
9. The cutting tool assembly according to claim 6, wherein the width W is greater than a second thickness t that is measured, in a front view of the

cutting insert, as a minimum distance between the insert upper and lower clamping surfaces.

10. The cutting tool assembly according to claim 9, wherein W/t lies in the range 4.0 to 6.0.
11. The cutting tool assembly according to claim 9, wherein W/t is equal to 5.3.
12. The cutting tool assembly according to claim 9 wherein the radius of curvature, r , of the cutting insert clamping surfaces is approximately equal to the width W , and the radius of curvature, R , of the clamping jaw's clamping surfaces is approximately equal to the width W .
13. The cutting tool assembly according to claim 2, wherein the insert receiving slot has a forward end for receiving a cutting insert and a rear end at which the upper clamping jaw is resiliently connected to the lower clamping jaw.
14. The cutting tool assembly according to claim 13, wherein the rear end of the insert receiving slot is provided with at least one insert axial location surface transverse to the axis of rotation (A) of the cutting insert holder.
15. The cutting tool assembly according to claim 14, wherein the rear end of the insert receiving slot is provided with at least one generally cylindrical groove transverse to the axis of rotation (A) of the cutting insert holder and adjacent the at least one insert axial location surface.
16. The cutting tool assembly according to claim 2, wherein the cutting insert has two end portions adjacent the axis of rotation (B) of the cutting insert, at least one of the two end portions being provided with axial abutment surfaces transverse to the axis of rotation (B) of the cutting insert.
17. The cutting tool assembly according to claim 16, wherein the axial abutment surfaces are ground.
18. The cutting tool assembly according to claim 2, wherein the at least one through hole in the cutting insert is implemented as a circular bore having a

bore axis located substantially at the center of the cutting insert in a top view of the cutting insert, the bore axis being perpendicular to the axis of rotation (B) of the cutting insert.

19. The cutting tool assembly according to claim 2, wherein, the at least one through hole in the cutting insert is implemented as two circular bores, each circular bore having a bore axis and a bore diameter (D1, D2), the bore diameter of each circular bore being substantially equal in magnitude, each bore axis being located at substantially the same distance from the center of the cutting insert in a top view of the cutting insert, each bore axis being perpendicular to the axis of rotation (B) of the cutting insert and the distance between the two bore axes being greater than the bore diameters (D1, D2).
20. The cutting tool assembly according to claim 2, wherein the at least one through hole is implemented by two intersecting circular bores, each circular bore having a bore axis and a bore diameter (D1, D2), the bore diameter of each circular bore being substantially equal in magnitude, each bore axis being located at substantially the same distance from the center of the cutting insert in a top view of the cutting insert, each bore axis being perpendicular to the axis of rotation (B) of the cutting insert and the distance between the two bore axes being less than the bore diameters (D1, D2).
21. The cutting tool assembly according to claim 19, wherein the cutting insert is retained in the insert receiving slot in a retained position by means of a clamping screw which passes through the through bore in the upper and lower clamping jaws of the cutting insert holder and through the circular bore in the cutting insert closest the forward end of the insert receiving slot and is screwed into the threaded through bore in one of the upper or lower clamping jaws.
22. The cutting tool assembly according to claim 20, wherein the cutting insert is retained in the insert receiving slot in a retained position by means of a clamping screw which passes through the through bore in the upper and lower clamping jaws of the cutting insert holder and through the circular bore in the

cutting insert closest the forward end of the insert receiving slot and is screwed into the threaded through bore in one of the upper or lower clamping jaws.

23. The cutting tool assembly according to claim 2, wherein, the peripheral side surface of the cutting insert is provided with two diametrically opposite pairs of cutting edges so that when the cutting insert is retained in the insert receiving slot, one pair of cutting edges is located closer to the forward end of the insert receiving slot and constitutes a pair of operative cutting edges and the other pair of cutting edges is located closer to the rear end of the insert receiving slot and constitutes a pair of inoperative cutting edges.
24. The cutting tool assembly according to claim 23, wherein the peripheral side surface is provided with two diametrically opposite notches which are located on a first transverse axis of rotational symmetry (T1) and which separate between the diametrically opposite sets of cutting edges, the first transverse axis of rotational symmetry (T1) passing through the peripheral side surface and perpendicular to the longitudinal axis of rotational symmetry (B), the cutting insert having 180 degree rotational symmetry about the first transverse axis of rotational symmetry (T1).
25. The cutting tool assembly according to claim 24, wherein each pair of cutting edges comprises one cutting edge which extends from a region close to where the longitudinal axis of rotational symmetry (B) passes through the peripheral side surface upwards towards a notch whilst the other cutting edge extends from the same region close to where the longitudinal axis of rotational symmetry passes through the peripheral side surface downwards towards the diametrically opposite notch.
26. The cutting tool assembly according to claim 25, wherein each cutting edge is provided with a relief surface and a rake surface.
27. A cutting tool assembly according to claim 1, wherein the clamping screw has a screw axis c and comprises:

an upper portion;

a central portion; and

a lower portion;

the upper portion comprises an upper cylindrical portion and an upper frusto-conical portion, the upper frusto-conical portion tapers downwardly and inwardly from the upper cylindrical portion towards the central portion, the clamping screw upper portion is provided with a socket, for receiving a wrench for tightening or loosening the clamping screw, the clamping screw central portion has a central cylindrical portion connected at its upper end to the upper frusto-conical portion and at its lower end to a central frusto-conical portion, the central frusto-conical portion tapers downwardly and inwardly from the upper end thereof, to the lower end thereof, at the lower end thereof the central frusto-conical portion is connected, via a narrow neck portion, to the clamping screw lower portion, the clamping screw lower portion comprises a threaded portion of the clamping screw, the central frusto-conical portion tapers at an angle q to the screw axis c .

28. A cutting insert having a longitudinal axis of rotational symmetry (B) and a center through which the longitudinal axis of rotational symmetry (B) passes, the longitudinal axis of rotational symmetry (B) constituting an axis of rotation of the cutting insert about which the cutting insert has 180 degree rotational symmetry, the cutting insert comprising:

an insert upper clamping surface bounded by an upper edge;

an insert lower clamping surface bounded by a lower edge;

a peripheral side surface between the insert upper clamping surface and the insert lower clamping surface;

at least one cutting edge associated with the peripheral side surface;

at least one through hole passing through the cutting insert between the insert upper and lower clamping surfaces;

wherein:

the insert upper clamping surface conforms with a first cylindrical surface having a first radius of curvature, r_1 , and a first cylinder axis;

the insert lower clamping surface conforms with a second cylindrical surface having a second radius of curvature, r_2 , and a second cylinder and

in a front view of the cutting insert, the insert upper and lower clamping surfaces are concave.

29. The cutting insert according to claim 28, wherein the first radius of curvature and the second radius of curvature are equal in magnitude, $r_1 = r_2$, defining a radius of curvature, r , of the cutting insert clamping surfaces.
30. The cutting insert according to claim 28, wherein the cutting insert has a width, W , which is greater than a first thickness, T , where the width and first thickness are measured in a front view of the cutting insert as, respectively, the distance between opposing portions of the peripheral side surface, and a maximum distance between the insert upper and lower clamping surfaces.
31. The cutting insert according to claim 30, wherein W/T lies in the range 2.5 to 4.0.
32. The cutting insert according to claim 30, wherein W/T is equal to 3.3.
33. The cutting insert according to claim 30, wherein the width W is greater than a second thickness t that is measured, in a front view of the cutting insert, as a minimum distance between the insert upper and lower clamping surfaces.
34. The cutting insert according to claim 33, wherein W/t lies in the range 4.0 to 6.0.
35. The cutting insert according to claim 33, wherein W/t is equal to 5.

36. The cutting insert according to claim 28, wherein the cutting insert has two end portions adjacent the axis of rotation (B) of the cutting insert, at least one of the two end portions being provided with axial abutment surfaces transverse to the axis of rotation (B) of the cutting insert.
37. The cutting insert according to claim 36, wherein the axial abutment surfaces are ground.
38. The cutting insert according to claim 28, wherein the at least one through hole in the cutting insert is implemented as a circular bore having a bore axis located substantially at the center of the cutting insert in a top view of the cutting insert, the bore axis being perpendicular to the axis of rotation (B) of the cutting insert.
39. The cutting insert according to claim 28, wherein the at least one through hole in the cutting insert is implemented as two circular bores, each circular bore having a bore axis and a bore diameter (D1, D2), the bore diameter of each circular bore being substantially equal in magnitude, each bore axis being located at substantially the same distance from the center of the cutting insert in a top view of the cutting insert, the bore axes being perpendicular to the axis of rotation (B) of the cutting insert and the distance between the two bore axes being greater than the bore diameters (D1, D2).
40. The cutting insert according to claim 28, wherein the at least one through hole is implemented by two intersecting circular bores, each circular bore having a bore axis and a bore diameter (D1, D2), the bore diameter of each circular bore being substantially equal in magnitude, each bore axis being located at substantially the same distance from the center of the cutting insert in a top view of the cutting insert, the bore axes being perpendicular to the axis of rotation (B) of the cutting insert and the distance between the two bore axes being less than the bore diameters (D1, D2).

Fig. 1

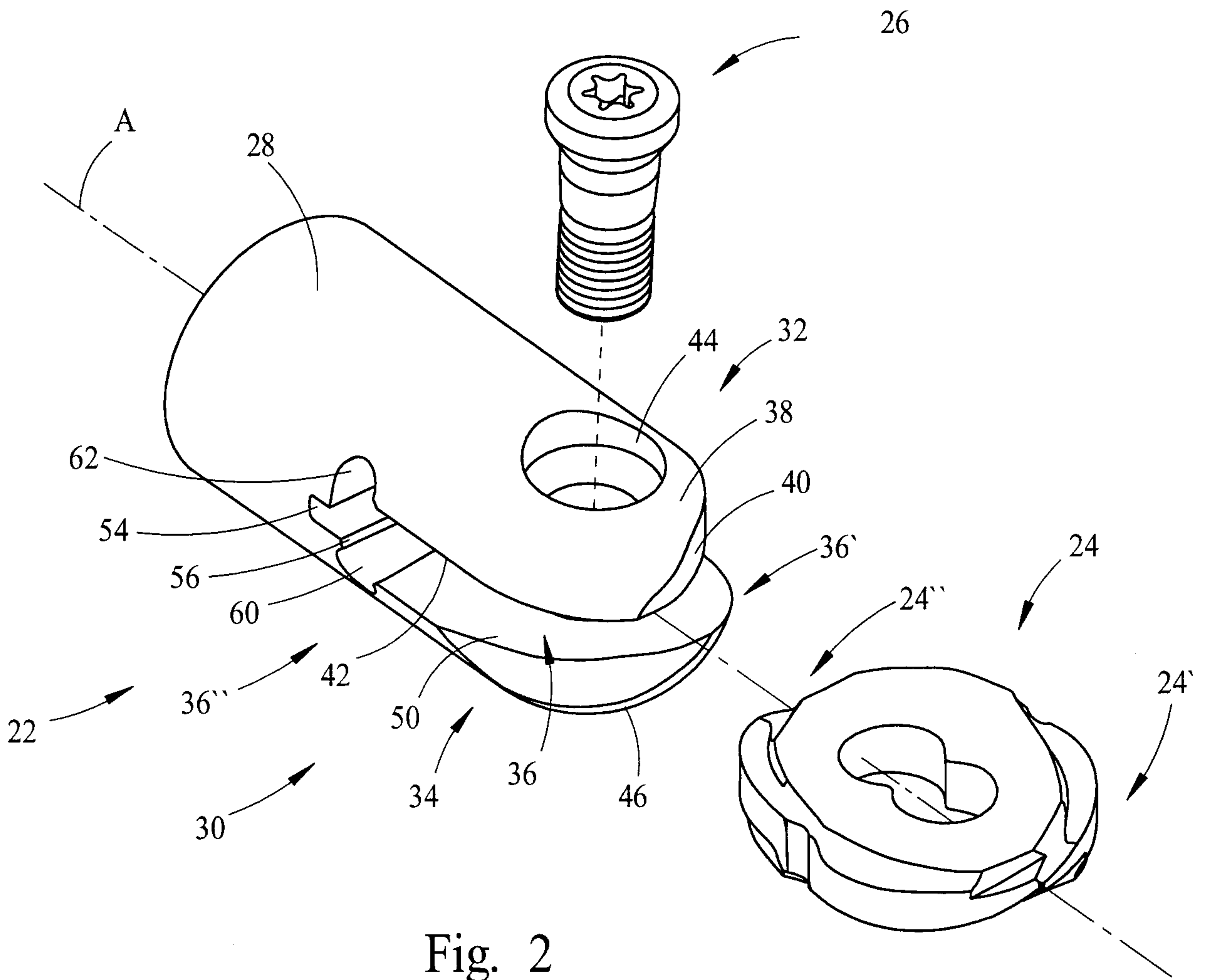
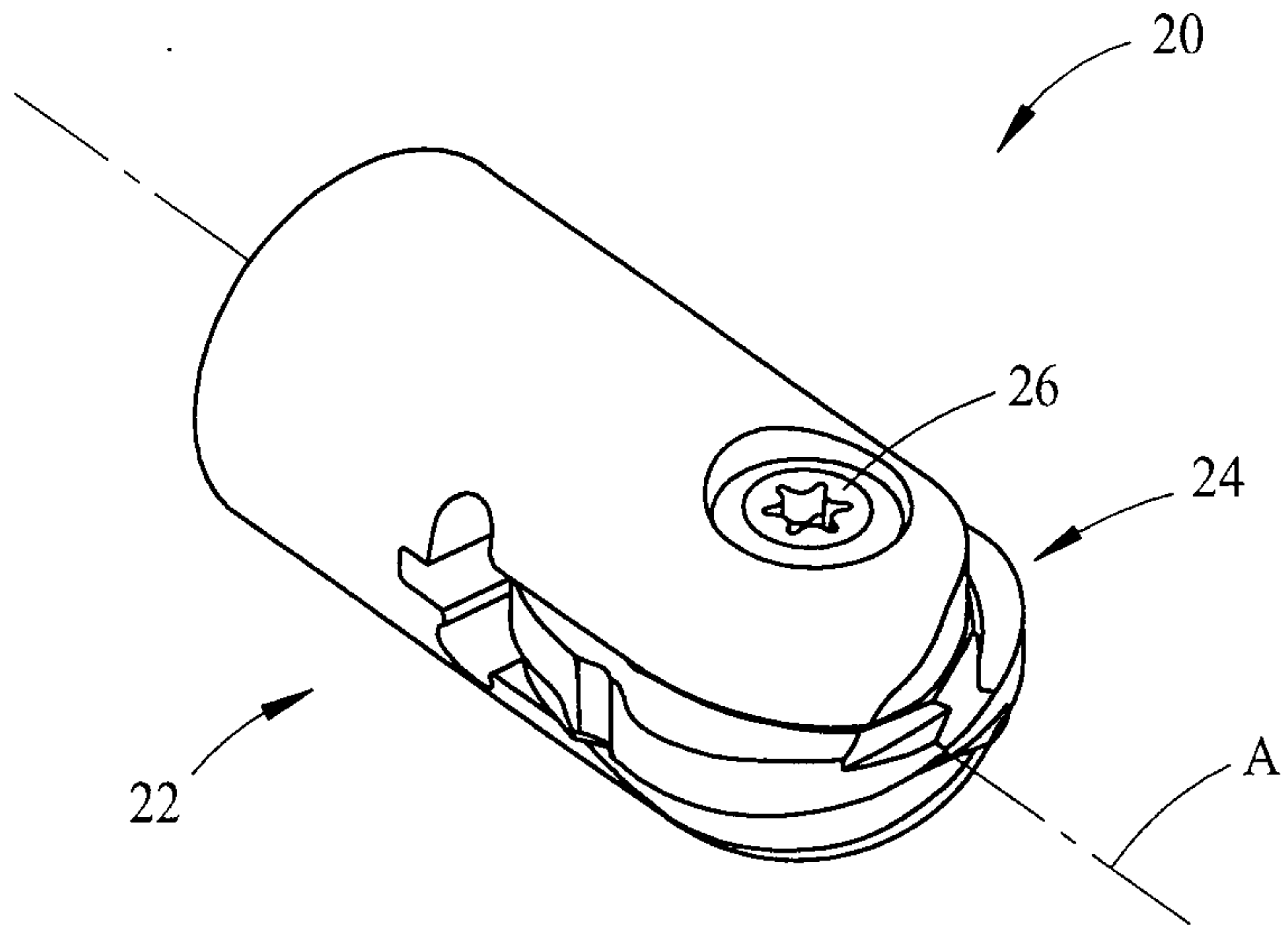
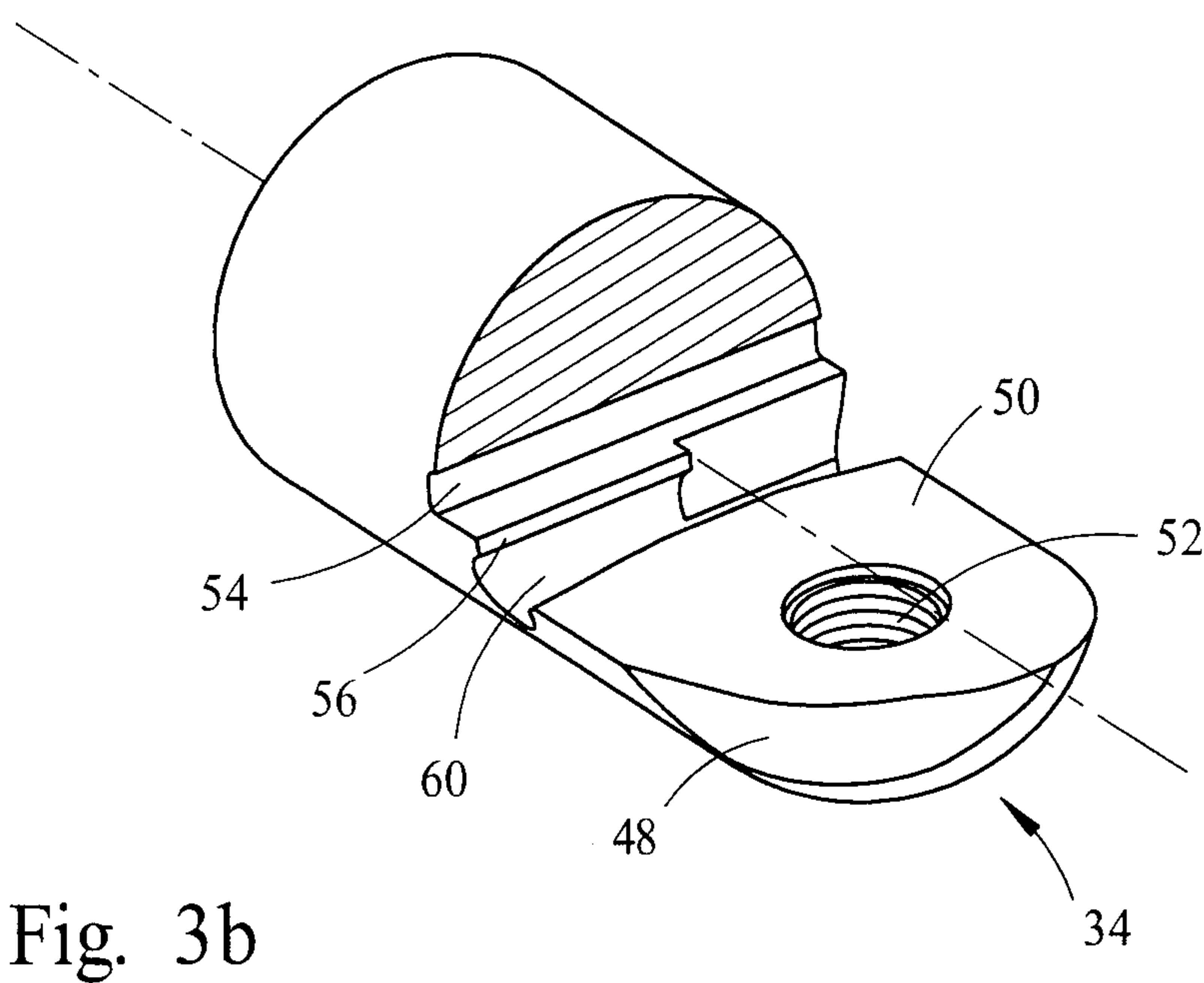
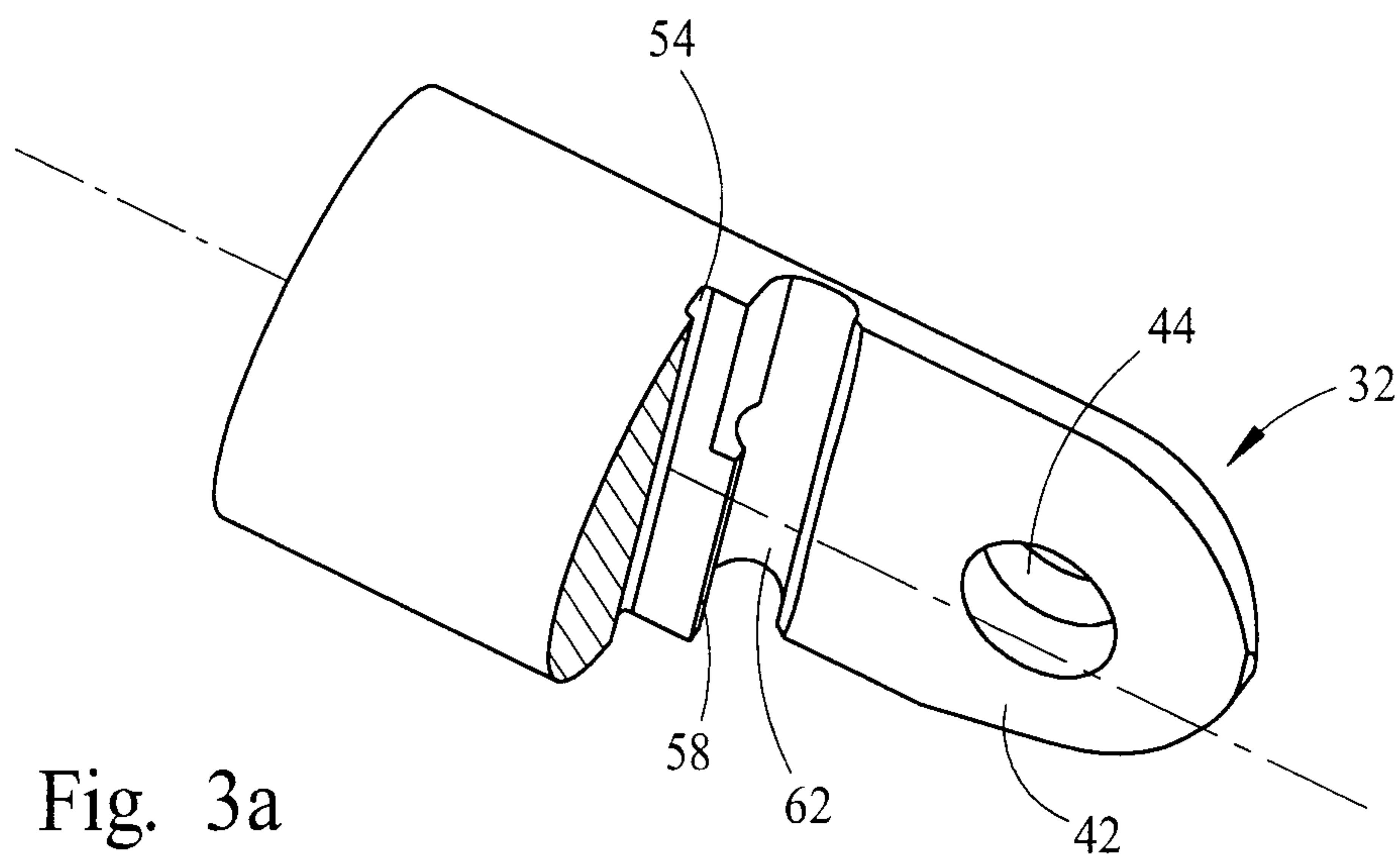


Fig. 2



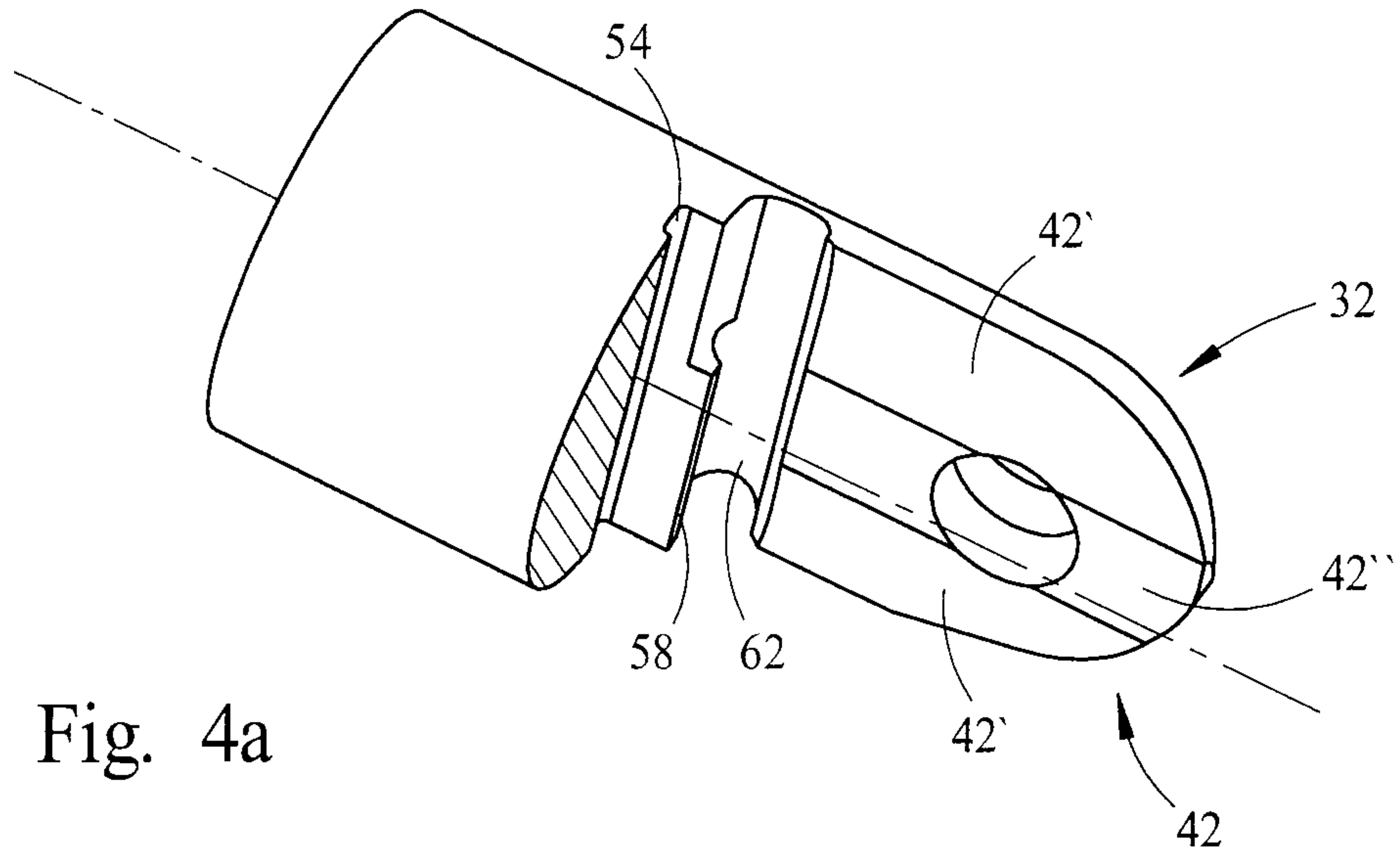


Fig. 4a

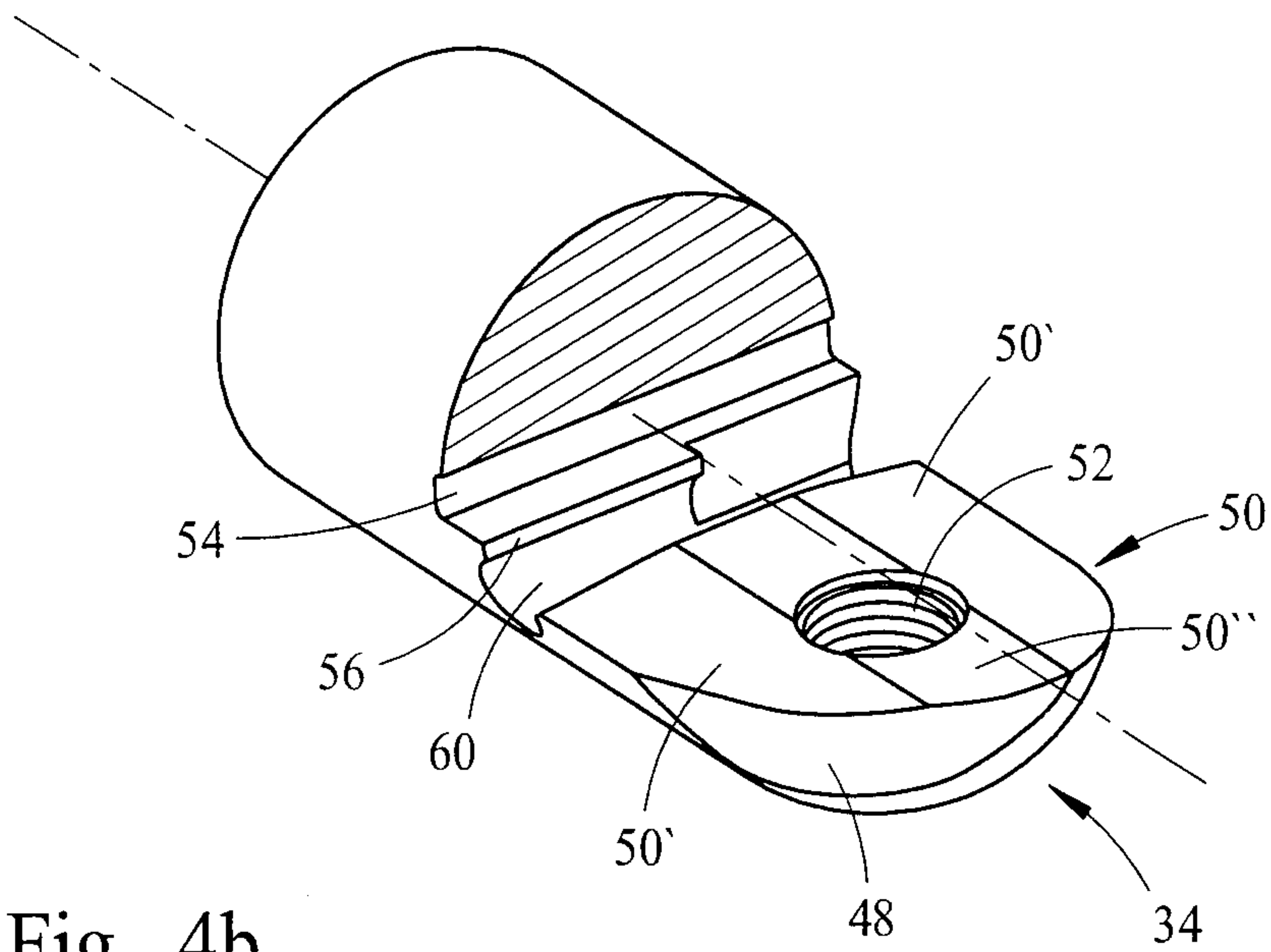


Fig. 4b

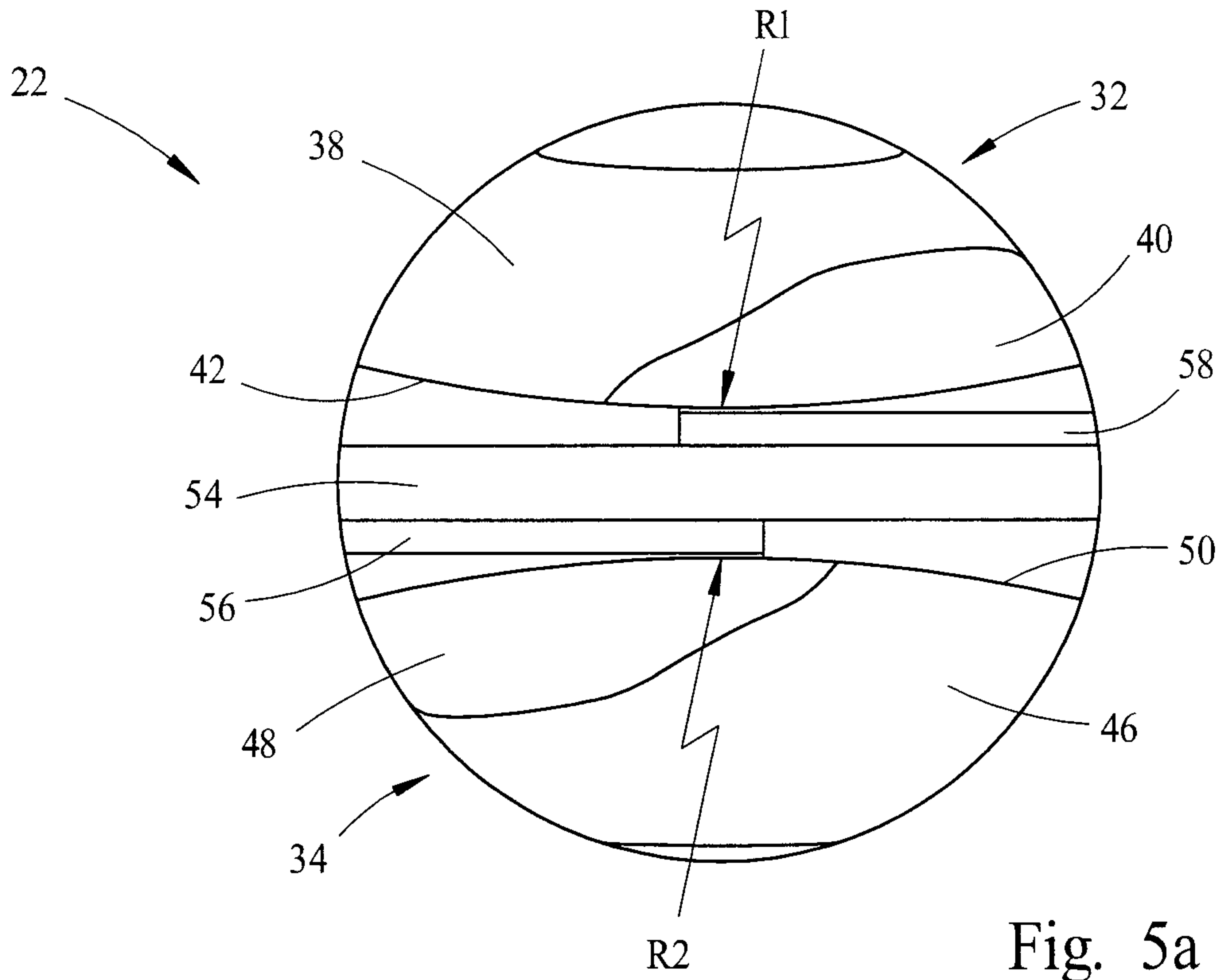


Fig. 5a

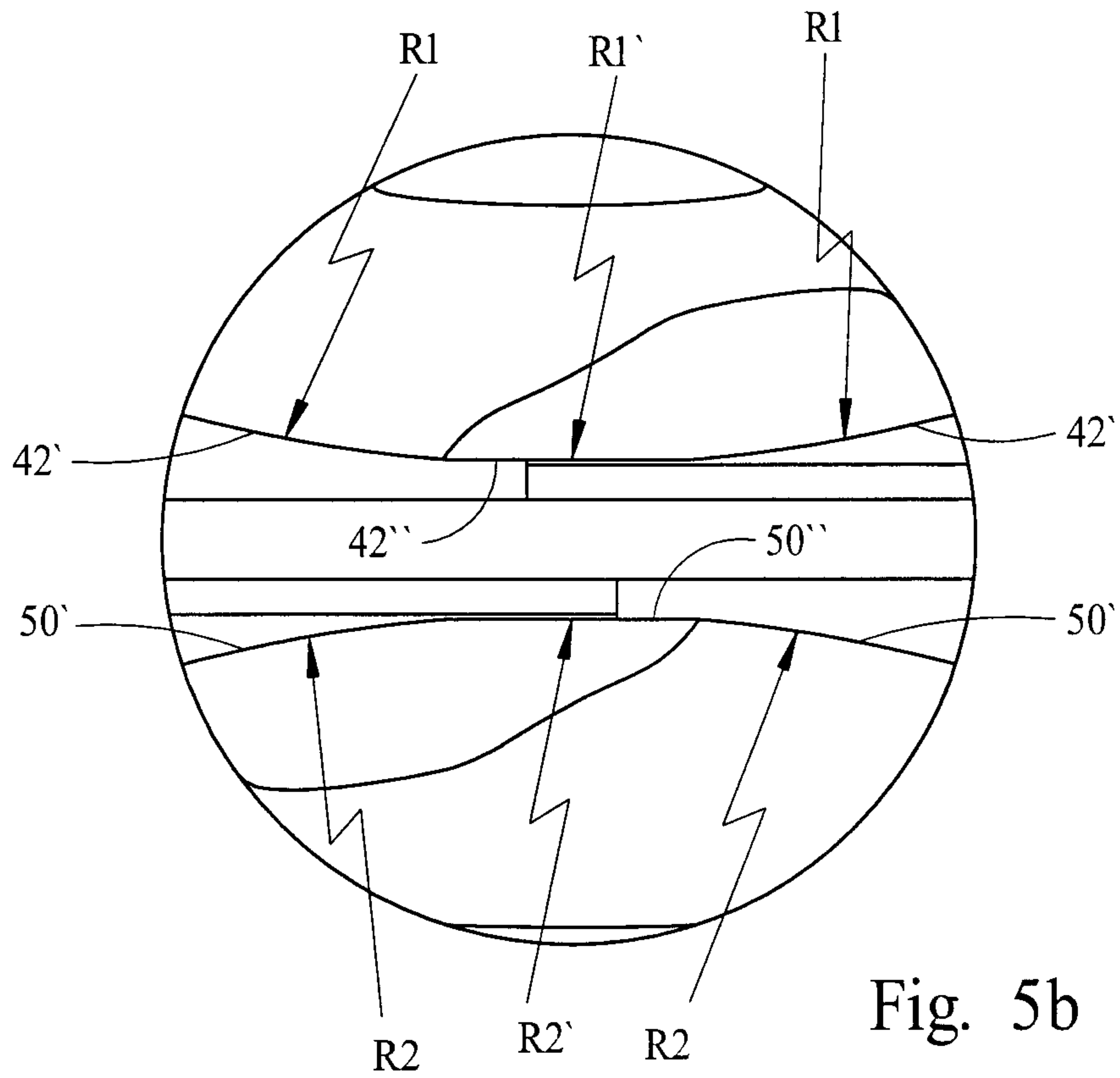


Fig. 5b

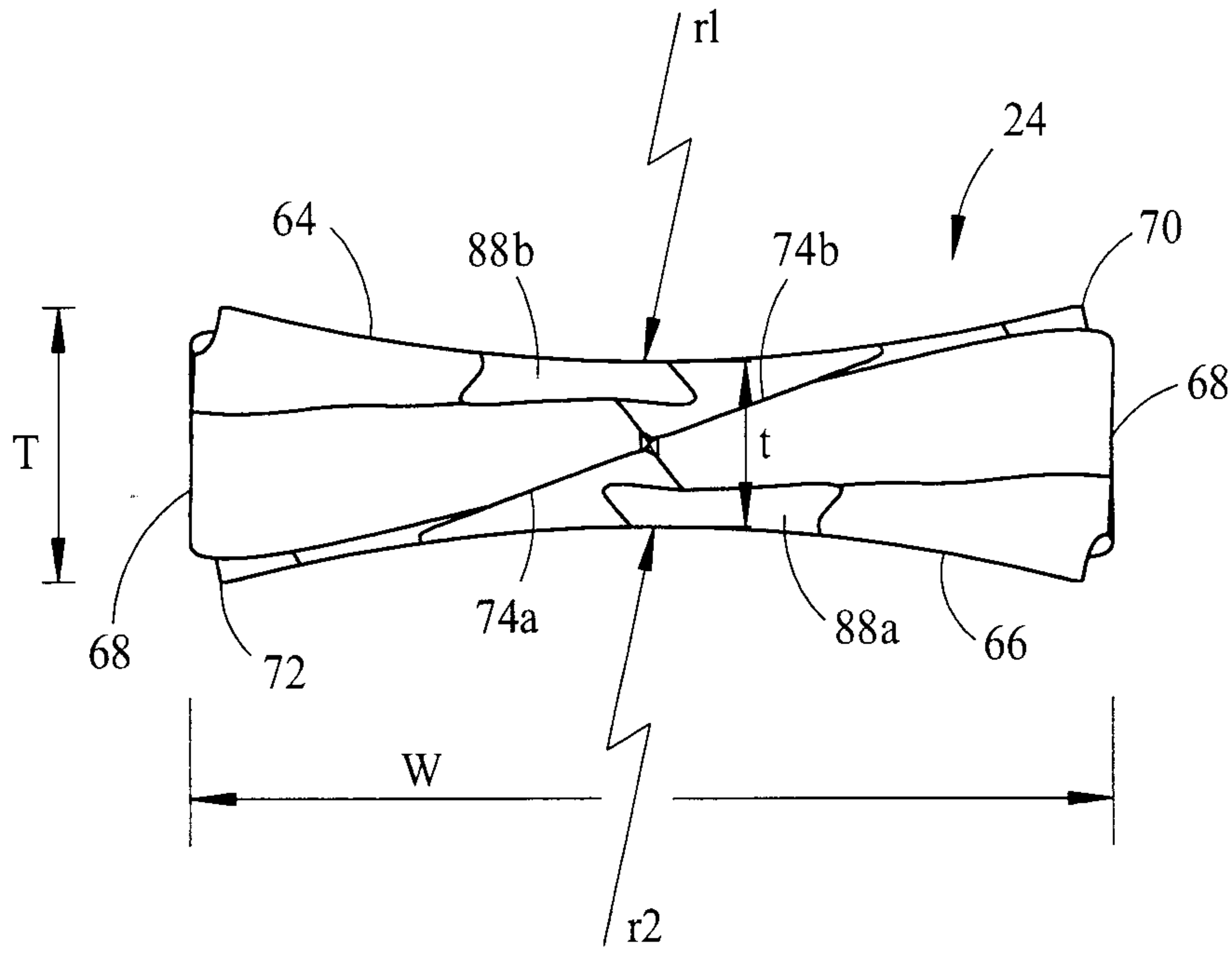


Fig. 6

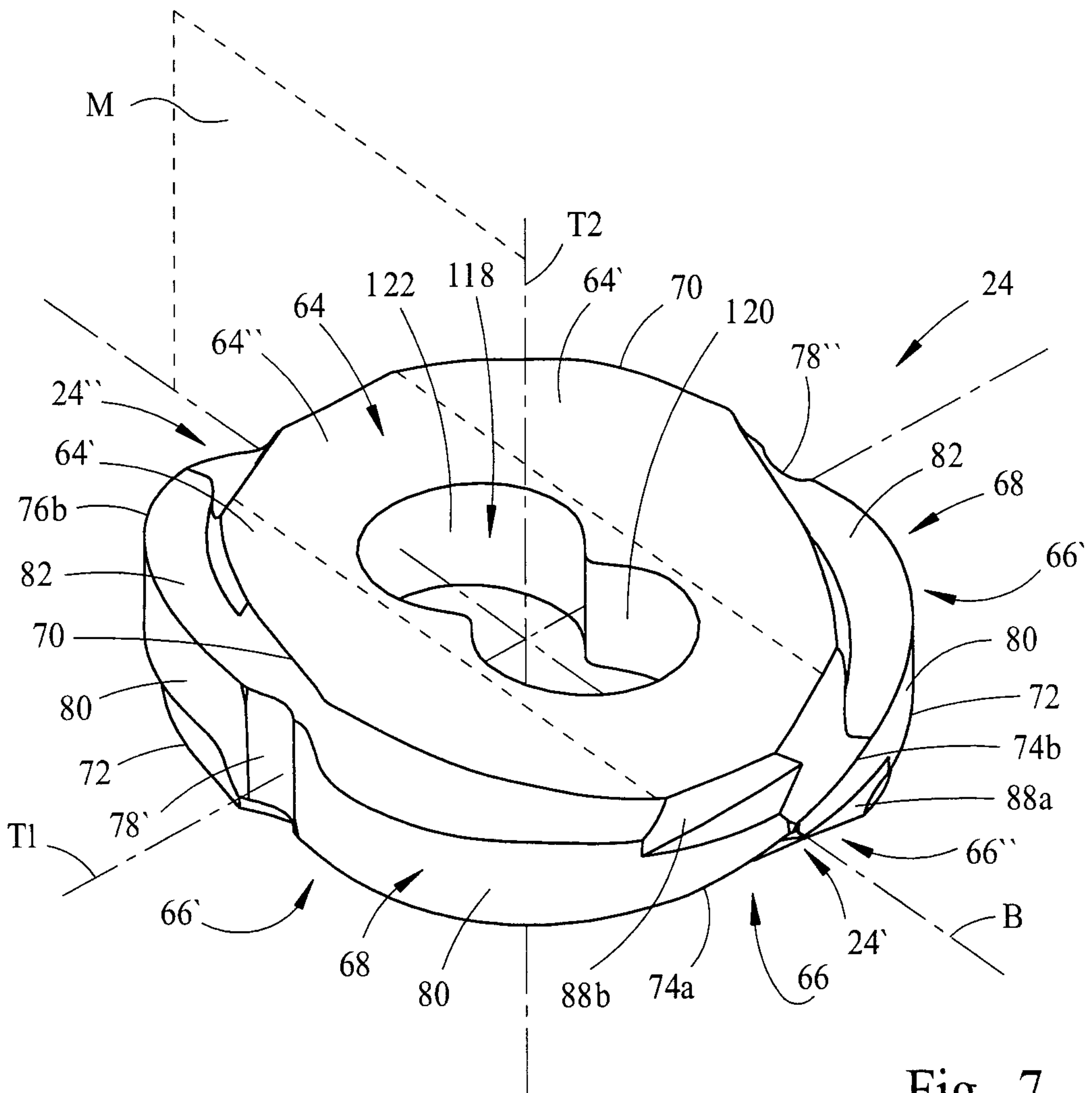


Fig. 7

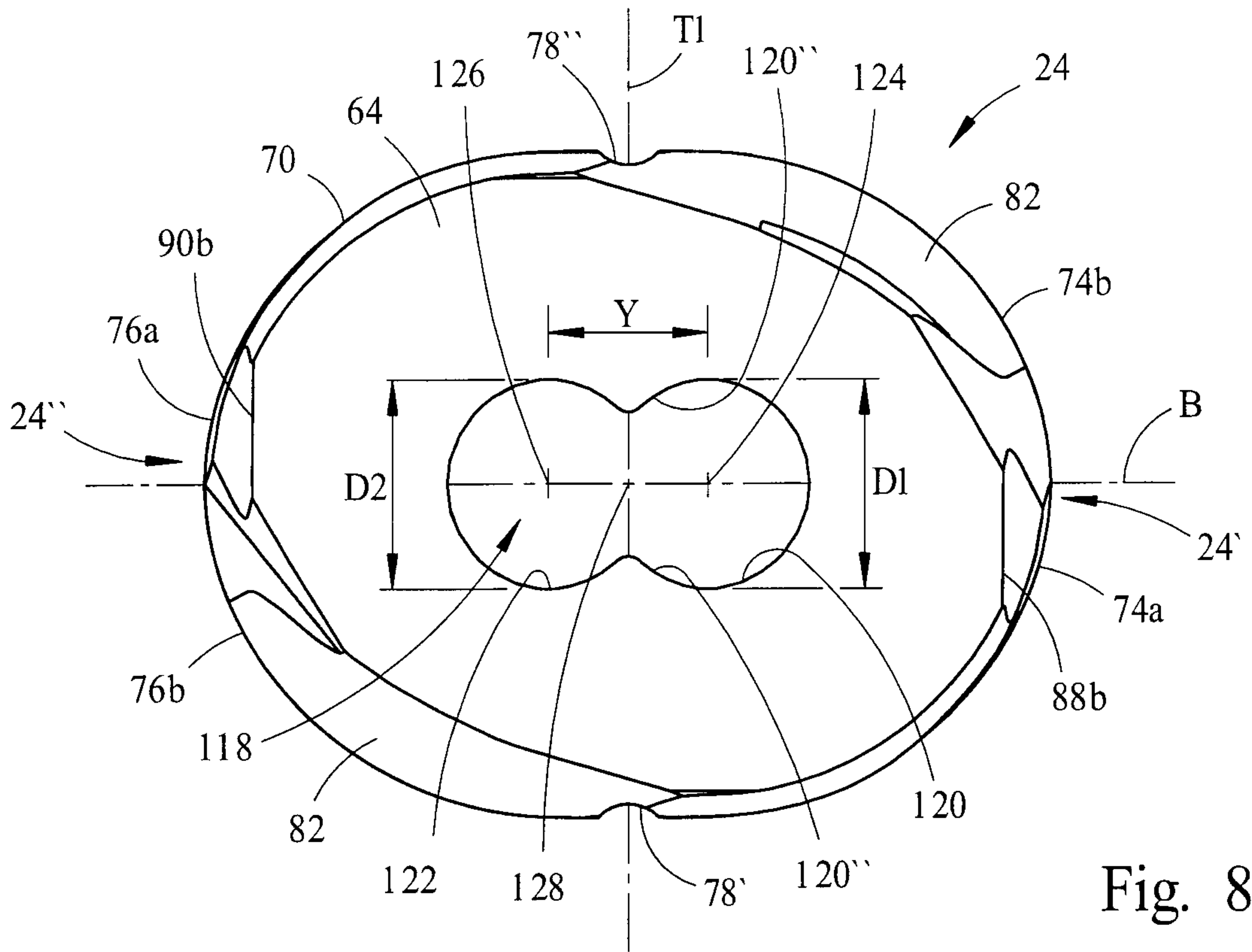


Fig. 8

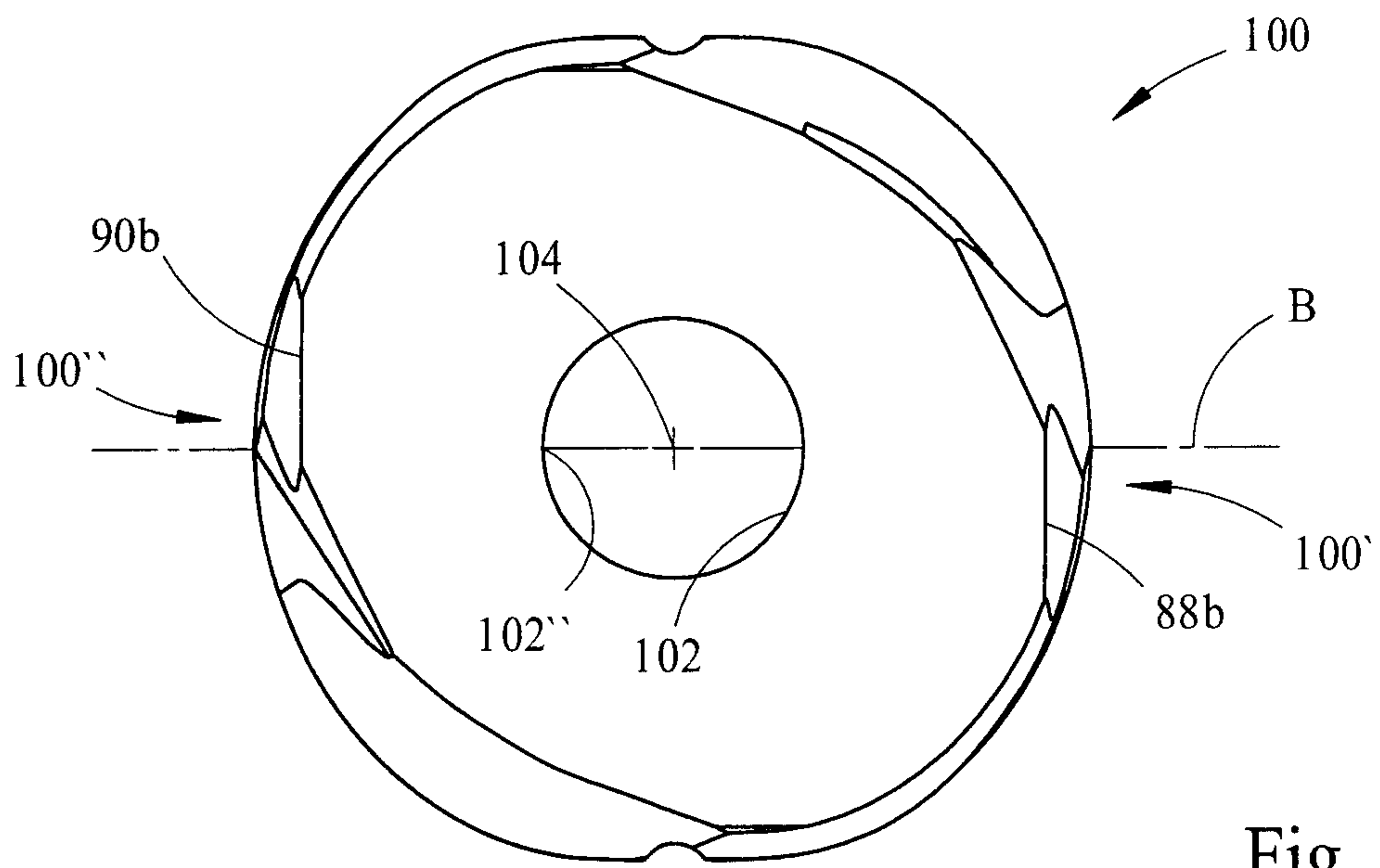


Fig. 9

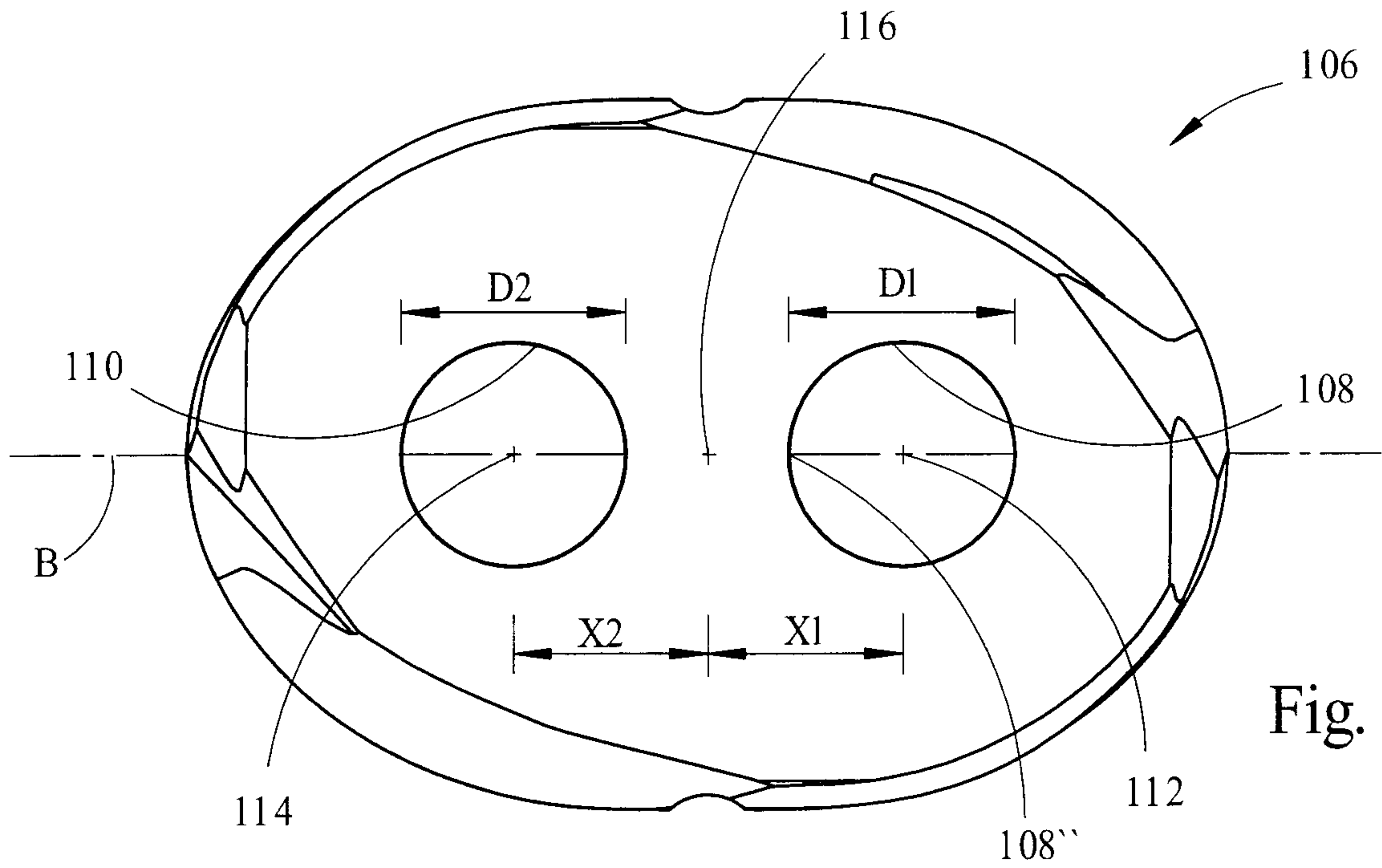


Fig. 10

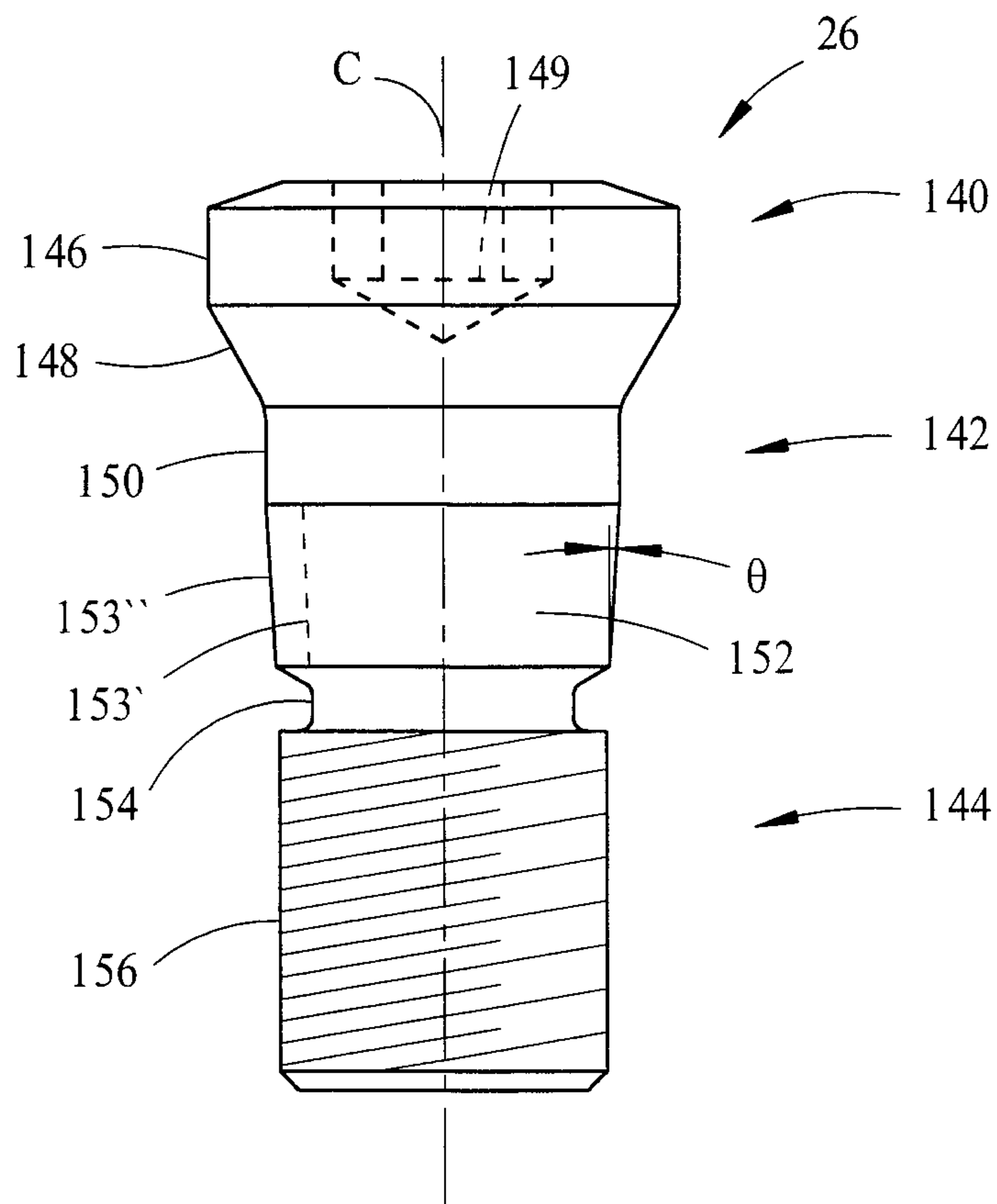


Fig. 11

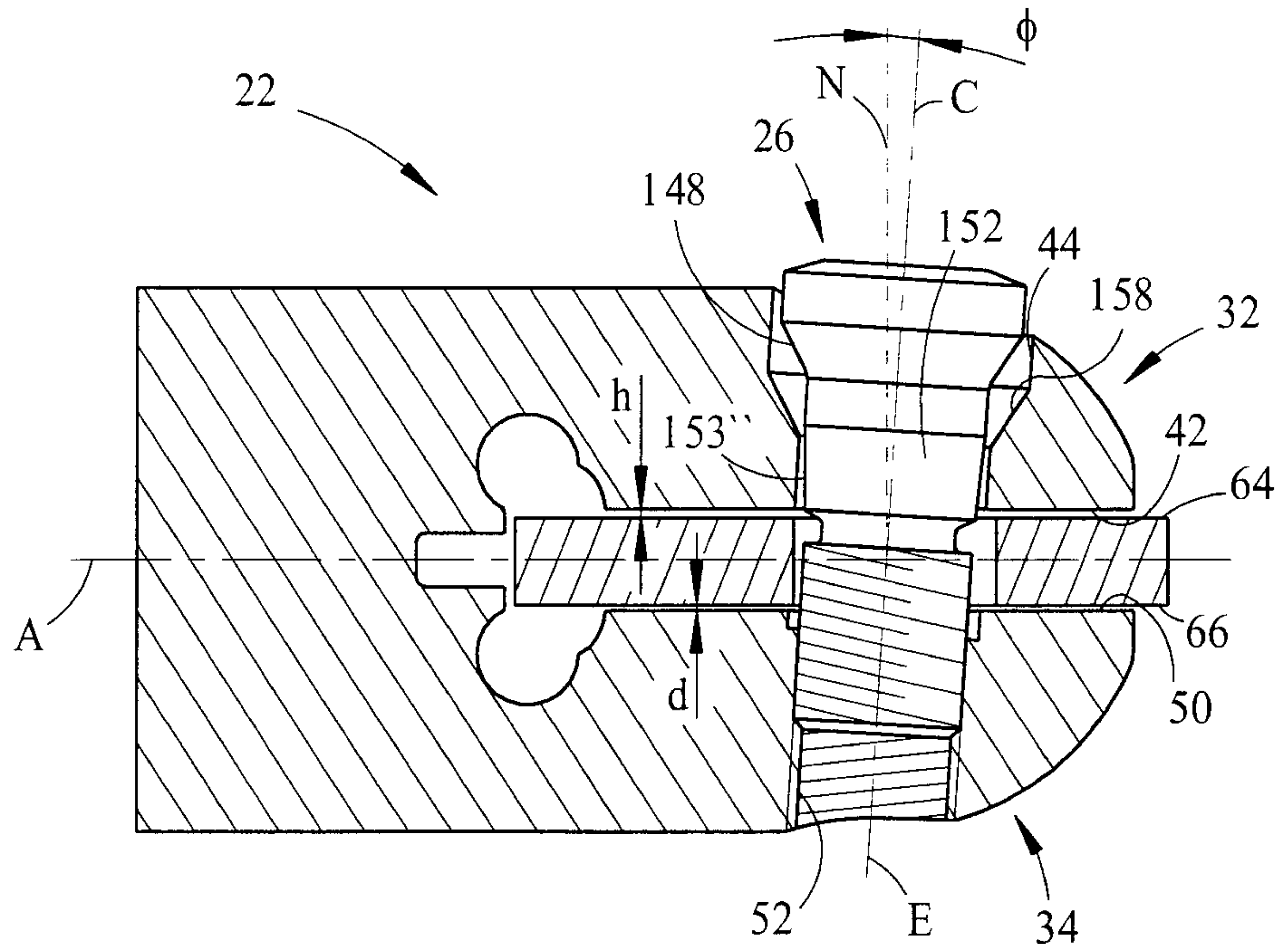


Fig. 12

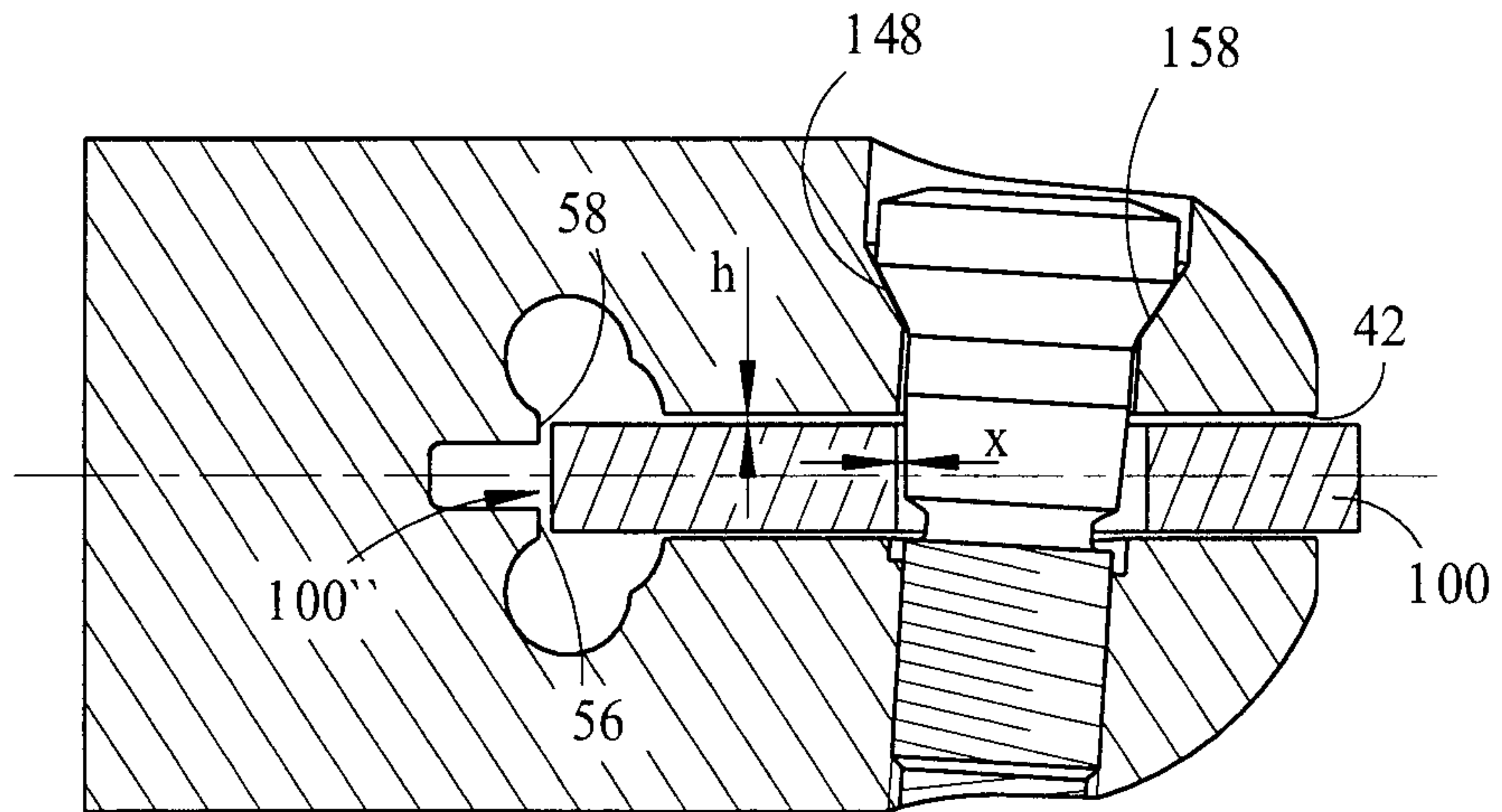


Fig. 13

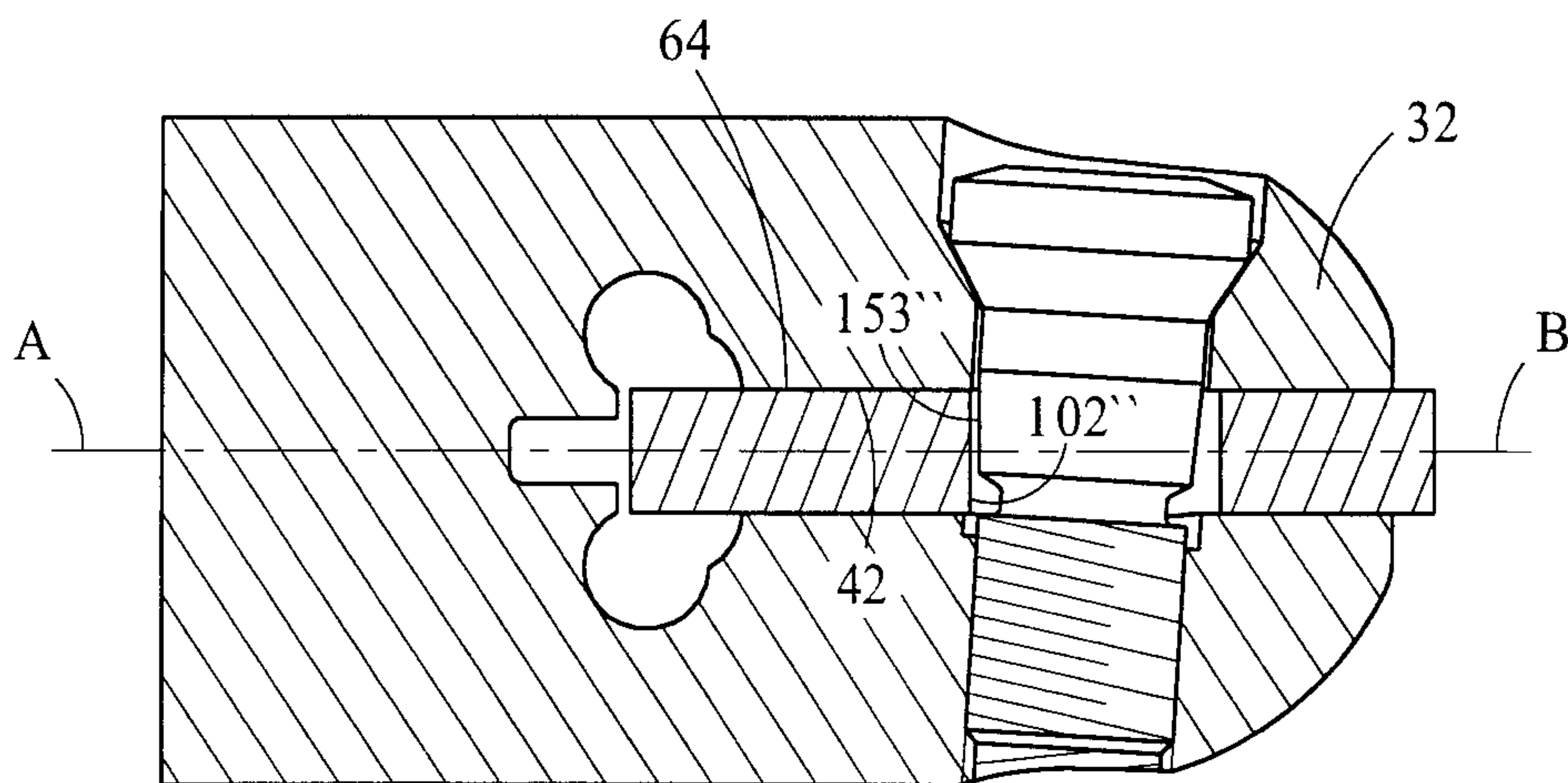
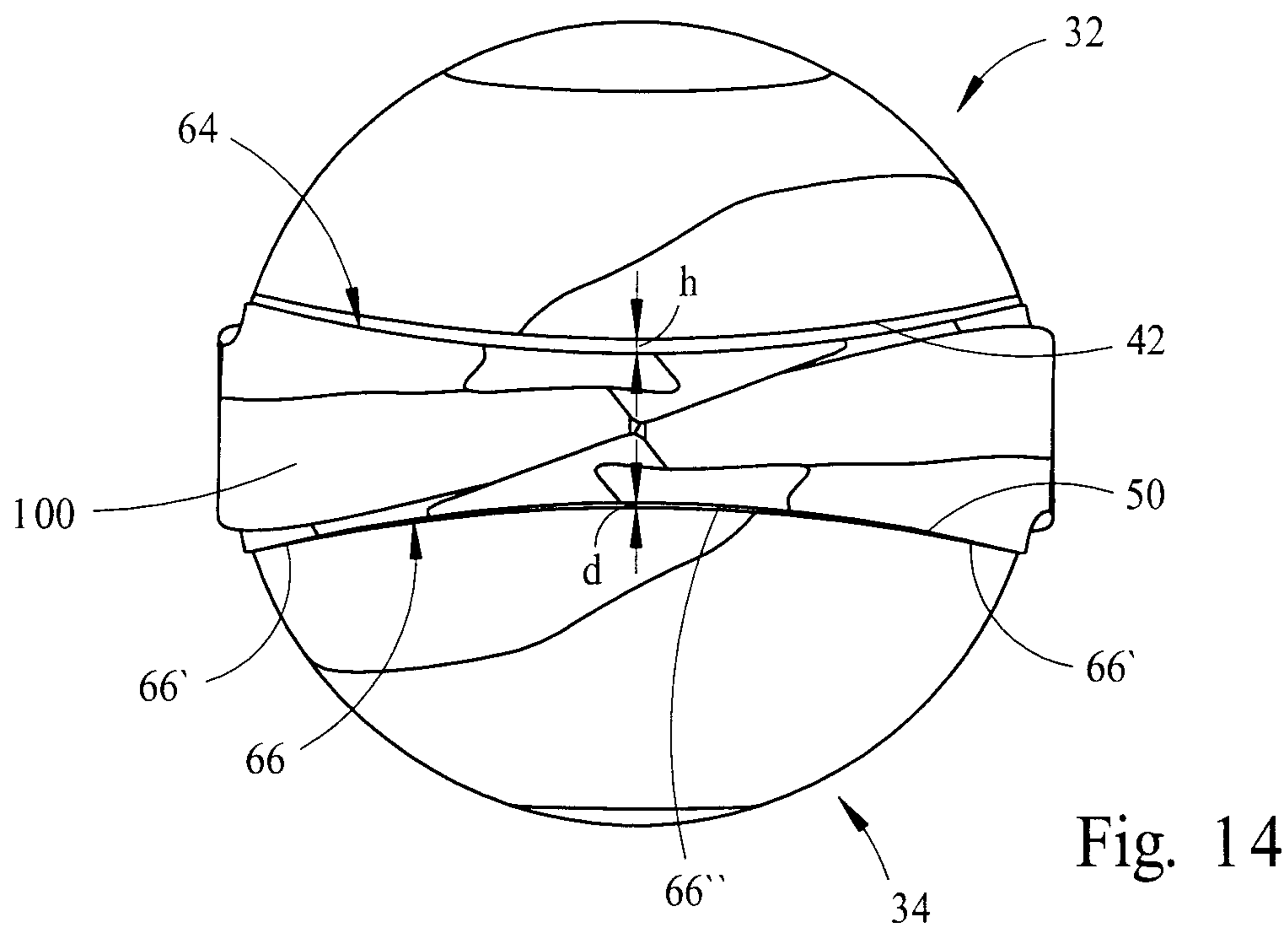


Fig. 15

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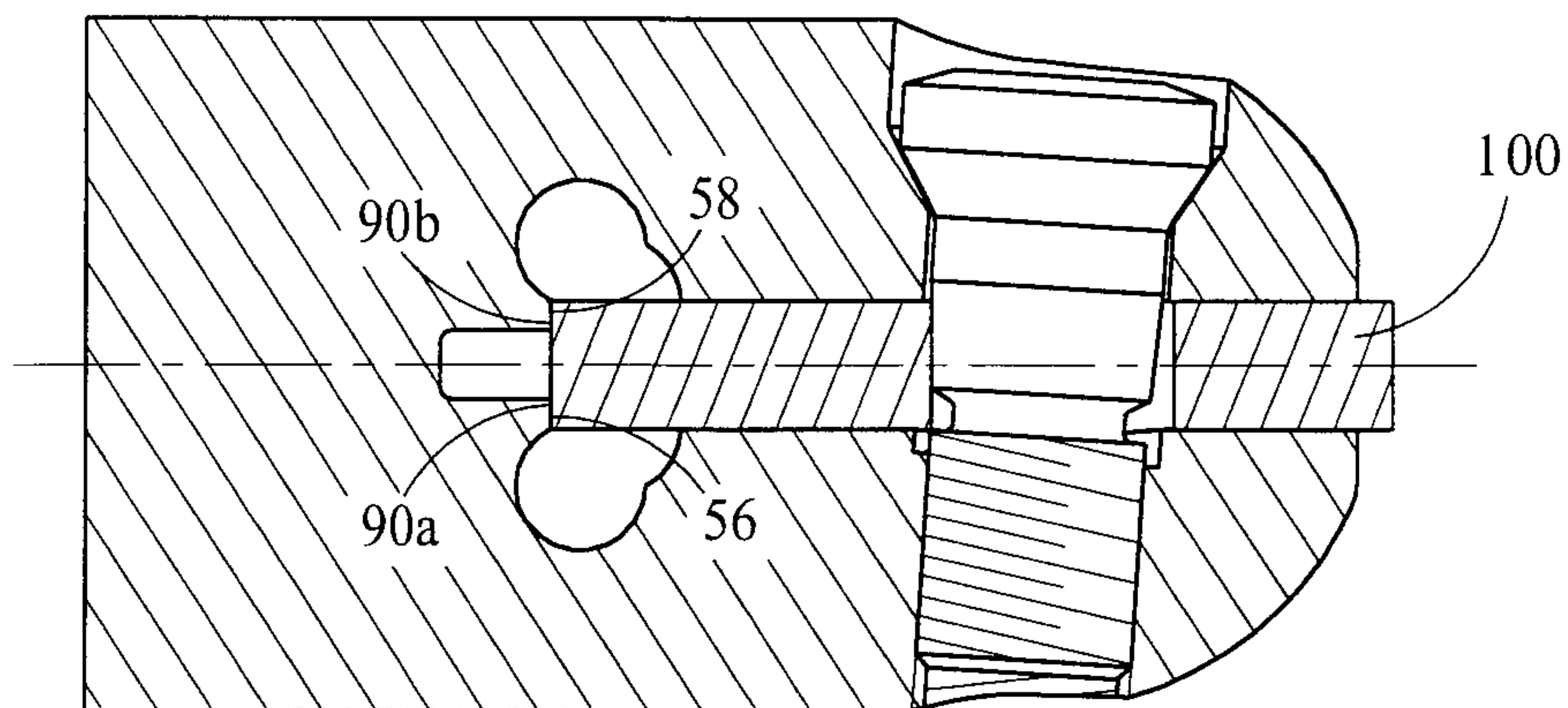


Fig. 16

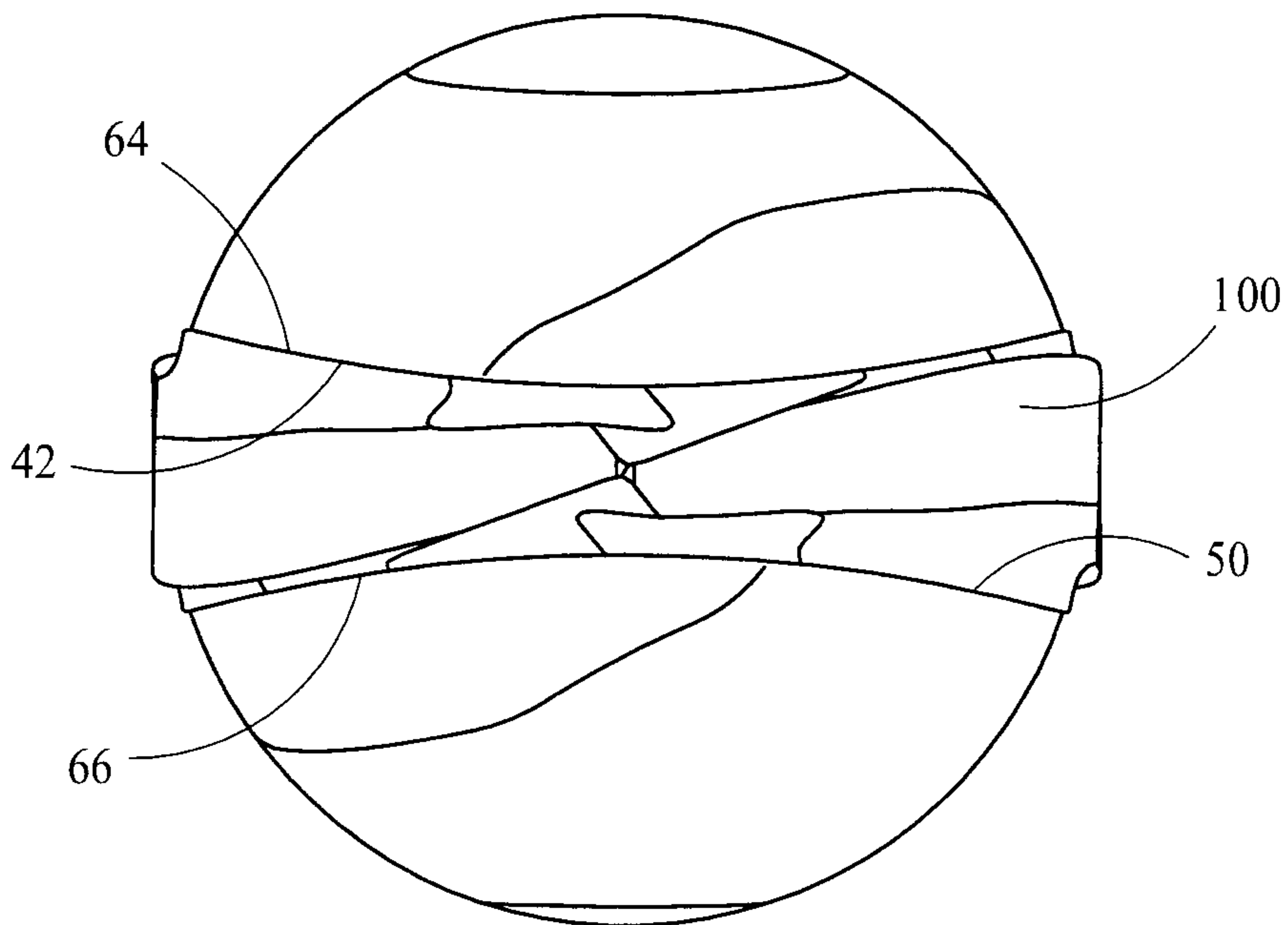


Fig. 17

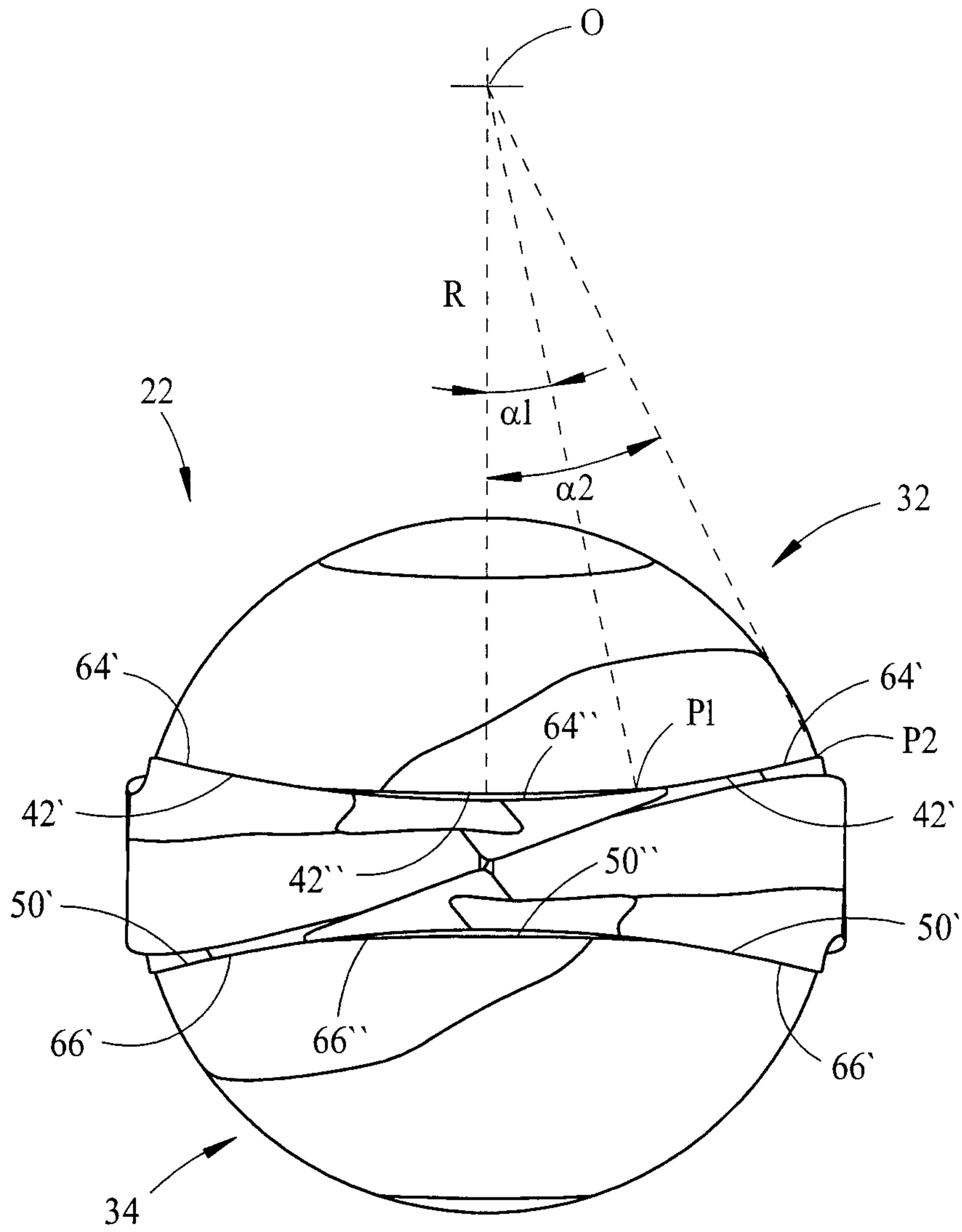


Fig. 18

