

(19)



(11)

EP 4 299 626 A1

(12)

EUROPEAN PATENT APPLICATION
published in accordance with Art. 153(4) EPC

(43) Date of publication:

03.01.2024 Bulletin 2024/01

(51) International Patent Classification (IPC):

C08F 8/20 ^(2006.01) **C08F 214/26** ^(2006.01)
H01B 7/02 ^(2006.01) **C08J 7/12** ^(2006.01)

(21) Application number: **22759859.6**

(52) Cooperative Patent Classification (CPC):

C08F 8/20; C08F 214/26; C08J 5/18; C08J 7/12;
H01B 7/02

(22) Date of filing: **28.02.2022**

(86) International application number:

PCT/JP2022/008442

(87) International publication number:

WO 2022/181826 (01.09.2022 Gazette 2022/35)

(84) Designated Contracting States:

AL AT BE BG CH CY CZ DE DK EE ES FI FR GB
GR HR HU IE IS IT LI LT LU LV MC MK MT NL NO
PL PT RO RS SE SI SK SM TR

Designated Extension States:

BA ME

Designated Validation States:

KH MA MD TN

(72) Inventors:

- **ISAKA, Tadaharu**
Osaka-shi, Osaka 530-0001 (JP)
- **YAMAMOTO, Yukari**
Osaka-shi, Osaka 530-0001 (JP)
- **ZENKE, Yumi**
Osaka-shi, Osaka 530-0001 (JP)

(30) Priority: **26.02.2021 JP 2021031103**

(74) Representative: **Hoffmann Eitle**

Patent- und Rechtsanwälte PartmbB
Arabellastraße 30
81925 München (DE)

(71) Applicant: **DAIKIN INDUSTRIES, LTD.**
Osaka 530-0001 (JP)

(54) **FLUORINE-CONTAINING COPOLYMER**

(57) There is provided a fluorine-containing copolymer comprising tetrafluoroethylene unit, hexafluoropropylene unit, and a perfluoro(propyl vinyl ether) unit, wherein the copolymer has a content of the hexafluoropropylene unit of 3.55 to 4.10% by mol with respect to

the whole of the monomer units, a content of the perfluoro(propyl vinyl ether) unit of 0.39 to 0.90% by mol with respect to the whole of the monomer units, and a melt flow rate at 372°C of 1.0 to 9.0 g/10 min.

EP 4 299 626 A1

Description

TECHNICAL FIELD

5 **[0001]** The present disclosure relates to a fluorine-containing copolymer.

BACKGROUND ART

10 **[0002]** Patent Literature 1 describes a terpolymer containing (a) tetrafluoroethylene, (b) hexafluoropropylene in an amount of about 4 to about 12% by weight based on the weight of the terpolymer, and (c) perfluoro(ethyl vinyl ether) or perfluoro(n-propyl vinyl ether) in an amount of about 0.5 to about 3% by weight based on the weight of the terpolymer, in a copolymerized form.

RELATED ART

15

PATENT LITERATURE

[0003] Patent Literature 1: Japanese Patent Laid-Open No. 52-109588

20 SUMMARY OF THE INVENTION

PROBLEM TO BE SOLVED BY THE INVENTION

25 **[0004]** An object of the present disclosure is to provide a fluorine-containing copolymer which can form a very thick coating layer in a uniform thickness on a core wire very large in diameter, can give a beautiful tube, can be formed at a high forming speed into thin films uniform in thickness, is unlikely to deform even in a melt state and can give a formed article excellent in the 50°C abrasion resistance, the heat aging resistance, the low hydrogen permeation, the 100°C high-temperature rigidity, the 140°C tensile creep resistance and the durability to repeated loads.

30 MEANS FOR SOLVING THE PROBLEM

[0005] According to the present disclosure, there is provided a fluorine-containing copolymer comprising tetrafluoroethylene unit, hexafluoropropylene unit and perfluoro(propyl vinyl ether) unit, wherein the copolymer has a content of hexafluoropropylene unit of 3.55 to 4.10% by mol with respect to the whole of the monomer units, a content of perfluoro(propyl vinyl ether) unit of 0.39 to 0.90% by mol with respect to the whole of the monomer units, and a melt flow rate at 372°C of 1.0 to 9.0 g/10 min.

[0006] It is preferable that the content of hexafluoropropylene unit is 3.55 to 3.92% by mol with respect to the whole of the monomer units.

40 **[0007]** It is preferable that the content of perfluoro(propyl vinyl ether) unit is 0.46 to 0.85% by mol with respect to the whole of the monomer units.

[0008] It is preferable that the melt flow rate at 372°C is 2.0 to 8.0 g/10 min.

[0009] It is preferable that the number of functional groups is 90 or less per 10⁶ main-chain carbon atoms.

[0010] Then, according to the present disclosure, there is provided an injection molded article, an extrusion formed article or a transfer molded article comprising the above fluorine-containing copolymer.

45 **[0011]** Further, according to the present disclosure, there is provided a coated electric wire comprising a coating layer comprising the above fluorine-containing copolymer.

[0012] Further, according to the present disclosure, there is provided a formed article comprising the above fluorine-containing copolymer, wherein the formed article is a tube, a film or an electric wire coating.

50 EFFECT OF INVENTION

[0013] According to the present disclosure, there can be provided a fluorine-containing copolymer which can form a very thick coating layer in a uniform thickness on a core wire very large in diameter, can give a beautiful tube, can be formed at a high forming speed into thin films uniform in thickness, is unlikely to deform even in a melt state and can give a formed article excellent in the 50°C abrasion resistance, the heat aging resistance, the low hydrogen permeation, the 100°C high-temperature rigidity, the 140°C tensile creep resistance and the durability to repeated loads.

DESCRIPTION OF EMBODIMENTS

[0014] Hereinafter, specific embodiments of the present disclosure will be described in detail, but the present disclosure is not limited to the following embodiments.

[0015] A fluorine-containing copolymer of the present disclosure comprises tetrafluoroethylene (TFE) unit, hexafluoropropylene (HFP) unit and perfluoro(propyl vinyl ether) (PPVE) unit.

[0016] As fluororesins, non melt-processible fluororesins such as polytetrafluoroethylene (PTFE), and melt-fabricable fluororesins are known. PTFE, though having excellent properties, has such a drawback that the melt processing is remarkably difficult. Meanwhile, as the melt-fabricable fluororesins, TFE/HFP copolymers (FEP), TFE/PPVE copolymers (PFA) and the like are known; however, these have a drawback of being inferior in the heat resistance and the like to PTFE. Then, Patent Literature 1 proposes the above-mentioned terpolymer as a fluorocarbon polymer improved in these drawbacks.

[0017] For tubes for making chemical solutions to flow through, it is demanded that the tubes have a uniform cross-sectional shape in order to make chemical solutions to smoothly flow through, and there are also demanded the abrasion resistance not causing abrasion even in flowing chemical solutions, the heat aging resistance not causing cracks even in a high-temperature environment, the low gas permeation not allowing gases such as hydrogen to permeate, the high-temperature rigidity and tensile creep resistance not causing deformation even in flowing high-temperature chemical solutions, the durability to repeated loads not exhibiting deterioration even in frequent changes in the pressure of chemical solutions, and the like. It is the present situation, however, that no fluororesins well balancedly meeting these demands are known.

[0018] It has been found that by regulating, in very limited ranges, the contents of HFP unit and PPVE unit of the fluorine-containing copolymer containing TFE unit, HFP unit and PPVE unit, and the melt flow rate, the fluorine-containing copolymer becomes one having high formability capable of being easily formed into tubes and can give formed articles excellent in the 50°C abrasion resistance, the heat aging resistance, the low hydrogen permeation, the 100°C high-temperature rigidity, the 140°C tensile creep resistance and the durability to repeated loads.

[0019] Moreover, by forming the fluorine-containing copolymer of the present disclosure by an extrusion forming method, a very thick coating layer can be formed in a uniform thickness on a core wire very large in diameter, and the fluorine-containing copolymer can be formed at a high forming speed into thin films uniform in thickness.

[0020] Further, since the fluorine-containing copolymer of the present disclosure causes little own weight deformation even in a melt state, thick pipes made of the copolymer have clear cross-sections and uniform thicknesses.

[0021] The fluorine-containing copolymer of the present disclosure is a melt-fabricable fluororesin. Being melt-fabricable means that a polymer can be melted and processed by using a conventional processing device such as an extruder or an injection molding machine.

[0022] The content of the HFP unit of the fluorine-containing copolymer is, with respect to the whole of the monomer units, 3.55 to 4.10% by mol, and preferably 3.56% by mol or higher, more preferably 3.57% by mol or higher and still more preferably 3.58% by mol or higher, and preferably 4.09% by mol or lower, more preferably 4.05% by mol or lower, still more preferably 4.00% by mol or lower, especially preferably 3.95% by mol or lower and most preferably 3.92% by mol or lower. When the content of the HFP unit is too low, formed articles excellent in the 50°C abrasion resistance and the heat aging resistance cannot be obtained; and when the content of the HFP unit is too high, formed articles excellent in the low hydrogen permeation, the 100°C high-temperature rigidity, the 140°C tensile creep resistance and the durability to repeated loads cannot be obtained.

[0023] The content of the PPVE unit of the fluorine-containing copolymer is, with respect to the whole of the monomer units, 0.39 to 0.90% by mol, and preferably 0.43% by mol or higher, more preferably 0.46% by mol or higher, still more preferably 0.52% by mol or higher, especially preferably 0.55% by mol or higher and most preferably 0.58% by mol or higher, and more preferably 0.87% by mol or lower, still more preferably 0.85% by mol or lower, especially preferably 0.80% by mol or lower and most preferably 0.77% by mol or lower. When the content of the PPVE unit is too low, formed articles excellent in the 50°C abrasion resistance and the heat aging resistance cannot be obtained. When the content of the PPVE unit is too high, formed articles excellent in the low hydrogen permeation and the 100°C high-temperature rigidity cannot be obtained.

[0024] The content of the TFE unit of the fluorine-containing copolymer is, with respect to the whole of the monomer units, preferably 95.00 to 96.06% by mol, and more preferably 95.08% by mol or higher, still more preferably 95.15% by mol or higher, further still more preferably 95.25% by mol or higher and especially preferably 95.31% by mol or higher, and more preferably 96.01% by mol or lower, still more preferably 95.97% by mol or lower, further still more preferably 95.90% by mol or lower, especially preferably 99.45% by mol or lower and most preferably 99.42% by mol or lower. Then, the content of the TFE unit may be selected so that the total of contents of the HFP unit, the PPVE unit, the TFE unit and other monomer units becomes 100% by mol.

[0025] The fluorine-containing copolymer of the present disclosure is not limited as long as the copolymer contains the above three monomer units, and may be a copolymer containing only the above three monomer units, or may be a

copolymer containing the above three monomer units and other monomer units.

[0026] The other monomers are not limited as long as being copolymerizable with TFE, HFP and PPVE, and may be fluoromonomers or fluorine-non-containing monomers.

[0027] It is preferable that the fluoromonomer is at least one selected from the group consisting of chlorotrifluoroethylene, vinyl fluoride, vinylidene fluoride, trifluoroethylene, hexafluoroisobutylene, monomers represented by $\text{CH}_2=\text{CZ}^1(\text{CF}_2)_n\text{Z}^2$ (wherein Z^1 is H or F, Z^2 is H, F or Cl, and n is an integer of 1 to 10), perfluoro(alkyl vinyl ether)s [PAVE] represented by $\text{CF}_2=\text{CF}-\text{ORf}^1$ (wherein Rf^1 is a perfluoroalkyl group having 1 to 8 carbon atoms)(here, excluding PPVE), alkyl perfluorovinyl ether derivatives represented by $\text{CF}_2=\text{CF}-\text{O}-\text{CH}_2-\text{Rf}^2$ (wherein Rf^2 is a perfluoroalkyl group having 1 to 5 carbon atoms), perfluoro-2,2-dimethyl-1,3-dioxol [PDD], and perfluoro-2-methylene-4-methyl-1,3-dioxolane [PMD].

[0028] The monomers represented by $\text{CH}_2=\text{CZ}^1(\text{CF}_2)_n\text{Z}^2$ include $\text{CH}_2=\text{CFCF}_3$, $\text{CH}_2=\text{CH}-\text{C}_4\text{F}_9$, $\text{CH}_2=\text{CH}-\text{C}_6\text{F}_{13}$, and $\text{CH}_2=\text{CF}-\text{C}_3\text{F}_6\text{H}$.

[0029] The perfluoro(alkyl vinyl ether)s represented by $\text{CF}_2=\text{CF}-\text{ORf}^1$ include $\text{CF}_2=\text{CF}-\text{OCF}_3$ and $\text{CF}_2=\text{CF}-\text{OCF}_2\text{CF}_3$.

[0030] The fluorine-non-containing monomers include hydrocarbon-based monomers copolymerizable with TFE, HFP and PPVE. Examples of the hydrocarbon-based monomers include alkenes such as ethylene, propylene, butylene, and isobutylene; alkyl vinyl ethers such as ethyl vinyl ether, propyl vinyl ether, butyl vinyl ether, isobutyl vinyl ether, and cyclohexyl vinyl ether; vinyl esters such as vinyl acetate, vinyl propionate, n-vinyl butyrate, vinyl isobutyrate, vinyl valerate, vinyl pivalate, vinyl caproate, vinyl caprylate, vinyl caprate, vinyl versatate, vinyl laurate, vinyl myristate, vinyl palmitate, vinyl stearate, vinyl benzoate, vinyl para-t-butylbenzoate, vinyl cyclohexanecarboxylate, vinyl monochloroacetate, vinyl adipate, vinyl acrylate, vinyl methacrylate, vinyl crotonate, vinyl sorbate, vinyl cinnamate, vinyl undecylenate, vinyl hydroxyacetate, vinyl hydroxypropionate, vinyl hydroxybutyrate, vinyl hydroxyvalerate, vinyl hydroxyisobutyrate, and vinyl hydroxycyclohexanecarboxylate; alkyl allyl ethers such as ethyl allyl ether, propyl allyl ether, butyl allyl ether, isobutyl allyl ether, and cyclohexyl allyl ether; and alkyl allyl esters such as ethyl allyl ester, propyl allyl ester, butyl allyl ester, isobutyl allyl ester, and cyclohexyl allyl ester.

[0031] The fluorine-non-containing monomers may also be functional group-containing hydrocarbon-based monomers copolymerizable with TFE, HFP and PPVE. Examples of the functional group-containing hydrocarbon-based monomers include hydroxyalkyl vinyl ethers such as hydroxyethyl vinyl ether, hydroxypropyl vinyl ether, hydroxybutyl vinyl ether, hydroxyisobutyl vinyl ether, and hydroxycyclohexyl vinyl ether; fluorine-non-containing monomers having a glycidyl group, such as glycidyl vinyl ether and glycidyl allyl ether; fluorine-non-containing monomers having an amino group, such as aminoalkyl vinyl ethers and aminoalkyl allyl ethers; fluorine-non-containing monomers having an amido group, such as (meth)acrylamide and methylolacrylamide; bromine-containing olefins, iodine-containing olefins, bromine-containing vinyl ethers, and iodine-containing vinyl ethers; and fluorine-non-containing monomers having a nitrile group.

[0032] The content of the other monomer units in the fluorine-containing copolymer of the present disclosure is, with respect to the whole of the monomer units, preferably 0 to 1.06% by mol, and more preferably 1.0% by mol or lower, still more preferably 0.5% by mol or lower and especially preferably 0.1% by mol or lower.

[0033] The melt flow rate (MFR) of the fluorine-containing copolymer is 1.0 to 9.0 g/10 min, and preferably 1.2 g/10 min or higher, more preferably 1.5 g/10 min or higher, still more preferably 2.0 g/10 min or higher, further still more preferably 3.0 g/10 min or higher, further still more preferably 4.0 g/10 min or higher, especially preferably 4.5 g/10 min or higher and most preferably 5.0 g/10 min or higher, and preferably 8.9 g/10 min or lower, more preferably 8.5 g/10 min or lower, still more preferably 8.0 g/10 min or lower, further still more preferably 7.0 g/10 min or lower, further still more preferably 6.0 g/10 min or lower, especially preferably 5.5 g/10 min or lower and most preferably 5.0 g/10 min or lower. Due to that the MFR of the fluorine-containing copolymer is in the above range, the formability of the copolymer is improved and formed articles excellent in the 50°C abrasion resistance, the heat aging resistance, the low hydrogen permeation, the 100°C high-temperature rigidity, the 140°C tensile creep resistance and the durability to repeated loads can be obtained. Further, due to that the MFR of the fluorine-containing copolymer is in the above range, the fluorine-containing copolymer causes relatively little own weight deformation in a melt state.

[0034] In the present disclosure, the MFR is a value obtained as a mass (g/10 min) of a polymer flowing out from a die of 2 mm in inner diameter and 8 mm in length per 10 min at 372°C under a load of 5 kg using a melt indexer G-01 (manufactured by Toyo Seiki Seisaku-sho Ltd.), according to ASTM D1238.

[0035] The MFR can be regulated by regulating the kind and amount of a polymerization initiator to be used in polymerization of monomers, the kind and amount of a chain transfer agent, and the like.

[0036] The fluorine-containing copolymer of the present disclosure may or may not have functional groups. The functional groups are functional groups present on the main chain terminals or side chain terminals of the fluorine-containing copolymer, and functional groups present on the main chain or side chains thereof. Typical functional groups are $-\text{CF}=\text{CF}_2$, $-\text{CF}_2\text{H}$, $-\text{COF}$, $-\text{COOH}$, $-\text{COOCH}_3$, $-\text{CONH}_2$ and $-\text{CH}_2\text{OH}$.

[0037] The number of functional groups per 10^6 main-chain carbon atoms of the fluorine-containing copolymer is preferably 90 or less, more preferably 70 or less, still more preferably 50 or less, further still more preferably 40 or lower, further still more preferably 30 or less, especially preferably 20 or less and most preferably less than 15. Due to that the

number of functional groups of the fluorine-containing copolymer is in the above range, formed articles hardly making fluorine ions to dissolve out in chemical solutions such as a hydrogen peroxide aqueous solution can be obtained.

[0038] The number of functional groups of the fluorine-containing copolymer is the total number of $-\text{CF}=\text{CF}_2$, $-\text{CF}_2\text{H}$, $-\text{COF}$, $-\text{COOH}$, $-\text{COOCH}_3$, $-\text{CONH}_2$ and $-\text{CH}_2\text{OH}$.

[0039] The number of $-\text{CF}_2\text{H}$ per 10^6 main-chain carbon atoms of the fluorine-containing copolymer is preferably 50 or less, more preferably 40 or less, still more preferably 30 or less, further still more preferably 20 or less, especially preferably less than 15 and most preferably 10 or less.

[0040] The total number, per 10^6 main-chain carbon atoms, of $-\text{COOH}$, $-\text{COOCH}_3$, $-\text{CH}_2\text{OH}$, $-\text{COF}$, $-\text{CF}=\text{CF}_2$ and $-\text{CONH}_2$ of the fluorine-containing copolymer is preferably 80 or less, more preferably 70 or less, still more preferably 50 or less, further still more preferably 40 or less, further still more preferably 30 or less, especially preferably 20 or less and most preferably less than 15.

[0041] For identification of the kind of the functional groups and measurement of the number of the functional groups, infrared spectroscopy can be used.

[0042] The number of the functional groups is measured, specifically, by the following method. First, the fluorine-containing copolymer is molded by cold press to prepare a film of 0.25 to 0.30 mm in thickness. The film is analyzed by Fourier transform infrared spectroscopy to obtain an infrared absorption spectrum, and a difference spectrum against a base spectrum that is completely fluorinated and has no functional groups is obtained. From an absorption peak of a specific functional group observed on this difference spectrum, the number N of the functional group per 1×10^6 carbon atoms in the fluorine-containing copolymer is calculated according to the following formula (A).

$$N = I \times K/t \dots (A)$$

I: absorbance

K: correction factor

t: thickness of film (mm)

[0043] For reference, for some functional groups, the absorption frequency, the molar absorption coefficient and the correction factor are shown in Table 1. Then, the molar absorption coefficients are those determined from FT-IR measurement data of low molecular model compounds.

[Table 1]

[0044]

Table 1

Functional Group	Absorption Frequency (cm ⁻¹)	Molar Extinction Coefficient (l/cm/mol)	Correction Factor	Model Compound
-COF	1883	600	388	C ₇ F ₁₅ COF
-COOH free	1815	530	439	H(CF ₂) ₆ COOH
-COOH bonded	1779	530	439	H(CF ₂) ₆ COOH
-COOCH ₃	1795	680	342	C ₇ F ₁₅ COOCH ₃
-CONH ₂	3436	506	460	C ₇ H ₁₅ CONH ₂
-CH ₂ OH ₂ , -OH	3648	104	2236	C ₇ H ₁₅ CH ₂ OH
-CF ₂ H	3020	8.8	26485	H(CF ₂ CF ₂) ₃ CH ₂ OH
-CF=CF ₂	1795	635	366	CF ₂ =CF ₂

[0045] Absorption frequencies of $-\text{CH}_2\text{CF}_2\text{H}$, $-\text{CH}_2\text{COF}$, $-\text{CH}_2\text{COOH}$, $-\text{CH}_2\text{COOCH}_3$ and $-\text{CH}_2\text{CONH}_2$ are lower by a few tens of kaysers (cm⁻¹) than those of $-\text{CF}_2\text{H}$, $-\text{COF}$, $-\text{COOH}$ free and $-\text{COOH}$ bonded, $-\text{COOCH}_3$ and $-\text{CONH}_2$ shown in the Table, respectively.

[0046] For example, the number of the functional group $-\text{COF}$ is the total of the number of a functional group determined from an absorption peak having an absorption frequency of 1,883 cm⁻¹ derived from $-\text{CF}_2\text{COF}$ and the number of a

functional group determined from an absorption peak having an absorption frequency of $1,840\text{ cm}^{-1}$ derived from $-\text{CH}_2\text{COF}$.

[0047] The number of $-\text{CF}_2\text{H}$ groups can also be determined from a peak integrated value of the $-\text{CF}_2\text{H}$ group acquired in a ^{19}F -NMR measurement using a nuclear magnetic resonance spectrometer and set at a measurement temperature of (the melting point of a polymer + 20) $^\circ\text{C}$.

[0048] Functional groups are functional groups present on the main chain terminals or side chain terminals of the fluorine-containing copolymer, and functional groups present on the main chain or the side chains thereof. The number of functional groups may be the total number of $-\text{CF}=\text{CF}_2$, $-\text{CF}_2\text{H}$, $-\text{COF}$, $-\text{COOH}$, $-\text{COOCH}_3$, $-\text{CONH}_2$ and $-\text{CH}_2\text{OH}$.

[0049] The functional groups are introduced to the fluorine-containing copolymer, for example, by a chain transfer agent or a polymerization initiator used in production of the fluorine-containing copolymer. For example, in the case of using an alcohol as the chain transfer agent, or a peroxide having a structure of $-\text{CH}_2\text{OH}$ as the polymerization initiator, $-\text{CH}_2\text{OH}$ is introduced on the main chain terminals of the fluorine-containing copolymer. Alternatively, the functional group is introduced on the side chain terminal of the fluorine-containing copolymer by polymerizing a monomer having the functional group.

[0050] By carrying out a treatment such as a wet heat treatment or a fluorination treatment on the fluorine-containing copolymer having such functional groups, there can be obtained the fluorine-containing copolymer having the number of functional groups in the above range. The fluorine-containing copolymer of the present disclosure is preferably one having been subjected to a wet heat treatment or a fluorination treatment, and more preferably one having been subjected to a fluorination treatment. It is also preferable that the fluorine-containing copolymer of the present disclosure has a $-\text{CF}_3$ terminal group.

[0051] The melting point of the fluorine-containing copolymer is preferably 260 to 290°C and more preferably 273 to 290°C . Due to that the melting point is in the above range, the formability of the copolymer is more improved; the copolymer is more unlikely to deform even in a melt state; and formed articles better in the 50°C abrasion resistance, the heat aging resistance, the low hydrogen permeation, the 100°C high-temperature rigidity, the 140°C tensile creep resistance and the durability to repeated loads can be obtained.

[0052] In the present disclosure, the melting point can be measured by using a differential scanning calorimeter [DSC].

[0053] The hydrogen permeation coefficient of the fluorine-containing copolymer is preferably $1900\text{ cm}^3\cdot\text{mm}/(\text{m}^2\cdot 24\text{h}\cdot\text{atm})$ or lower. The fluorine-containing copolymer of the present disclosure has an excellent low hydrogen permeation due to suitably regulated contents of the HFP unit and the PPVE unit, and melt flow rate (MFR).

[0054] In the present disclosure, the hydrogen permeation coefficient can be measured under the condition of a test temperature of 60°C and a test humidity of $0\%\text{RH}$. The specific measurement of the hydrogen permeation coefficient can be carried out by a method described in Examples.

[0055] In the fluorine-containing copolymer of the present disclosure, the amount of fluorine ions dissolving out therefrom detected by an immersion test in a hydrogen peroxide aqueous solution is, in terms of mass, preferably 4.0 ppm or lower, more preferably 3.0 ppm or lower and still more preferably 2.8 ppm or lower.

[0056] In the present disclosure, the immersion test in a hydrogen peroxide aqueous solution can be carried out by using the fluorine-containing copolymer and preparing a test piece having a weight corresponding to that of 10 sheets of a formed article ($15\text{ mm} \times 15\text{ mm} \times 0.2\text{ mm}$), and putting, in a thermostatic chamber of 95°C , a polypropylene-made bottle in which the test piece and 15 g of a $3\text{-mass}\%$ hydrogen peroxide aqueous solution are put and allowing the resultant to stand for 20 hours.

[0057] The fluorine-containing copolymer of the present disclosure can be produced by any polymerization method of bulk polymerization, suspension polymerization, solution polymerization, emulsion polymerization and the like. In these polymerization methods, conditions such as temperature and pressure, a polymerization initiator, a chain transfer agent, a solvent and other additives can suitably be set depending on the composition and the amount of a desired fluorine-containing copolymer.

[0058] The polymerization initiator may be an oil-soluble radical polymerization initiator or a water-soluble radical initiator.

[0059] An oil-soluble radical polymerization initiator may be a known oil-soluble peroxide, and examples thereof typically include:

dialkyl peroxycarbonates such as di-n-propyl peroxydicarbonate, diisopropyl peroxydicarbonate, di-sec-butyl peroxydicarbonate;

peroxyesters such as t-butyl peroxyisobutyrate and t-butyl peroxyvalerate;

dialkyl peroxides such as di-t-butyl peroxide; and

di[fluoro(or fluorochloro)acyl] peroxides.

[0060] The di[fluoro(or fluorochloro)acyl] peroxides include diacyl peroxides represented by $[(\text{RfCOO})_2]$ wherein Rf is a perfluoroalkyl group, an ω -hydroperfluoroalkyl group or a fluorochloroalkyl group.

[0061] Examples of the di[fluoro(or fluorochloro)acyl] peroxides include di(ω -hydro-dodecafluorohexanoyl) peroxide, di(ω -hydro-tetradecafluoroheptanoyl) peroxide, di(ω -hydro-hexadecafluorononanoyl) peroxide, di(perfluorobutyryl) peroxide, di(perfluorovaleryl) peroxide, di(perfluoroheptanoyl) peroxide, di(perfluoroheptanoyl) peroxide, di(perfluorooctanoyl) peroxide, di(perfluorononanoyl) peroxide, di(ω -chloro-hexafluorobutyryl) peroxide, di(ω -chloro-decafluoro-hexanoyl) peroxide, di(ω -chloro-tetradecafluorooctanoyl) peroxide, ω -hydrodo-decafluoroheptanoyl- ω -hydrohexadecafluorononanoyl peroxide, ω -chloro-hexafluorobutyryl- ω -chloro-decafluoroheptanoyl peroxide, ω -hydrododecafluoroheptanoyl-perfluorobutyryl peroxide, di(dichloropentafluorobutanoyl) peroxide, di(trichlorooctafluorohexanoyl) peroxide, di(tetrachloroundecafluorooctanoyl) peroxide, di(pentachlorotetradecafluorodecanoyl) peroxide and di(undecachlorotri-acontfluorodocosanoyl) peroxide.

[0062] The water-soluble radical polymerization initiator may be a well known water-soluble peroxide, and examples thereof include ammonium salts, potassium salts and sodium salts of persulfuric acid, perboric acid, perchloric acid, perphosphoric acid, percarbonic acid and the like, and t-butyl permaleate and t-butyl hydroperoxide. A reductant such as a sulfite salt may be combined with a peroxide and used, and the amount thereof to be used may be 0.1 to 20 times with respect to the peroxide.

[0063] Examples of the chain transfer agent include hydrocarbons such as ethane, isopentane, n-hexane and cyclohexane; aromatics such as toluene and xylene; ketones such as acetone; acetates such as ethyl acetate and butyl acetate; alcohols such as methanol, ethanol and 2,2,2-trifluoroethanol; mercaptans such as methyl mercaptan; halogenated hydrocarbons such as carbon tetrachloride, chloroform, methylene chloride and methyl chloride; and 3-fluorobenzotrifluoride. The amount thereof to be added can vary depending on the magnitude of the chain transfer constant of a compound to be used, but the chain transfer agent is used usually in the range of 0.01 to 20 parts by mass with respect to 100 parts by mass of a solvent.

[0064] For example, in the cases of using a dialkyl peroxy carbonate, a di[fluoro(or fluorochloro)acyl] peroxide or the like as a polymerization initiator, although there are some cases where the molecular weight of an obtained fluorine-containing copolymer becomes too high and the regulation of the melt flow rate to a desired one is not easy, the molecular weight can be regulated by using the chain transfer agent. It is especially suitable that the fluorine-containing copolymer is produced by suspension polymerization using the chain transfer agent such as an alcohol and the oil-soluble radical polymerization initiator.

[0065] The solvent includes water and mixed solvents of water and an alcohol. A monomer to be used for the polymerization of the fluorine-containing copolymer of the present disclosure can also be used as the solvent.

[0066] In the suspension polymerization, in addition to water, a fluorosolvent may be used. The fluorosolvent may include hydrochlorofluoroalkanes such as CH_3CClF_2 , $\text{CH}_3\text{CCl}_2\text{F}$, $\text{CF}_3\text{CF}_2\text{CCl}_2\text{H}$ and $\text{CF}_2\text{ClCF}_2\text{CFHCl}$; chlorofluoroalkanes such as $\text{CF}_2\text{ClCFClCF}_2\text{CF}_3$ and $\text{CF}_3\text{CFClCFClCF}_3$; and perfluoroalkanes such as perfluorocyclobutane, $\text{CF}_3\text{CF}_2\text{CF}_2\text{CF}_3$, $\text{CF}_3\text{CF}_2\text{CF}_2\text{CF}_2\text{CF}_3$ and $\text{CF}_3\text{CF}_2\text{CF}_2\text{CF}_2\text{CF}_2\text{CF}_3$, and among these, perfluoroalkanes are preferred. The amount of the fluorosolvent to be used is, from the viewpoint of the suspensibility and the economic efficiency, preferably 10 to 100 parts by mass with respect to 100 parts by mass of the solvent.

[0067] The polymerization temperature is not limited, and may be 0 to 100°C. In the case where the decomposition rate of the polymerization initiator is too high, including cases of using a dialkyl peroxy carbonate, a di[fluoro(or fluorochloro)acyl] peroxide or the like as the polymerization initiator, it is preferable to adopt a relatively low polymerization temperature such as in the temperature range of 0 to 35°C.

[0068] The polymerization pressure can suitably be determined according to other polymerization conditions such as the kind of the solvent to be used, the amount of the solvent, the vapor pressure and the polymerization temperature, but usually may be 0 to 9.8 MPaG. The polymerization pressure is preferably 0.1 to 5 MPaG, more preferably 0.5 to 2 MPaG and still more preferably 0.5 to 1.5 MPaG. When the polymerization pressure is 1.5 MPaG or higher, the production efficiency can be improved.

[0069] Examples of the additives in the polymerization include suspension stabilizers. The suspension stabilizers are not limited as long as being conventionally well-known ones, and methylcellulose, polyvinyl alcohols and the like can be used. With the use of a suspension stabilizer, suspended particles produced by the polymerization reaction are dispersed stably in an aqueous medium, and therefore the suspended particles hardly adhere on the reaction vessel even when a SUS-made reaction vessel not having been subjected to adhesion preventing treatment such as glass lining is used. Accordingly, a reaction vessel withstanding a high pressure can be used, and therefore the polymerization under a high pressure becomes possible and the production efficiency can be improved. By contrast, in the case of carrying out the polymerization without using the suspension stabilizer, the suspended particles may adhere and the production efficiency may be lowered with the use of a SUS-made reaction vessel not having been subjected to adhesion preventing treatment is used. The concentration of the suspension stabilizer in the aqueous medium can suitably be regulated depending on conditions.

[0070] In the case of obtaining an aqueous dispersion containing a fluoropolymer by a polymerization reaction, a dried fluoropolymer may be recovered by coagulating, cleaning and drying the fluorine-containing copolymer contained in the aqueous dispersion. Alternatively, in the case of obtaining the fluorine-containing copolymer as a slurry by a polymeri-

zation reaction, a dried fluoropolymer may be recovered by taking out the slurry from a reaction vessel, and cleaning and drying the slurry. The fluorine-containing copolymer can be recovered in a powder form by the drying.

[0071] The fluorine-containing copolymer obtained by the polymerization may be formed into pellets. A method of forming into pellets is not limited, and a conventionally known method can be used. Examples thereof include methods of melt extruding the fluorine-containing copolymer by using a single-screw extruder, a twin-screw extruder or a tandem extruder and cutting the resultant into a predetermined length to form the fluorine-containing copolymer into pellets. The extrusion temperature in the melt extrusion needs to be varied depending on the melt viscosity and the production method of the fluorine-containing copolymer, and is preferably the melting point of the fluorine-containing copolymer + 20°C to the melting point of the fluorine-containing copolymer + 140°C. A method of cutting the fluorine-containing copolymer is not limited, and there can be adopted a conventionally known method such as a strand cut method, a hot cut method, an underwater cut method, or a sheet cut method. Volatile components in the obtained pellets may be removed by heating the pellets (degassing treatment). Alternatively, the obtained pellets may be treated by bringing the pellets into contact with hot water of 30 to 200°C, steam of 100 to 200°C or hot air of 40 to 200°C.

[0072] The fluorine-containing copolymer obtained by the polymerization may be heated in the presence of air and water at a temperature of 100°C or higher (wet heat treatment). Examples of the wet heat treatment include a method in which by using an extruder, the fluorine-containing copolymer obtained by the polymerization is melted and extruded while air and water are fed. The wet heat treatment can convert thermally unstable functional groups of the fluorine-containing copolymer, such as -COF and -COOH, to thermally relatively stable -CF₂H, whereby the total number of -COF and -COOH and the total number of -COOH, -COOCH₃, -CH₂OH, -COF, -CF=CF₂ and -CONH₂ of the fluorine-containing copolymer can easily be regulated in the above-mentioned ranges. By heating the fluorine-containing copolymer, in addition to air and water, in the presence of an alkali metal salt, the conversion reaction to -CF₂H can be promoted. Depending on applications of the fluorine-containing copolymer, however, it should be paid regard to that contamination by the alkali metal salt must be avoided.

[0073] The fluorine-containing copolymer obtained by the polymerization may be subjected to a fluorination treatment. The fluorination treatment can be carried out by bringing the fluorine-containing copolymer subjected to no fluorination treatment into contact with a fluorine-containing compound. The fluorination treatment can convert thermally unstable functional groups of the fluorine-containing copolymer, such as -COOH, -COOCH₃, -CH₂OH, -COF, -CF=CF₂ and -CONH₂, and thermally relatively stable functional groups thereof, such as -CF₂H, to thermally very stable -CF₃. Resultantly, the total number of COOH, -COOCH₃, -CH₂OH, -COF, -CF=CF₂, -CONH₂ and -CF₂H of the fluorine-containing copolymer can easily be regulated in the above-mentioned ranges.

[0074] The fluorine-containing compound is not limited, but includes fluorine radical sources generating fluorine radicals under the fluorination treatment condition. The fluorine radical sources include F₂ gas, CoF₃, AgF₂, UF₆, OF₂, N₂F₂, CF₃OF, halogen fluorides (for example, IF₃ and ClF₃).

[0075] The fluorine radical source such as F₂ gas may be, for example, one having a concentration of 100%, but from the viewpoint of safety, the fluorine radical source is preferably mixed with an inert gas and diluted therewith to 5 to 50% by mass, and then used; and it is more preferably to be diluted to 15 to 30% by mass. The inert gas includes nitrogen gas, helium gas and argon gas, but from the viewpoint of the economic efficiency, nitrogen gas is preferred.

[0076] The condition of the fluorination treatment is not limited, and the fluorine-containing copolymer in a melted state may be brought into contact with the fluorine-containing compound, but the fluorination treatment can be carried out usually at a temperature of not higher than the melting point of the fluorine-containing copolymer, preferably at 20 to 220°C and more preferably at 100 to 200°C. The fluorination treatment is carried out usually for 1 to 30 hours and preferably 5 to 25 hours. The fluorination treatment is preferred which brings the fluorine-containing copolymer having been subjected to no fluorination treatment into contact with fluorine gas (F₂ gas).

[0077] A composition may be obtained by mixing the fluorine-containing copolymer of the present disclosure and as required, other components. The other components include fillers, plasticizers, processing aids, mold release agents, pigments, flame retarders, lubricants, light stabilizers, weathering stabilizers, electrically conductive agents, antistatic agents, ultraviolet absorbers, antioxidants, foaming agents, perfumes, oils, softening agents and dehydrofluorination agents.

[0078] Examples of the fillers include silica, kaolin, clay, organo clay, talc, mica, alumina, calcium carbonate, calcium terephthalate, titanium oxide, calcium phosphate, calcium fluoride, lithium fluoride, crosslinked polystyrene, potassium titanate, carbon, boron nitride, carbon nanotube and glass fiber. The electrically conductive agents include carbon black. The plasticizers include dioctyl phthalate and pentaerythritol. The processing aids include carnauba wax, sulfone compounds, low molecular weight polyethylene and fluorine-based auxiliary agents. The dehydrofluorination agents include organic oniums and amidines.

[0079] Then, the other components may be other polymers other than the above-mentioned fluorine-containing copolymer. The other polymers include fluoroelastomers other than the above fluorine-containing copolymer, fluoroelastomers and non-fluorinated polymers.

[0080] A method of producing the above composition includes a method in which the fluorine-containing copolymer

and other components are dry mixed, and a method in which the fluorine-containing copolymer and other components are previously mixed by a mixer, and then, melt kneaded by a kneader, a melt extruder or the like.

[0081] The fluorine-containing copolymer of the present disclosure or the above-mentioned composition can be used as a processing aid, a forming material or the like, but it is suitable to use that as a forming material. Then, aqueous dispersions, solutions and suspensions of the fluorine-containing copolymer of the present disclosure, and the copolymer/solvent-based materials can also be utilized; and these can be used for application of coating materials, encapsulation, impregnation, and casting of films. However, since the fluorine-containing copolymer of the present disclosure has the above-mentioned properties, it is preferable to use the copolymer as the forming material.

[0082] Formed articles may be obtained by forming the fluorine-containing copolymer of the present disclosure or the above-mentioned composition.

[0083] A method of forming the fluorine-containing copolymer or the composition is not limited, and includes injection molding, extrusion forming, compression molding, blow molding, transfer molding, rotomolding and rotolining molding. As the forming method, among these, preferable are extrusion forming, compression molding, injection molding and transfer molding; from the viewpoint of being able to produce forming articles in a high productivity, more preferable are injection molding, extrusion forming and transfer molding, and still more preferable are injection molding and extrusion forming. That is, it is preferable that formed articles are extrusion formed articles, compression molded articles, injection molded articles or transfer molded articles; and from the viewpoint of being able to produce molded articles in a high productivity, being injection molded articles, extrusion formed articles or transfer molded articles is more preferable, and being injection molded articles or extrusion formed articles is still more preferable.

[0084] Formed articles containing the fluorine-containing copolymer of the present disclosure may be, for example, nuts, bolts, joints, films, bottles, gaskets, electric wire coatings, tubes, hoses, pipes, valves, sheets, seals, packings, tanks, rollers, containers, cocks, connectors, filter housings, filter cages, flowmeters, pumps, wafer carriers, and wafer boxes.

[0085] The fluorine-containing copolymer of the present disclosure, the above composition and the above formed articles can be used, for example, in the following applications.

Food packaging films, and members for liquid transfer for food production apparatuses, such as lining materials of fluid transfer lines, packings, sealing materials and sheets, used in food production processes;

chemical stoppers and packaging films for chemicals, and members for chemical solution transfer, such as lining materials of liquid transfer lines, packings, sealing materials and sheets, used in chemical production processes; inner surface lining materials of chemical solution tanks and piping of chemical plants and semiconductor factories; members for fuel transfer, such as O (square) rings, tubes, packings, valve stem materials, hoses and sealing materials, used in fuel systems and peripheral equipment of automobiles, and such as hoses and sealing materials, used in ATs of automobiles;

members used in engines and peripheral equipment of automobiles, such as flange gaskets of carburetors, shaft seals, valve stem seals, sealing materials and hoses, and other vehicular members such as brake hoses, hoses for air conditioners, hoses for radiators, and electric wire coating materials;

members for chemical transfer for semiconductor production apparatuses, such as O (square) rings, tubes, packings, valve stem materials, hoses, sealing materials, rolls, gaskets, diaphragms and joints;

members for coating and inks, such as coating rolls, hoses and tubes, for coating facilities, and containers for inks; members for food and beverage transfer, such as tubes, hoses, belts, packings and joints for food and beverage, food packaging materials, and members for glass cooking appliances; members for waste liquid transport, such as tubes and hoses for waste transport;

members for high-temperature liquid transport, such as tubes and hoses for high-temperature liquid transport;

members for steam piping, such as tubes and hoses for steam piping;

corrosionproof tapes for piping, such as tapes wound on piping of decks and the like of ships;

various coating materials, such as electric wire coating materials, optical fiber coating materials, and transparent front side coating materials installed on the light incident side and back side lining materials of photoelectromotive elements of solar cells;

diaphragms and sliding members such as various types of packings of diaphragm pumps;

films for agriculture, and weathering covers for various kinds of roof materials, sidewalls and the like;

interior materials used in the building field, and coating materials for glasses such as non-flammable fireproof safety glasses; and

lining materials for laminate steel sheets used in the household electric field.

[0086] The fuel transfer members used in fuel systems of automobiles further include fuel hoses, filler hoses and evap hoses. The above fuel transfer members can also be used as fuel transfer members for gasoline additive-containing fuels, resultant to sour gasoline, resultant to alcohols, and resultant to methyl tertiary butyl ether and amines and the like.

[0087] The above chemical stoppers and packaging films for chemicals have excellent chemical resistance to acids and the like. The above chemical solution transfer members also include corrosionproof tapes wound on chemical plant pipes.

[0088] The above formed articles also include vehicular radiator tanks, chemical solution tanks, bellows, spacers, rollers and gasoline tanks, waste solution transport containers, high-temperature liquid transport containers and fishery and fish farming tanks.

[0089] The above formed articles further include members used for vehicular bumpers, door trims and instrument panels, food processing apparatuses, cooking devices, water- and oil-repellent glasses, illumination-related apparatuses, display boards and housings of OA devices, electrically illuminated billboards, displays, liquid crystal displays, cell phones, printed circuit boards, electric and electronic components, sundry goods, dust bins, bathtubs, unit baths, ventilating fans, illumination frames and the like.

[0090] Since formed articles containing the fluorine-containing copolymer of the present disclosure are excellent in the 50°C abrasion resistance, the heat aging resistance, the low hydrogen permeation, the 100°C high-temperature rigidity, the 140°C tensile creep resistance and the durability to repeated loads, the formed articles can suitably be utilized for nuts, bolts, joints, packings, valves, cocks, connectors, filter housings, filter cages, flowmeters, pumps, and the like. Among these, the formed articles can suitably be utilized as piping members (particularly, valves and joints) to be used for transportation of chemical solutions and flowmeter frames having flow paths of chemical solutions in flowmeters. The piping members and the flowmeter frames of the present disclosure are excellent in the 50°C abrasion resistance, the heat aging resistance, the low hydrogen permeation, the 100°C high-temperature rigidity, the 140°C tensile creep resistance and the durability to repeated loads. Hence, the piping members and the flowmeter frames of the present disclosure are hardly damaged even when stresses are repeatedly loaded according to the flow initiation, the flow suspension and the changes of flow amount of the chemical solutions.

[0091] Since formed articles containing the fluorine-containing copolymer of the present disclosure are excellent in the 50°C abrasion resistance, the heat aging resistance, the low hydrogen permeation, the 100°C high-temperature rigidity, the 140°C tensile creep resistance and the durability to repeated loads, the formed articles can suitably be utilized as members to be compressed such as gaskets and packings. The members to be compressed of the present disclosure may be gaskets or packings. The gaskets or the packings of the present disclosure can be produced at low cost by an injection molding method, and are excellent in the 50°C abrasion resistance, the heat aging resistance, the low hydrogen permeation, the 100°C high-temperature rigidity, the 140°C tensile creep resistance and the durability to repeated loads.

[0092] The size and shape of the members to be compressed of the present disclosure may suitably be set according to applications, and are not limited. The shape of the members to be compressed of the present disclosure may be, for example, annular. The members to be compressed of the present disclosure may also have, in plan view, a circular shape, an elliptic shape, a corner-rounded square or the like, and may be a shape having a throughhole in the central portion thereof.

[0093] It is preferable that the members to be compressed of the present disclosure are used as members constituting non-aqueous electrolyte batteries. Since the members to be compressed of the present disclosure are excellent in the 50°C abrasion resistance, the heat aging resistance, the low hydrogen permeation, the 100°C high-temperature rigidity, the 140°C tensile creep resistance and the durability to repeated loads, the members to be compressed are especially suitable as members to be used in the state of contacting with non-aqueous electrolytes in non-aqueous electrolyte batteries. That is, the members to be compressed of the present disclosure may also be ones having a liquid-contact surface with a non-aqueous electrolyte in the non-aqueous electrolyte batteries.

[0094] The non-aqueous electrolyte batteries are not limited as long as being batteries having a non-aqueous electrolyte, and examples thereof include lithium ion secondary batteries and lithium ion capacitors. Members constituting the non-aqueous electrolyte batteries include sealing members and insulating members.

[0095] For the non-aqueous electrolyte, one or two or more of well-known solvents can be used such as propylene carbonate, ethylene carbonate, butylene carbonate, γ -butyrolactone, 1,2-dimethoxyethane, 1,2-diethoxyethane, dimethyl carbonate, diethyl carbonate and ethyl methyl carbonate. The non-aqueous electrolyte batteries may further have an electrolyte. The electrolyte is not limited, but may be LiClO_4 , LiAsF_6 , LiPF_6 , LiBF_4 , LiCl , LiBr , $\text{CH}_3\text{SO}_3\text{Li}$, $\text{CF}_3\text{SO}_3\text{Li}$, cesium carbonate and the like.

[0096] The members to be compressed of the present disclosure can suitably be utilized, for example, as sealing members such as sealing gaskets and sealing packings, and insulating members such as insulating gaskets and insulating packings. The sealing members are members to be used for preventing leakage of a liquid or a gas, or penetration of a liquid or a gas from the outside. The insulating members are members to be used for insulating electricity. The members to be compressed of the present disclosure may also be members to be used for the purpose of both of sealing and insulation.

[0097] Since the members to be compressed of the present disclosure are excellent in the 50°C abrasion resistance, the heat aging resistance, the low hydrogen permeation, the 100°C high-temperature rigidity, the 140°C tensile creep resistance and the durability to repeated loads, the members to be compressed can suitably be utilized as sealing

members for non-aqueous electrolyte batteries or insulating members for non-aqueous electrolyte batteries. Further, the members to be compressed of the present disclosure, due to containing the above fluorine-containing copolymer, have the excellent insulating property. Therefore, in the case of using the members to be compressed of the present disclosure as insulating members, the member firmly adhere to two or more electrically conductive members and prevent short circuit over a long term.

[0098] Since by using the fluorine-containing copolymer of the present disclosure, a very thick coating layer can be formed in a uniform thickness on a core wire very large in diameter by an extrusion forming method, the fluorine-containing copolymer can suitably be utilized as a material for forming electric wire coatings. Since coated electric wires having a coating layer containing the fluorine-containing copolymer of the present disclosure exhibit almost no fluctuation in the outer diameter, the coated electric wires are excellent in the electric properties.

[0099] The coated electric wire has a core wire, and the coating layer installed on the periphery of the core wire and containing the fluorine-containing copolymer of the present disclosure. For example, an extrusion formed article made by melt extruding the fluorine-containing copolymer in the present disclosure on a core wire can be made into the coating layer. The coated electric wires are suitable for LAN cables (Ethernet Cables), high-frequency transmission cables, flat cables and heat-resistant cables and the like, and particularly, for transmission cables such as LAN cables (Ethernet Cables) and high-frequency transmission cables.

[0100] As a material for the core wire, for example, a metal conductor material such as copper or aluminum can be used. The core wire is preferably one having a diameter of 0.02 to 3 mm. The diameter of the core wire is more preferably 0.04 mm or larger, still more preferably 0.05 mm or larger and especially preferably 0.1 mm or larger. The diameter of the core wire is more preferable 2 mm or smaller.

[0101] With regard to specific examples of the core wire, there may be used, for example, AWG (American Wire Gauge)-46 (solid copper wire of 40 μm in diameter), AWG-26 (solid copper wire of 404 μm in diameter), AWG-24 (solid copper wire of 510 μm in diameter), and AWG-22 (solid copper wire of 635 μm in diameter).

[0102] The coating layer is preferably one having a thickness of 0.1 to 3.0 mm. It is also preferable that the thickness of the coating layer is 2.0 mm or smaller.

[0103] The high-frequency transmission cables include coaxial cables. The coaxial cables generally have a structure configured by laminating an inner conductor, an insulating coating layer, an outer conductor layer and a protective coating layer in order from the core part to the peripheral part. A formed article containing the fluorine-containing copolymer of the present disclosure can suitably be utilized as the insulating coating layer containing the fluorine-containing copolymer. The thickness of each layer in the above structure is not limited, but is usually: the diameter of the inner conductor is approximately 0.1 to 3 mm; the thickness of the insulating coating layer is approximately 0.3 to 3 mm; the thickness of the outer conductor layer is approximately 0.5 to 10 mm; and the thickness of the protective coating layer is approximately 0.5 to 2 mm.

[0104] Alternatively, the coating layer may be one containing cells, and is preferably one in which cells are homogeneously distributed.

[0105] The average cell size of the cells is not limited, but is, for example, preferably 60 μm or smaller, more preferably 45 μm or smaller, still more preferably 35 μm or smaller, further still more preferably 30 μm or smaller, especially preferable 25 μm or smaller and further especially preferably 23 μm or smaller. Then, the average cell size is preferably 0.1 μm or larger and more preferably 1 μm or larger. The average cell size can be determined by taking an electron microscopic image of an electric wire cross section, calculating the diameter of each cell and averaging the diameters.

[0106] The foaming ratio of the coating layer may be 20% or higher, and is more preferably 30% or higher, still more preferably 33% or higher and further still more preferably 35% or higher. The upper limit is not limited, but is, for example, 80%. The upper limit of the foaming ratio may be 60%. The foaming ratio is a value determined as $((\text{the specific gravity of an electric wire coating material} - \text{the specific gravity of the coating layer}) / (\text{the specific gravity of the electric wire coating material})) \times 100$. The foaming ratio can suitably be regulated according to applications, for example, by regulation of the amount of a gas, described later, to be injected in an extruder, or by selection of the kind of a gas dissolving.

[0107] Alternatively, the coated electric wire may have another layer between the core wire and the coating layer, and may further have another layer (outer layer) on the periphery of the coating layer. In the case where the coating layer contains cells, the electric wire of the present disclosure may be of a two-layer structure (skin-foam) in which a non-foaming layer is inserted between the core wire and the coating layer, a two-layer structure (foam-skin) in which a non-foaming layer is coated as the outer layer, or a three-layer structure (skin-foam-skin) in which a non-foaming layer is coated as the outer layer of the skin-foam structure. The non-foaming layer is not limited, and may be a resin layer composed of a resin, such as a TFE/HFP-based copolymer, a TFE/PAVE copolymer, a TFE/ethylene-based copolymer, a vinylidene fluoride-based polymer, a polyolefin resin such as polyethylene [PE], or polyvinyl chloride [PVC].

[0108] The coated electric wire can be produced, for example, by using an extruder, heating the fluorine-containing copolymer, extruding the fluorine-containing copolymer in a melt state on the core wire to thereby form the coating layer.

[0109] In formation of a coating layer, by heating the fluorine-containing copolymer and introducing a gas in the fluorine-containing copolymer in a melt state, the coating layer containing cells can be formed. As the gas, there can be used,

for example, a gas such as chlorodifluoromethane, nitrogen or carbon dioxide, or a mixture thereof. The gas may be introduced as a pressurized gas in the heated fluorine-containing copolymer, or may be generated by mingling a chemical foaming agent in the fluorine-containing copolymer. The gas dissolves in the fluorine-containing copolymer in a melt state.

[0110] Then, the fluorine-containing copolymer of the present disclosure can suitably be utilized as a material for products for high-frequency signal transmission.

[0111] The products for high-frequency signal transmission are not limited as long as being products to be used for transmission of high-frequency signals, and include (1) formed boards such as insulating boards for high-frequency circuits, insulating materials for connection parts and printed circuit boards, (2) formed articles such as bases of high-frequency vacuum tubes and antenna covers, and (3) coated electric wires such as coaxial cables and LAN cables. The products for high-frequency signal transmission can suitably be used in devices utilizing microwaves, particularly microwaves of 3 to 30 GHz, in satellite communication devices, cell phone base stations, and the like.

[0112] In the products for high-frequency signal transmission, the fluorine-containing copolymer of the present disclosure can suitably be used as insulators in that the dielectric loss tangent is low.

[0113] As the (1) formed boards, printed wiring boards are preferable in that the good electric property is provided. The printed wiring boards are not limited, but examples thereof include printed wiring boards of electronic circuits for cell phones, various computers, communication devices and the like. As the (2) formed articles, antenna covers are preferable in that the dielectric loss is low.

[0114] Since the fluorine-containing copolymer of the present disclosure can be formed at a high forming speed into thin films uniform in thickness by an extrusion forming method, and further, the obtained formed articles are excellent in the 50°C abrasion resistance, the heat aging resistance, the low hydrogen permeation, the 100°C high-temperature rigidity, the 140°C tensile creep resistance and the durability to repeated loads, the fluorine-containing copolymer can suitably be utilized for films.

[0115] The films of the present disclosure are useful as release films. The release films can be produced by forming the fluorine-containing copolymer of the present disclosure by melt extrusion, calendering, press molding, casting or the like. From the viewpoint that uniform thin films can be obtained, the release films can be produced by melt extrusion.

[0116] The films of the present disclosure can be applied to roll surfaces used in OA devices. Then, the fluorine-containing copolymer of the present disclosure is formed into needed shapes by extrusion forming, compression molding, press molding or the like to be formed into sheet-shapes, filmy shapes or tubular shapes, and can be used as surface materials for OA device rolls, OA device belts or the like. Thin-wall tubes and films can be produced particularly by a melt extrusion forming method.

[0117] Forming the fluorine-containing copolymer of the present disclosure by extrusion forming can give beautiful tubes, and further, the obtained formed articles are excellent in the 50°C abrasion resistance, the heat aging resistance, the low hydrogen permeation, the 100°C high-temperature rigidity, the 140°C tensile creep resistance and the durability to repeated loads, and therefore the fluorine-containing copolymer can suitably be utilized for tubes. Accordingly, the tubes containing the fluorine-containing copolymer of the present disclosure can be produced at a high productivity, and have beautiful shapes and are excellent in the 50°C abrasion resistance, the heat aging resistance, the low hydrogen permeation, the 100°C high-temperature rigidity, the 140°C tensile creep resistance and the durability to repeated loads.

[0118] So far, embodiments have been described, but it is to be understood that various changes and modifications of patterns and details may be made without departing from the subject matter and the scope of the claims.

EXAMPLES

[0119] The embodiments of the present disclosure will be described by Examples as follows, but the present disclosure is not limited only to these Examples.

[0120] Each numerical value in Examples was measured by the following methods.

(Contents of monomer units)

[0121] The content of each monomer unit of the fluorine-containing copolymer was measured by an NMR analyzer (for example, manufactured by Bruker BioSpin GmbH, AVANCE 300, high-temperature probe), or an infrared absorption spectrometer (manufactured by PerkinElmer, Inc., Spectrum One).

(The number of -CF₂H)

[0122] The number of -CF₂H groups of the fluorine-containing copolymer was determined from a peak integrated value of the -CF₂H group acquired in a ¹⁹F-NMR measurement using a nuclear magnetic resonance spectrometer AVANCE-300 (manufactured by Bruker BioSpin GmbH) and set at a measurement temperature of (the melting point of the polymer + 20)°C.

EP 4 299 626 A1

(The numbers of -COOH, -COOCH₃, -CH₂OH, -COF, -CF=CF₂ and -CONH₂)

[0123] A dried powder or pellets obtained in each of Examples and Comparative Examples were molded by cold press to prepare a film of 0.25 to 0.3 mm in thickness. The film was 40 times scanned by a Fourier transform infrared spectrometer [FT-IR (Spectrum One, manufactured by PerkinElmer, Inc.)] and analyzed to obtain an infrared absorption spectrum. The obtained infrared absorption spectrum was compared with an infrared absorption spectrum of an already known film to determine the kinds of terminal groups. Further, from an absorption peak of a specific functional group emerging in a difference spectrum between the obtained infrared absorption spectrum and the infrared absorption spectrum of the already known film, the number N of the functional group per 1×10⁶ carbon atoms in the sample was calculated according to the following formula (A).

$$N = I \times K/t \dots (A)$$

I: absorbance

K: correction factor

t: thickness of film (mm)

[0124] Regarding the functional groups in Examples, for reference, the absorption frequency, the molar absorption coefficient and the correction factor are shown in Table 2. Further, the molar absorption coefficients are those determined from FT-IR measurement data of low molecular model compounds.

[Table 2]

[0125]

Table 2

Functional Group	Absorption Frequency (cm ⁻¹)	Molar Extinction Coefficient (l/cm/mol)	Correction Factor	Model Compound
-COF	1883	600	388	C ₇ F ₁₅ COF
-COOH free	1815	530	439	H(CF ₂) ₆ COOH
-COOH bonded	1779	530	439	H(CF ₂) ₆ COOH
-COOCH ₃	1795	680	342	C ₇ F ₁₅ COOCH ₃
-CONH ₂	3436	506	460	C ₇ H ₁₅ CONH ₂
-CH ₂ OH ₂ , -OH	3648	104	2236	C ₇ H ₁₅ CH ₂ OH
-CF=CF ₂	1795	635	366	CF ₂ =CF ₂

(Melt flow rate (MFR))

[0126] The MFR of the fluorine-containing copolymer was determined by using a Melt Indexer G-01 (manufactured by Toyo Seiki Seisaku-sho, Ltd.), and making the polymer to flow out from a die of 2 mm in inner diameter and 8 mm in length at 372°C under a load of 5 kg and measuring the mass (g/10 min) of the polymer flowing out per 10 min from the die, according to ASTM D1238.

(Melting point)

[0127] The fluorine-containing copolymer was heated, as a first temperature raising step at a temperature-increasing rate of 10°C/min from 200°C to 350°C, then cooled at a cooling rate of 10°C/min from 350°C to 200°C, and then again heated, as second temperature raising step, at a temperature-increasing rate of 10°C/min from 200°C to 350°C by using a differential scanning calorimeter (trade name: X-DSC7000, manufactured by Hitachi High-Tech Science Corp.); and the melting point of the fluorine-containing copolymer was determined from a melting curve peak observed in the second temperature raising step.

Example 1

5 [0128] 40.25 kg of deionized water and 0.419 kg of methanol were fed in a 174 L-volume autoclave with a stirrer, and the autoclave inside was sufficiently vacuumized and replaced with nitrogen. Thereafter, the autoclave inside was vacuum deaerated, and in the autoclave put in a vacuum state, 40.25 kg of HFP and 0.82 kg of PPVE were fed; and the autoclave was heated to 25.5°C. Then, TFE was fed until the internal pressure of the autoclave became 0.970 MPa; and then, 1.25 kg of a 8-mass% di(ω -hydroperfluorohexanoyl) peroxide solution (hereinafter, abbreviated to DHP) was fed in the autoclave to initiate polymerization. The internal pressure of the autoclave at the initiation of the polymerization was set at 0.970 MPa, and by continuously adding TFE, the set pressure was made to be held. After 1.5 hours from the polymerization initiation, 0.419 kg of methanol was additionally fed. After 2 hours and 4 hours from the polymerization initiation, 1.25 kg of DHP was additionally fed, and the internal pressure was lowered by 0.002 MPa, respectively; after 6 hours therefrom, 0.96 kg thereof was fed and the internal pressure was lowered by 0.002 MPa. Hereafter, 0.25 kg of DHP was fed at every 2 hours until the reaction finished, and at the every time, the internal pressure was lowered by 0.002 MPa.

10 [0129] Then, at each time point when the amount of TFE continuously additionally fed reached 8.1 kg, 16.2 kg and 24.3 kg, 0.13 kg of PPVE was additionally fed. Then, at each time point when the amount of TFE additionally fed reached 6.0 kg and 18.1 kg, 0.419 kg of methanol was additionally fed in the autoclave. Then, when the amount of TFE additionally fed reached 40.25 kg, the polymerization was made to finish. After the finish of the polymerization, unreacted TFE and HFP were discharged to thereby obtain a wet powder. Then, the wet powder was washed with pure water, and thereafter dried at 150°C for 10 hours to thereby obtain 43.4 kg of a dry powder.

15 [0130] The obtained powder was melt extruded at 370°C by a screw extruder (trade name: PCM46, manufactured by Ikegai Corp.) to thereby obtain pellets of a copolymer. By using the obtained pellets, the HFP content and the PPVE content were measured by the methods described above. The results are shown in Table 3.

20 [0131] The obtained pellets were deaerated at 200°C for 72 hours in an electric furnace, thereafter put in a vacuum vibration-type reactor VVD-30 (manufactured by Okawara Mfg. Co. Ltd.), and heated to 110°C. After vacuumizing, an F₂ gas diluted to 20% by volume with N₂ gas was introduced to the atmospheric pressure. After 0.5 hour from the F₂ gas introduction, vacuumizing was once carried out and the F₂ gas was again introduced. Further after 0.5 hour therefrom, vacuumizing was again carried out, and the F₂ gas was again introduced. Hereafter, the F₂ gas introduction and the vacuumizing operation were repeated once an hour while the reaction was carried out at a temperature of 110°C for 8 hours. After the finish of the reaction, the reactor inside was replaced sufficiently with N₂ gas to finish the fluorination reaction to thereby obtain pellets. By using the obtained pellets, the above physical properties were measured by the methods described above. The results are shown in Table 3.

Example 2

25 [0132] Copolymer pellets were obtained as in Example 1, except for changing the amount of methanol fed before the polymerization initiation to 0.518 kg, changing the each amount of methanol dividedly additionally fed after the polymerization initiation to 0.518 kg, changing the amount of PPVE fed before the polymerization initiation to 1.03 kg, changing the each amount of PPVE dividedly additionally fed after the polymerization initiation to 0.17 kg, and changing the each set pressure in the autoclave inside before and after the polymerization initiation to 0.970 MPa. By using the obtained pellets without being fluorinated, the above physical properties were measured by the methods described above. The results are shown in Table 3.

Example 3

30 [0133] Copolymer pellets were obtained as in Example 1, except for changing the amount of methanol fed before the polymerization initiation to 0.516 kg, changing the each amount of methanol dividedly additionally fed after the polymerization initiation to 0.516 kg, changing the amount of PPVE fed before the polymerization initiation to 1.37 kg, changing the each amount of PPVE dividedly additionally fed after the polymerization initiation to 0.22 kg, and changing the each set pressure in the autoclave inside before and after the polymerization initiation to 0.970 MPa. By using the obtained pellets, the content of HFP and the content of PPVE were measured by the methods described above. The results are shown in Table 3.

35 [0134] The obtained pellets were deaerated at 200°C for 8 hours in an electric furnace, put in a vacuum vibration-type reactor WD-30 (manufactured by Okawara Mfg. Co. Ltd.), and heated to 200°C. After vacuumizing, F₂ gas diluted to 20% by volume with N₂ gas was introduced to the atmospheric pressure. 0.5 hour after the F₂ gas introduction, vacuumizing was once carried out and F₂ gas was again introduced. Further, 0.5 hour thereafter, vacuumizing was again carried out and F₂ gas was again introduced. Thereafter, while the above operation of the F₂ gas introduction and the vacuumizing was carried out once every 1 hour, the reaction was carried out at a temperature of 200°C for 8 hours. After the reaction was finished, the reactor interior was replaced sufficiently by N₂ gas to finish the fluorination reaction,

thereby obtaining pellets. By using the obtained pellets, the above physical properties were measured by the methods described above. The results are shown in Table 3.

Example 4

[0135] Copolymer pellets were obtained as in Example 1, except for changing the amount of methanol fed before the polymerization initiation to 0.526 kg, changing the each amount of methanol dividedly additionally fed after the polymerization initiation to 0.526 kg, changing the amount of PPVE fed before the polymerization initiation to 1.51 kg, changing the each amount of PPVE dividedly additionally fed after the polymerization initiation to 0.24 kg, and changing the each set pressure in the autoclave inside before and after the polymerization initiation to 0.970 MPa. By using the obtained pellets, the HFP content and the PPVE content were measured by the methods described above. The results are shown in Table 3.

[0136] The obtained pellets were fluorinated as in Example 3. By using the obtained pellets, the above physical properties were measured by the methods described above. The results are shown in Table 3.

Example 5

[0137] Copolymer pellets were obtained as in Example 1, except for changing the amount of methanol fed before the polymerization initiation to 0.450 kg, changing the each amount of methanol dividedly additionally fed after the polymerization initiation to 0.450 kg, changing the amount of PPVE fed before the polymerization initiation to 1.09 kg, changing the each amount of PPVE dividedly additionally fed after the polymerization initiation to 0.19 kg, and changing the each set pressure in the autoclave inside before and after the polymerization initiation to 0.948 MPa. By using the obtained pellets, the HFP content and the PPVE content were measured by the methods described above. The results are shown in Table 3.

[0138] The obtained pellets were fluorinated as in Example 3. By using the obtained pellets, the above physical properties were measured by the methods described above. The results are shown in Table 3.

Comparative Example 1

[0139] Copolymer pellets were obtained as in Example 1, except for changing the amount of methanol fed before the polymerization initiation to 0.257 kg, changing the each amount of methanol dividedly additionally fed after the polymerization initiation to 0.257 kg, changing the amount of PPVE fed before the polymerization initiation to 1.12 kg, changing the each amount of PPVE dividedly additionally fed after the polymerization initiation to 0.23 kg, and changing the each set pressure in the autoclave inside before and after the polymerization initiation to 0.892 MPa. By using the obtained pellets without being fluorinated, the above physical properties were measured by the methods described above. The results are shown in Table 3.

Comparative Example 2

[0140] Copolymer pellets were obtained as in Example 1, except for changing the amount of methanol fed before the polymerization initiation to 0.374 kg, changing the each amount of methanol dividedly additionally fed after the polymerization initiation to 0.374 kg, changing the amount of PPVE fed before the polymerization initiation to 1.54 kg, changing the each amount of PPVE dividedly additionally fed after the polymerization initiation to 0.29 kg, and changing the each set pressure in the autoclave inside before and after the polymerization initiation to 0.924 MPa. By using the obtained pellets without being fluorinated, the above physical properties were measured by the methods described above. The results are shown in Table 3.

Comparative Example 3

[0141] Copolymer pellets were obtained as in Example 1, except for changing the amount of methanol fed before the polymerization initiation to 0.502 kg, changing the each amount of methanol dividedly additionally fed after the polymerization initiation to 0.502 kg, changing the amount of PPVE fed before the polymerization initiation to 0.47 kg, changing the each amount of PPVE dividedly additionally fed after the polymerization initiation to 0.09 kg, and changing the each set pressure in the autoclave inside before and after the polymerization initiation to 0.924 MPa. By using the obtained pellets without being fluorinated, the above physical properties were measured by the methods described above. The results are shown in Table 3.

Comparative Example 4

5 [0142] 0.945 kg of deionized water and 0.014 kg of methanol were fed in a 4 L-volume autoclave with a stirrer, and the autoclave inside was sufficiently vacuumized and replaced with nitrogen. Thereafter, the autoclave inside was vacuum deaerated, and in the autoclave put in a vacuum state, 0.945 kg of HFP was fed; and the autoclave was heated to 25.5°C. Then, TFE was fed until the internal pressure of the autoclave became 0.970 MPa; and then, 0.029 kg of an 8-mass% di(ω -hydroperfluorohexanoyl) peroxide solution (hereinafter, abbreviated to DHP) was fed in the autoclave to initiate polymerization. The internal pressure of the autoclave at the initiation of the polymerization was set at 0.970 MPa, and by continuously adding TFE, the set pressure was held. After 1.5 hours from the polymerization initiation, 10 0.014 kg of methanol was additionally fed. After 2 hours and 4 hours from the polymerization initiation, 0.029 kg of DHP was additionally fed, and the internal pressure was lowered by 0.002 MPa, respectively.

15 [0143] Then, at the time point when the amount of TFE additionally fed reached 0.141 kg, 0.014 kg of methanol was additionally fed in the autoclave. Then, when the amount of TFE additionally fed reached 0.473 kg, the polymerization was made to finish. After the finish of the polymerization, unreacted TFE and HFP were discharged to thereby obtain a wet powder. Then, the wet powder was washed with pure water, and thereafter dried at 150°C for 10 hours to thereby obtain 0.504 kg of a dry powder.

[0144] The obtained powder was melt extruded at 370°C by a 14 ϕ screw extruder (manufactured by Imoto Machinery Co. Ltd.) to thereby obtain pellets of a copolymer. By using the obtained pellets, the HFP content and the PPVE content were measured by the methods described above. The results are shown in Table 3.

20 [0145] The obtained pellets were deaerated at 200°C for 8 hours in an electric furnace, thereafter put in a 500-ml portable reactor (TVS-1 type, manufactured by Taiatsu Techno Corporation), and heated to 200°C. After vacuumizing, an F₂ gas diluted to 20% by volume with N₂ gas was introduced to the atmospheric pressure. After 0.5 hour from the F₂ gas introduction, vacuumizing was once carried out and the F₂ gas was again introduced. Further after 0.5 hour therefrom, vacuumizing was again carried out, and the F₂ gas was again introduced. Hereafter, the F₂ gas introduction and the vacuumizing operation were repeated once an hour while the reaction was carried out at a temperature of 200°C 25 for 8 hours. After the finish of the reaction, the reactor inside was replaced sufficiently with N₂ gas to finish the fluorination reaction to thereby obtain pellets. By using the obtained pellets, the above physical properties were measured by the methods described above. The results are shown in Table 3.

30 Comparative Example 5

[0146] Copolymer pellets were obtained as in Example 1, except for changing the amount of methanol fed before the polymerization initiation to 0.749 kg, changing the each amount of methanol dividedly additionally fed after the polymerization initiation to 0.749 kg, changing the amount of PPVE fed before the polymerization initiation to 1.53 kg, changing the each amount of PPVE dividedly additionally fed after the polymerization initiation to 0.19 kg, changing the temperature of the autoclave to 23°C, and changing the each set pressure in the autoclave inside before and after the polymerization initiation to 0.994 MPa. By using the obtained pellets, the HFP content and the PPVE content were measured by the methods described above. The results are shown in Table 3.

35 [0147] The obtained pellets were fluorinated as in Example 3. By using the obtained pellets, the above physical properties were measured by the methods described above. The results are shown in Table 3.

Comparative Example 6

40 [0148] Copolymer pellets were obtained as in Example 1, except for changing the amount of methanol fed before the polymerization initiation to 0.570 kg, changing the each amount of methanol dividedly additionally fed after the polymerization initiation to 0.570 kg, changing the amount of PPVE fed before the polymerization initiation to 1.09 kg, changing the each amount of PPVE dividedly additionally fed after the polymerization initiation to 0.19 kg, and changing the each set pressure in the autoclave inside before and after the polymerization initiation to 0.948 MPa. By using the obtained pellets, the HFP content and the PPVE content were measured by the methods described above. The results are shown in Table 3.

45 [0149] The obtained pellets were fluorinated as in Example 3. By using the obtained pellets, the above physical properties were measured by the methods described above. The results are shown in Table 3.

Comparative Example 7

50 [0150] Copolymer pellets were obtained as in Example 1, except for changing the amount of methanol fed before the polymerization initiation to 0.407 kg, changing the each amount of methanol dividedly additionally fed after the polymerization initiation to 0.407 kg, changing the amount of PPVE fed before the polymerization initiation to 2.40 kg, changing

the each amount of PPVE dividedly additionally fed after the polymerization initiation to 0.37 kg, and changing the each set pressure in the autoclave inside before and after the polymerization initiation to 0.989 MPa. By using the obtained pellets without being fluorinated, the above physical properties were measured by the methods described above. The results are shown in Table 3.

5

Comparative Example 8

[0151] Copolymer pellets were obtained as in Example 1, except for changing the amount of methanol fed before the polymerization initiation to 0.592 kg, changing the each amount of methanol dividedly additionally fed after the polymerization initiation to 0.592 kg, changing the amount of PPVE fed before the polymerization initiation to 1.41 kg, changing the each amount of PPVE dividedly additionally fed after the polymerization initiation to 0.22 kg, and changing the each set pressure in the autoclave inside before and after the polymerization initiation to 0.979 MPa. By using the obtained pellets without being fluorinated, the above physical properties were measured by the methods described above. The results are shown in Table 3.

15

Comparative Example 9

[0152] 945 g of deionized water and 3.1 g of methanol were fed in a 4 L-volume autoclave with a stirrer, and the autoclave inside was sufficiently vacuumized and replaced with nitrogen. Thereafter, the autoclave inside was vacuum deaerated, and in the autoclave put in a vacuum state, 945 g of HFP and 32.3 g of PPVE were fed; and the autoclave was heated to 25.5°C. Then, TFE was fed until the internal pressure of the autoclave became 0.970 MPa; and then, 29.4 g of an 8-mass% di(*o*-hydroperfluorohexanoyl) peroxide solution (hereinafter, abbreviated to DHP) was fed in the autoclave to initiate polymerization. The internal pressure of the autoclave at the initiation of the polymerization was set at 0.970 MPa, and by continuously adding TFE, the set pressure was held. After 1.5 hours from the polymerization initiation, 3.1 g of methanol was additionally fed. After 2 hours and 4 hours from the polymerization initiation, 29.4 g of DHP was additionally fed, and the internal pressure was lowered by 0.002 MPa, respectively; and after 6 hours therefrom, 22.6 g thereof was fed and the internal pressure was lowered by 0.002 MPa. Hereafter, 6.0 g of DHP was additionally fed at every 2 hours until the reaction finished, and at the every time, the internal pressure was lowered by 0.002 MPa.

20

25

[0153] Then, at each time point when the amount of TFE continuously additionally fed reached 190 g and 380 g, 5.2 g of PPVE was additionally fed. Then, when the amount of TFE additionally fed reached 140 g, 3.1 g of methanol was additionally fed in the autoclave. Then, when the amount of TFE additionally fed reached 380 g, the polymerization was made to finish. After the finish of the polymerization, unreacted TFE and HFP were discharged to thereby obtain a wet powder. Then, the wet powder was washed with pure water, and thereafter dried at 150°C for 10 hours and then at 205°C for 24 hours to thereby obtain 411 g of a dry powder. By using the obtained powder, the HFP content and the PEVE content were measured by the methods described above. The results are shown in Table 3.

35

[0154] The obtained powder was put in a portable reactor TVS-1 type (manufactured by Taiatsu Techno Corporation), and heated to 200°C. After vacuumizing, an F₂ gas diluted to 20% by volume with N₂ gas was introduced to the atmospheric pressure. After 0.5 hour from the F₂ gas introduction, vacuumizing was once carried out and the F₂ gas was again introduced. Further after 0.5 hour therefrom, vacuumizing was again carried out, and the F₂ gas was again introduced. Hereafter, the F₂ gas introduction and the vacuumizing operation were repeated once an hour while the reaction was carried out at a temperature of 200°C for 8 hours. After the finish of the reaction, the reactor inside was replaced sufficiently with N₂ gas to finish the fluorination reaction to thereby obtain a powder. By using the obtained powder, the above physical properties were measured by the methods described above. The results are shown in Table 3.

40

45 [Table 3]

[0155]

Table 3

	HFP content (% by mol)	PPVE content (% by mol)	Number of -CF ₂ H (number/C10 ⁶)	Number of functional groups, N (number/C10 ⁶)	MFR (g/10 min)	Melting point (°C)
Example 1	3.55	0.46	13	<6	2.0	285
Example 2	3.56	0.58	248	24	4.0	284
Example 3	3.57	0.77	<9	<6	6.0	280

50

55

EP 4 299 626 A1

(continued)

	HFP content (% by mol)	PPVE content (% by mol)	Number of -CF ₂ H (number/C10 ⁶)	Number of functional groups, N (number/C10 ⁶)	MFR (g/10 min)	Melting point (°C)
5	Example 4	3.58	0.85	<9	<6	8.0 278
	Example 5	3.92	0.66	<9	<6	5.0 279
10	Comparative Example 1	4.98	0.82	217	32	3.3 266
	Comparative Example 2	4.36	1.02	274	36	5.4 268
15	Comparative Example 3	4.31	0.31	315	18	6.6 283
	Comparative Example 4	3.53	0	<9	<6	5.0 296
20	Comparative Example 5	2.39	0.65	<9	<6	7.0 292
	Comparative Example 6	3.92	0.66	<9	<6	13.0 279
25	Comparative Example 7	3.30	1.00	185	35	2.6 277
	Comparative Example 8	3.43	0.77	329	29	8.0 281
30	Comparative Example 9	3.57	0.77	<9	<6	0.2 278

[0156] The description of "<9" in Table 3 means that the number of -CF₂H groups was less than 9. The description of "<6" in Table 3 means that the total number (number of functional groups, N) of -COOH, -COOCH₃, -CH₂OH, -COF, -CF=CF₂ and -CONH₂ was less than 6.

[0157] Then, by using the obtained pellets, the following properties were evaluated. The results are shown in Table 4.

(Abrasion test)

[0158] By using the pellets and a heat press molding machine, a sheet-shape test piece of approximately 0.2 mm in thickness was prepared and cut out into a test piece of 10 cm × 10 cm. The prepared test piece was fixed on a test bench of a Taber abrasion tester (No. 101, Taber type abrasion tester with an option, manufactured by Yasuda Seiki Seisakusho, Ltd.), and the abrasion test was carried out under the conditions of a test piece surface temperature of 50°C, at a load of 500 g, using an abrasion wheel CS-10 (rotationally polished in 20 rotations with an abrasion paper #240), and at a rotation rate of 60 rpm, using the Taber abrasion tester. The weight of the test piece after 1,000 rotations was measured, and the same test piece was further subjected to the test of 7,000 rotations and thereafter, the weight thereof was measured. The abrasion loss was determined by the following formula.

$$\text{Abrasion loss (mg)} = M1 - M2$$

M1: the weight of the test piece after the 1,000 rotations (mg)

M2: the weight of the test piece after the 7,000 rotations (mg)

(Hot air crack test)

[0159] By using the pellets and a heat press molding machine, a sheet-shape formed article of approximately 2 mm

EP 4 299 626 A1

in thickness was prepared. The obtained sheet was punched out by using a rectangular dumbbell of 13.5 mm × 38 mm to obtain three test pieces. A notch was formed on the middle of a long side of the each obtained test piece according to ASTM D1693 by a blade of 19 mm × 0.45 mm. The three notched test pieces were continuously exposed to a hot air at 200°C for 2 weeks. The obtained three notched test pieces were mounted on a stress crack test jig according to ASTM D1693, and heated in an electric furnace at 200°C for 24 hours; thereafter, the notches and their vicinities were visually observed and the number of cracks was counted. A sheet having no crack generated is excellent in the heat aging resistance.

Good: the number of cracks was 0

Poor: the number of cracks was 1 or more

(Hydrogen permeation coefficient)

[0160] By using the pellets and a heat press molding machine, a sheet-shape test piece of approximately 0.1 mm in thickness was prepared. Measurement of the hydrogen permeability was carried out on the obtained test piece according to a method described in JIS K7126-1:2006 by using a differential pressure type permeability tester (L100-5000 type gas permeability tester, manufactured by Systech Illinois Ltd.). There was obtained a numerical value of the hydrogen permeability at a permeation area of 50.24 cm², a test temperature of 60°C and at a test humidity of 0%RH. By using the obtained hydrogen permeability and the thickness of the test piece, the hydrogen permeability coefficient was calculated by the following formula.

$$\text{Hydrogen permeability coefficient (cm}^3\cdot\text{mm}/(\text{m}^2\cdot 24\text{h}\cdot\text{atm})) = \text{GTR}$$

× d

GTR: hydrogen permeability (cm³/(m²·24h·atm))

d: test piece thickness (mm)

(100°C load deflection rate)

[0161] By using the pellets and a heat press molding machine, a sheet-shape test piece of approximately 4 mm in thickness was prepared and cut out into a test piece of 80 × 10 mm; and the test piece was heated in an electric furnace at 100°C for 20 hours. A test for the 100°C load deflection rate was carried out according to a method described in JIS K7191-1 except for using the obtained test piece, by a heat distortion tester (manufactured by Yasuda Seiki Seisakusho, Ltd.) under the conditions of at a test temperature of 30 to 150°C, at a temperature-increasing rate of 120°C/h, at a bending stress of 1.8 MPa and the flatwise method. The load deflection rate was determined by the following formula. A sheet low in the 100°C load deflection rate is excellent in the 100°C high-temperature rigidity.

$$\text{Load deflection rate (\%)} = a2/a1 \times 100$$

a1: a thickness of the test piece before the test (mm)

a2: an amount deflected at 100°C (mm)

(Tensile creep test)

[0162] The tensile creep strain was measured by using TMA-7100, manufactured by Hitachi High-Tech Science Corp. By using the pellets and a heat press molding machine, a sheet of approximately 0.1 mm in thickness was prepared, and a sample of 2 mm in width and 22 mm in length was prepared from the sheet. The sample was mounted on measurement jigs with the distance between the jigs of 10 mm. A load was applied on the sample so that the cross-sectional load became 3.32 N/mm², and allowed to stand at 140°C; and there was measured the displacement (mm) from the timepoint of 90 min from the test initiation to the timepoint of 450 min from the test initiation, and there was calculated the proportion (tensile creep strain (%)) of the displacement (mm) to the initial sample length (10 mm). A sheet low in the tensile creep stain (%) measured under the condition of at 140°C for 450 min is hardly elongated even when a tensile load is applied for a long time in a high-temperature environment, being excellent in the high-temperature tensile creep property (140°C).

(Tensile strength after 8,000 cycles)

[0163] The tensile strength after 8,000 cycles was measured by using a fatigue testing machine, MMT-250NV-10, manufactured by Shimadzu Corp. By using the pellets and a heat press molding machine, a sheet of approximately 2.4 mm in thickness was prepared, and a sample in a dumbbell shape (thickness: 2.4 mm, width: 5.0 mm, measuring section length: 22 mm) was prepared by using an ASTM D1708 microdumbbell. The sample was mounted on measuring jigs and the measuring jigs were installed in a state of the sample being mounted in a thermostatic chamber at 110°C. The tensile operation in the uniaxial direction was repeated at a stroke of 0.2 mm and at a frequency of 100 Hz, and there was measured the tensile strength at every tensile operation (tensile strength at the time the stroke was +0.2 mm, unit: N).

[0164] A sheet high in the tensile strength after 8,000 cycles retains the high tensile strength even after loading is repeated 8,000 times, being excellent in the durability (110°C) to repeated loads.

(Test of the own weight deformation in the melt time)

[0165] By using the pellets and a heat press molding machine, there was prepared a formed article of 13 mm in diameter and approximately 6.5 mm in height. A test piece of 6.3 mm in height was prepared by cutting the obtained formed article. The prepared test piece was put in a SUS-made petri dish, and heated in an electric furnace at 330°C for 30 min; and thereafter, the test piece together with the petri dish was water cooled. The diameter of the surface (bottom surface) of the test piece having contacted with the petri dish was measured by calipers, and the percentage increase of the bottom area was calculated by the following formula.

[0166] Percentage increase of the bottom area (%) = {a bottom area of the test piece after the heating (mm²) - a bottom area of the test piece before the heating (mm²)} / the bottom area of the test piece before the heating (mm²) × 100

[0167] It is meant that the lower the percentage increase of the bottom area, the more hardly the formed article is deformed by its own weight in a melt time. The fluorine-containing copolymer which gives formed articles low in the bottom area percentage increase, even in the case of being formed by the extrusion forming method to prepare thick sheets and large pipes, is excellent in that there are obtained formed articles in a melt state which are hardly deformed and the formed articles which have a desired shape after being cooled and solidified.

(Electric wire coating extrusion conditions)

[0168] By using a 30-mm ϕ electric wire coating extruder (manufactured by Tanabe Plastics Machinery Co. Ltd.), the fluorine-containing copolymer was extrusion coated in the following coating thickness on a copper conductor of 1.00 mm in conductor diameter to thereby obtain a coated electric wire. The electric wire coating extrusion conditions were as follows.

- a) Core conductor: conductor diameter: 1.00 mm
- b) Coating thickness: 0.70 mm
- c) Coated electric wire diameter: 2.40 mm
- d) Electric wire take-over speed: 3 m/min
- e) Extrusion condition:

- Cylinder screw diameter = 30 mm, a single-screw extruder of L/D = 22
- Die (inner diameter)/tip (outer diameter) = 24.0 mm/10.0 mm Set temperature of the extruder: barrel section C-1 (340°C), barrel section C-2 (375°C), barrel section C-3 (390°C), head section H (400°C), die section D-1 (400°C), die section D-2 (400°C), Set temperature for preheating core wire: 80°C

(Fluctuation in the outer diameter)

[0169] By using an outer diameter measuring device (ODAC18XY, manufactured by Zumbach Electronic AG), the outer diameter of the obtained coated electric wire was measured continuously for 1 hour. A fluctuation value of the outer diameter was determined by rounding, to two decimal places, an outer diameter value most separated from the predetermined outer diameter value (2.40 mm) among measured outer diameter values. The proportion (fluctuation rate of the outer diameter) of the absolute value of a difference between the predetermined outer diameter and the fluctuation value of the outer diameter to the predetermined outer diameter (2.40 mm) was calculated and evaluated according to the following criteria.

Fluctuation rate of the outer diameter (%) = |(the fluctuation value of the outer diameter) - (the predetermined outer diameter)| / (the predetermined outer diameter) × 100

±1%: the fluctuation rate of the outer diameter was 1% or lower.

±2%: the fluctuation rate of the outer diameter was higher than 1% and 2% or lower.

Poor: the fluctuation rate of the outer diameter was higher than 2%.

(Tube formability)

[0170] By using a φ30-mm extruder (manufactured by Tanabe Plastics Machinery Co. Ltd.), the pellets were extruded to obtain a tube of 10.0 mm in outer diameter and 1.0 mm in wall thickness. The extrusion conditions were as follows.

a) Die inner diameter: 25 mm

b) Mandrel outer diameter: 13 mm

c) Sizing die inner diameter: 10.5 mm

d) Take-over speed: 0.4 m/min

e) Outer diameter: 10.0 mm

f) Wall thickness: 1.0 mm

g) Extrusion condition:

· Cylinder screw diameter = 30 mm, a single-screw extruder of L/D = 22

Set temperature of the extruder: barrel section C-1 (350°C), barrel section C-2 (370°C), barrel section C-3 (380°C), head section H-1 (390°C), die section D-1 (390°C), die section D-2 (390°C)

[0171] The obtained tube was observed and evaluated according to the following criteria. The appearance of the tube was visually observed.

Good: The appearance was good.

Poor: The cross-section did not become circular and the appearance was poor, including that flattening occurred and uneven wall thickness emerged.

(Film formability)

[0172] By using a φ14-mm extruder (manufactured by Imoto Machinery Co. Ltd.) and a T die, the pellets were formed to prepare a film. The extrusion conditions were as follows.

a) Take-up speed: 1 m/min

b) Roll temperature: 120°C

c) Film width: 70 mm

d) Thickness: 0.10 mm

e) Extrusion condition:

· Cylinder screw diameter = 14 mm, a single-screw extruder of L/D = 20

Set temperature of the extruder: barrel section C-1 (330°C), barrel section C-2 (350°C), barrel section C-3 (365°C), T die section (370°C)

[0173] The extrusion forming of the fluorine-containing copolymer was continued until the fluorine-containing copolymer became enabled to be stably extruded from the extruder. Successively, by extruding the fluorine-containing copolymer, a film (70 mm wide) of 11 m or longer in length was prepared so that that thickness became 0.10 mm. A portion of 10 to 11 m of the obtained film was cut out from one end of the film and there was prepared a test piece (1 m long and 70 mm wide) for measuring the fluctuation in the thickness. Then, there were measured thicknesses of 3 points in total on one end of the obtained film of a middle point in the width direction and 2 points separated by 25 mm from the middle point in the width direction. Further, there were measured 9 points in total of 3 middle points in the width direction spaced

EP 4 299 626 A1

at intervals of 25 mm from the middle point in the width direction of the one end of the film toward the other end thereof, and 2 points separated by 25 mm in the width direction from the each middle point of the 3 middle points. Among the 12 measurement values in total, the case where the number of points having measurement values out of the range of $\pm 10\%$ of 0.10 mm was 1 or less was taken as good; and the case where the number of points having measurement values out of the range of $\pm 10\%$ of 0.10 mm was 2 or more was taken as poor.

(Immersion test in a hydrogen peroxide aqueous solution)

[0174] By using the pellets and a heat press molding machine, a sheet of approximately 0.2 mm in thickness was prepared and test pieces of 15 mm square were prepared. 10 sheets of the test pieces and 15 g of a 3-mass% hydrogen peroxide aqueous solution were put in a 50-mL polypropylene-made bottle, and heated in an electric furnace at 95°C for 20 hours, and thereafter cooled to room temperature. The test pieces were removed from the hydrogen peroxide aqueous solution; and a TISAB solution (10) (manufactured by Kanto Chemical Co., Inc.) was added to the remaining hydrogen peroxide aqueous solution; and the fluorine ion concentration in the obtained hydrogen peroxide aqueous solution was measured by a fluorine ion meter. The fluorine ion concentration (concentration of fluorine ions having dissolved out) per sheet weight was calculated from an obtained measurement value according to the following formula.

Dissolving-out fluorine ion concentration (ppm by mass) =
the measurement value (ppm) \times the amount of the hydrogen peroxide
aqueous solution (g) / the weight of the test piece (g)

[Table 4]

5
10
15
20
25
30
35
40
45
50
55

[0175]

Table 4

	50°C Abrasion loss (mg) (mg)	Hot air crack test	Hydrogen permeation coefficient (cm ³ ·mm/ (m ² ·24h· atm))	100°C Load deflection rate (%)	140°C Tensile creep strain (%)	Tensile strength after 8,000 cycles (N)	Own weight deformation test (%)	Electric wirecoating test		Tube formability	Film formability	Hydrogen peroxide aqueous solution immersion test (ppm by mass)
								Fluctuation in outer diameter				
Example 1	16.7	good	1866	45%	0.23	12.83	43	±2%	good	good	2.4	
Example 2	18.7	good	1890	41%	0.28	12.44	80	±1%	good	good	4.6	
Example 3	20.0	good	1771	41%	0.33	12.20	110	±1%	good	good	2.3	
Example 4	21.0	good	1746	41%	0.37	12.03	133	±2%	good	good	2.3	
Example 5	19.3	good	1785	43%	0.37	11.71	96	±1%	good	good	2.3	
Comparative Example 1	14.9	good	2046	62%	0.64	10.15	68	±1%	good		4.4	
Comparative Example 2	17.2	good	2013	57%	0.56	10.93	102	±1%	good		4.9	
Comparative Example 3	22.6	poor	1756	35%	0.42	10.90	118	±1%	good		5.2	
Comparative Example 4	23.5	poor	1532	26%	0.14	12.37	96				2.3	
Comparative Example 5	22.7	poor	1600	28%	0.17	14.11	123	±1%	good		2.3	
Comparative Example 6	24.9	poor	1584	34%	0.45	11.90	160	poor	poor		2.3	
Comparative Example 7	14.6	good	2161	53%	0.26	13.11	55	±2%	good		4.0	
Comparative Example 8	22.0	poor	1845	37%	0.32	12.30	133	±2%	good		5.3	

5
10
15
20
25
30
35
40
45
50
55

(continued)

									Hydrogen peroxide aqueous solution immersion test (ppm by mass)	2.3
									Film formability	
									Tube formability	
									Electric wirecoating test	
									Fluctuation in outer diameter	
									Own weight deformation test (%)	4
									Tensile strength after 8,000 cycles (N)	14.03
									140°C Tensile creep strain (%)	0.14
									100°C Load deflection rate (%)	75%
									Hydrogen permeation coefficient (cm ³ ·mm/(m ² ·24h·atm))	2488
									Hot air crack test	good
									50°C Abrasion loss (mg) (mg)	9.7
									Comparative Example 9	

Claims

1. A fluorine-containing copolymer, comprising:

5 tetrafluoroethylene unit; hexafluoropropylene unit; and
perfluoro(propyl vinyl ether) unit,

wherein the copolymer has a content of hexafluoropropylene unit of 3.55 to 4.10% by mol with respect to the whole of the monomer units, a content of perfluoro(propyl vinyl ether) unit of 0.39 to 0.90% by mol with respect to the whole of the monomer units, and a melt flow rate at 372°C of 1.0 to 9.0 g/10 min.

- 10 2. The fluorine-containing copolymer according to claim 1, wherein the copolymer has a content of hexafluoropropylene unit of 3.55 to 3.92% by mol with respect to the whole of the monomer units.

- 15 3. The fluorine-containing copolymer according to claim 1 or 2, wherein the copolymer has a content of perfluoro(propyl vinyl ether) unit of 0.46 to 0.85% by mol with respect to the whole of the monomer units.

4. The fluorine-containing copolymer according to any one of claims 1 to 3, wherein the copolymer has a melt flow rate at 372°C of 2.0 to 8.0 g/10 min.

- 20 5. The fluorine-containing copolymer according to any one of claims 1 to 4, wherein the copolymer has a number of functional groups of 90 or less per 10⁶ main-chain carbon atoms.

6. An injection molded article, comprising the fluorine-containing copolymer according to any one of claims 1 to 5.

- 25 7. An extrusion formed article, comprising the fluorine-containing copolymer according to any one of claims 1 to 5.

8. A transfer molded article, comprising the fluorine-containing copolymer according to any one of claims 1 to 5.

- 30 9. A coated electric wire, comprising a coating layer comprising the fluorine-containing copolymer according to any one of claims 1 to 5.

- 35 10. A formed article, comprising the fluorine-containing copolymer according to any one of claims 1 to 5, wherein the formed article is a tube, a film or an electric wire coating.

INTERNATIONAL SEARCH REPORT

International application No.

PCT/JP2022/008442

A. CLASSIFICATION OF SUBJECT MATTER <i>C08F 8/20</i> (2006.01)i; <i>C08F 214/26</i> (2006.01)i; <i>H01B 7/02</i> (2006.01)i; <i>C08J 7/12</i> (2006.01)i FI: C08F214/26; C08F8/20; H01B7/02 Z; C08J7/12 A CEW According to International Patent Classification (IPC) or to both national classification and IPC																
B. FIELDS SEARCHED Minimum documentation searched (classification system followed by classification symbols) C08F8/20; C08F214/26; H01B7/02; C08J7/12 Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched Published examined utility model applications of Japan 1922-1996 Published unexamined utility model applications of Japan 1971-2022 Registered utility model specifications of Japan 1996-2022 Published registered utility model applications of Japan 1994-2022 Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)																
C. DOCUMENTS CONSIDERED TO BE RELEVANT <table border="1"> <thead> <tr> <th>Category*</th> <th>Citation of document, with indication, where appropriate, of the relevant passages</th> <th>Relevant to claim No.</th> </tr> </thead> <tbody> <tr> <td>X</td> <td>WO 2015/104974 A1 (DAIKIN INDUSTRIES, LTD.) 16 July 2015 (2015-07-16) claims, paragraphs [0009], [0023], [0033]</td> <td>1-10</td> </tr> <tr> <td>A</td> <td>JP 2014-28953 A (DAIKIN INDUSTRIES, LTD.) 13 February 2014 (2014-02-13)</td> <td>1-10</td> </tr> <tr> <td>A</td> <td>WO 2005/049661 A1 (DAIKIN INDUSTRIES, LTD.) 02 June 2005 (2005-06-02)</td> <td>1-10</td> </tr> <tr> <td>A</td> <td>JP 2017-503052 A (THE CHEMOURS COMPANY FC, LLC.) 26 January 2017 (2017-01-26)</td> <td>1-10</td> </tr> </tbody> </table>		Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.	X	WO 2015/104974 A1 (DAIKIN INDUSTRIES, LTD.) 16 July 2015 (2015-07-16) claims, paragraphs [0009], [0023], [0033]	1-10	A	JP 2014-28953 A (DAIKIN INDUSTRIES, LTD.) 13 February 2014 (2014-02-13)	1-10	A	WO 2005/049661 A1 (DAIKIN INDUSTRIES, LTD.) 02 June 2005 (2005-06-02)	1-10	A	JP 2017-503052 A (THE CHEMOURS COMPANY FC, LLC.) 26 January 2017 (2017-01-26)	1-10
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.														
X	WO 2015/104974 A1 (DAIKIN INDUSTRIES, LTD.) 16 July 2015 (2015-07-16) claims, paragraphs [0009], [0023], [0033]	1-10														
A	JP 2014-28953 A (DAIKIN INDUSTRIES, LTD.) 13 February 2014 (2014-02-13)	1-10														
A	WO 2005/049661 A1 (DAIKIN INDUSTRIES, LTD.) 02 June 2005 (2005-06-02)	1-10														
A	JP 2017-503052 A (THE CHEMOURS COMPANY FC, LLC.) 26 January 2017 (2017-01-26)	1-10														
<input type="checkbox"/> Further documents are listed in the continuation of Box C. <input checked="" type="checkbox"/> See patent family annex.																
* Special categories of cited documents: "A" document defining the general state of the art which is not considered to be of particular relevance "E" earlier application or patent but published on or after the international filing date "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) "O" document referring to an oral disclosure, use, exhibition or other means "P" document published prior to the international filing date but later than the priority date claimed	"I" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention "X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art "&" document member of the same patent family															
Date of the actual completion of the international search 18 April 2022	Date of mailing of the international search report 10 May 2022															
Name and mailing address of the ISA/JP Japan Patent Office (ISA/JP) 3-4-3 Kasumigaseki, Chiyoda-ku, Tokyo 100-8915 Japan	Authorized officer Telephone No.															

Form PCT/ISA/210 (second sheet) (January 2015)

INTERNATIONAL SEARCH REPORT
Information on patent family members

International application No.
PCT/JP2022/008442

5
 10
 15
 20
 25
 30
 35
 40
 45
 50
 55

Patent document cited in search report			Publication date (day/month/year)	Patent family member(s)			Publication date (day/month/year)
WO	2015/104974	A1	16 July 2015	JP	2015-149274	A	
				US	2016/0322128	A1	
					claims, paragraphs [0014], [0042]-[0044], [0064], [0065]		
				EP	3076405	A1	
				CN	105900186	A	
				CN	110246613	A	
JP	2014-28953	A	13 February 2014	WO	2014/007350	A1	
WO	2005/049661	A1	02 June 2005	US	2007/0112155	A1	
				US	2012/0016089	A1	
				EP	1688442	A1	
				CN	1882614	A	
JP	2017-503052	A	26 January 2017	US	2015/0175757	A1	
				WO	2015/095746	A1	
				CN	105916920	A	

REFERENCES CITED IN THE DESCRIPTION

This list of references cited by the applicant is for the reader's convenience only. It does not form part of the European patent document. Even though great care has been taken in compiling the references, errors or omissions cannot be excluded and the EPO disclaims all liability in this regard.

Patent documents cited in the description

- JP 52109588 A [0003]