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(54) **ACTIVE NOISE CONTROL DEVICE**

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**ABSTRACT**

An active noise control device controls a speaker so as to output a canceling sound for canceling noise transmitted from a vibration source. The active noise control device includes a control signal generating unit configured to perform signal processing on a basic signal corresponding to a predetermined frequency by a feedback filter and an extraction filter, which is an adaptive notch filter, to generate a control signal that control the speaker, a secondary path filter updating unit configured to update sequentially and adaptively a secondary path filter, and a feedback filter setting unit configured to set the feedback filter based on the secondary path filter.

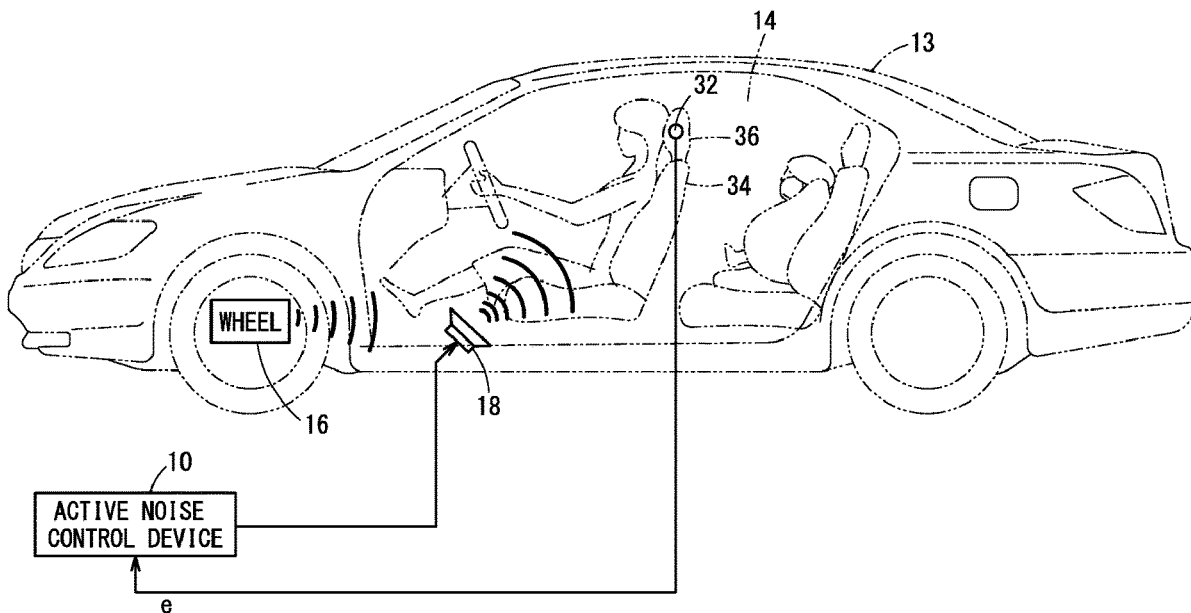


FIG. 1

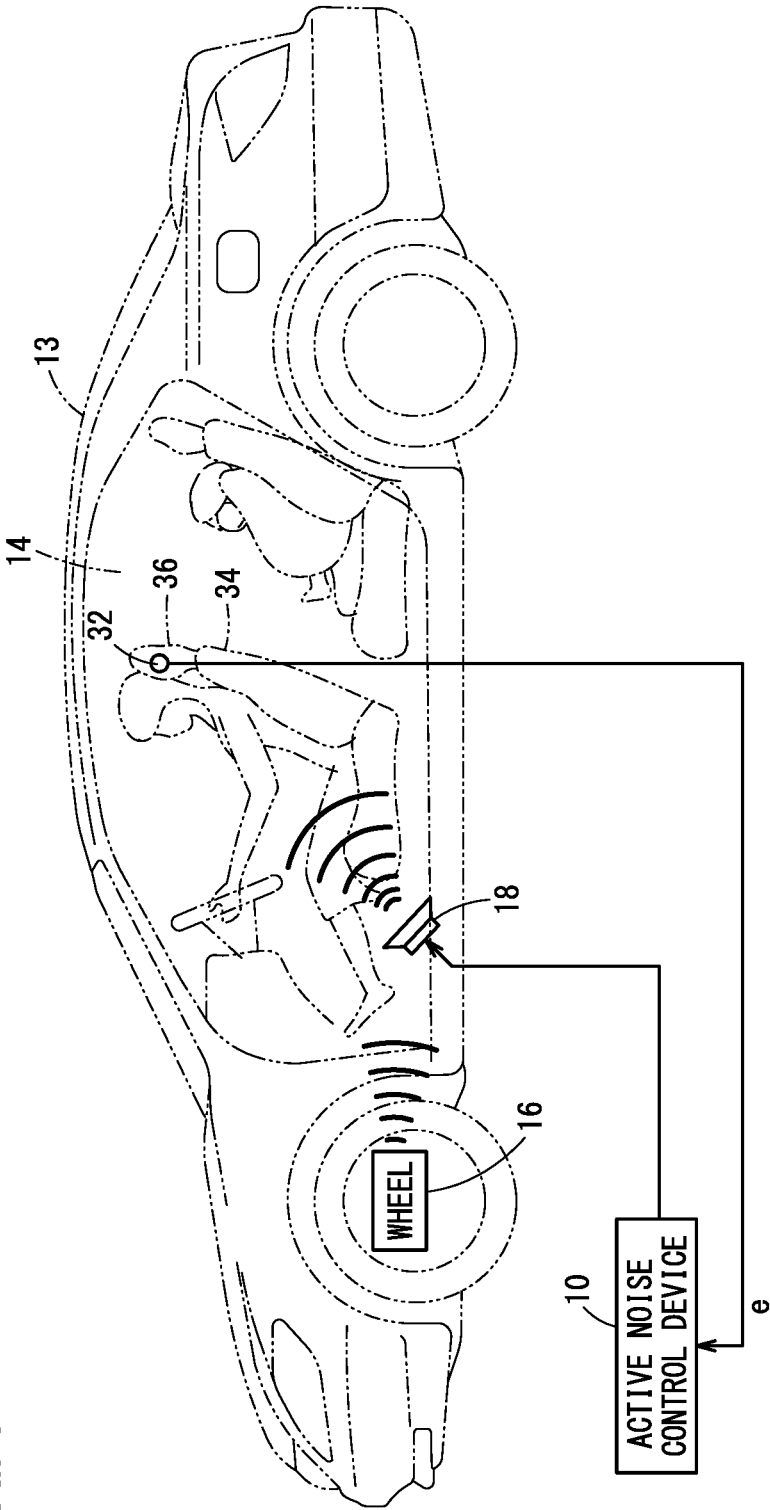
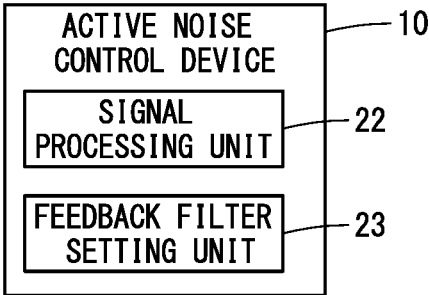
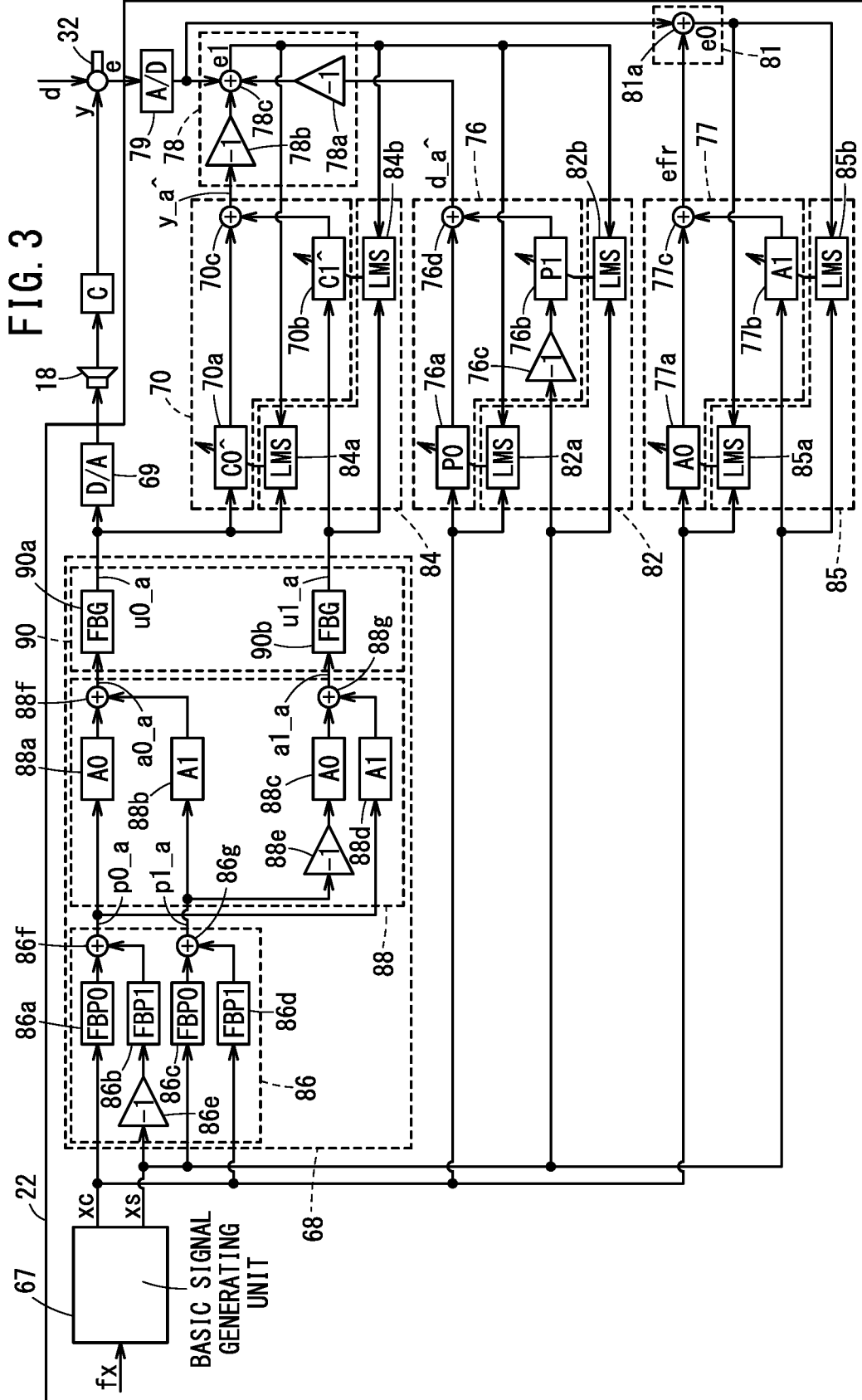
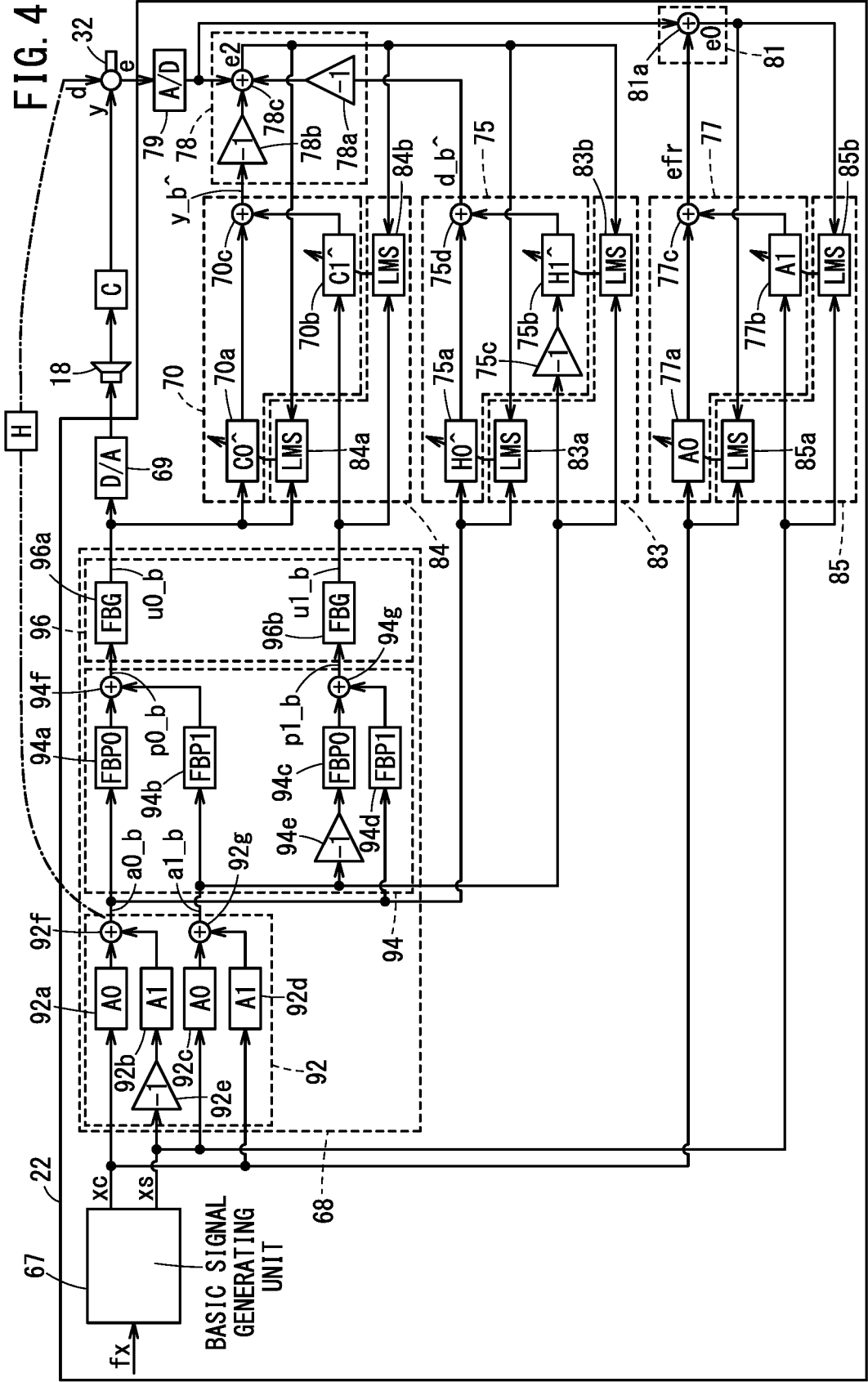


FIG. 2







## ACTIVE NOISE CONTROL DEVICE

### CROSS-REFERENCE TO RELATED APPLICATIONS

[0001] This application is based upon and claims the benefit of priority from Japanese Patent Application No. 2021-044977 filed on Mar. 18, 2021, the contents of which are incorporated herein by reference.

### BACKGROUND OF THE INVENTION

#### Field of the Invention

[0002] The present invention relates to an active noise control device.

#### Description of the Related Art

[0003] JP 2007-025527 A discloses an active noise reduction device. The active noise reduction device generates a signal for controlling a speaker. Thus, an interference sound is output from the speaker. The sound pressure of noise such as road noise is reduced by the interference sound.

### SUMMARY OF THE INVENTION

[0004] An active noise control device as disclosed in JP 2007-025527 A generates a control signal that controls a speaker based on a transfer characteristic between the speaker and a microphone. In the active noise control device, the transfer characteristic between the speaker and the microphone is fixed. Therefore, when the transfer characteristic changes, there are problems such that the active noise control device cannot reduce the sound pressure of the noise.

[0005] An object of the present invention is to solve the above-described problems.

[0006] According to an aspect of the present invention, an active noise control device controls a speaker based on a component of a frequency band around a predetermined frequency of an error signal output from a detector that detects, at a control point, a synthetic sound of a noise transmitted from a vibration source and a canceling sound output from the speaker to cancel the noise, and includes a basic signal generating unit configured to generate a basic signal corresponding to the predetermined frequency, a control signal generating unit configured to perform signal processing on the basic signal by a feedback filter and an extraction filter, which is an adaptive notch filter, to generate a control signal that controls the speaker, an estimated canceling sound signal generating unit configured to perform signal processing on the control signal by a secondary path filter, which is an adaptive notch filter, to generate an estimated canceling sound signal, an extraction signal generating unit configured to perform signal processing on the basic signal by the extraction filter to generate an extraction signal, a virtual error signal generating unit configured to generate a virtual error signal from the error signal and the estimated canceling sound signal, a differential signal generating unit configured to generate a differential signal from the error signal and an extraction signal, a secondary path filter updating unit configured to update sequentially and adaptively the secondary path filter based on the control signal and the virtual error signal in a manner that a magnitude of the virtual error signal is minimized, an extraction filter updating unit configured to update sequen-

tially and adaptively the extraction filter based on the basic signal and the differential signal in a manner that a magnitude of the differential signal is minimized, and a feedback filter setting unit configured to set the feedback filter based on the secondary path filter.

[0007] The active noise control device according to the present invention can reduce noise even if the transfer characteristic changes.

[0008] The above and other objects, features, and advantages of the present invention will become more apparent from the following description when taken in conjunction with the accompanying drawings in which a preferred embodiment of the present invention is shown by way of illustrative example.

### BRIEF DESCRIPTION OF THE DRAWINGS

[0009] FIG. 1 is a diagram illustrating an outline of active noise control executed by an active noise control device;

[0010] FIG. 2 is a schematic diagram illustrating a configuration of an active noise control device;

[0011] FIG. 3 is a control block diagram of a signal processing unit; and

[0012] FIG. 4 is a control block diagram of a signal processing unit.

### DESCRIPTION OF THE INVENTION

#### First Embodiment

[0013] FIG. 1 is a diagram illustrating an outline of active noise control executed by an active noise control device 10.

[0014] A wheel 16 is vibrated by a force received from a road surface when the vehicle travels. This vibration is transmitted to the vehicle body via the suspension, and road noise is generated in a vehicle compartment 14 of a vehicle 13. The road noise has a peak from 40 to 50 Hz. The range of frequencies from 40 to 50 Hz is a range of frequencies excited by acoustic resonance characteristics of a closed space such as the vehicle compartment 14. Narrow band components with a constant bandwidth around the peak frequency produce a roaring sound, also called drumming noise. Drumming noise is likely to cause discomfort to vehicle occupants.

[0015] The active noise control device 10 according to the present embodiment causes a speaker 18 provided in the vehicle compartment 14 to output a canceling sound. Thus, the sound pressure of the drumming noise at a control point in the vehicle compartment 14 is reduced.

[0016] FIG. 2 is a schematic diagram illustrating a configuration of the active noise control device 10. The active noise control device 10 includes a signal processing unit 22 and a feedback filter setting unit 23.

[0017] The active noise control device 10 includes a computation unit and a storage unit (not shown). The signal processing unit 22 and the feedback filter setting unit 23 described above are realized by the computation unit.

[0018] The computation unit may be configured by a processor such as a CPU (Central Processing Unit) or a GPU (Graphics Processing Unit).

[0019] The computation unit includes a determination unit and a control unit which are not illustrated. The determination unit and the control unit are realized by the computation unit executing a program stored in the storage unit.

[0020] At least a part of the determination unit and the control unit may be realized by an integrated circuit such as an ASIC (Application Specific Integrated Circuit) or an FPGA (Field-Programmable Gate Array). In addition, at least a part of the determination unit and the control unit may be configured by an electronic circuit including a discrete device.

[0021] The storage unit can be configured by a volatile memory (not illustrated) and a nonvolatile memory (not illustrated). Examples of the volatile memory include, for example, a RAM (Random Access Memory) or the like. Examples of the nonvolatile memory include, for example, a ROM (Read Only Memory), a flash memory, or the like. Data or the like may be stored, for example, in the volatile memory. Programs, tables, maps, and the like are stored, for example, in the nonvolatile memory. At least a part of the storage unit may be provided in the processor, the integrated circuit, or the like as described above.

#### [Configuration of Signal Processing Unit]

[0022] FIG. 3 is a control block diagram of the signal processing unit 22. The signal processing unit 22 performs feedback signal processing. In the feedback signal processing, a control signal  $u0\_a$  is generated. The control signal  $u0\_a$  is a signal for causing the speaker 18 to output a canceling sound that cancels the drumming noise. The control signal  $u0\_a$  is generated on the basis of an error signal  $e$  output from a microphone 32 provided at the control point. Hereinafter, a sound transfer path from the speaker 18 to the microphone 32 is referred to as a secondary path, and a transfer characteristic of the secondary path is denoted by  $C$ .

[0023] In the present embodiment, the control point is near the ears of the vehicle occupant. For this purpose, as shown in FIG. 1, the microphone 32 is provided at a headrest 36 of a seat 34 in the vehicle compartment 14. The error signal  $e$  is a signal output from the microphone 32 that has detected a synthetic sound of the noise  $d$  at the control point and the canceling sound  $y$  at the control point.

[0024] The signal processing unit 22 includes a basic signal generating unit 67, a control signal generating unit 68, an estimated canceling sound signal generating unit 70, an estimated noise signal generating unit 76, an extraction signal generating unit 77, a virtual error signal generating unit 78, a differential signal generating unit 81, an adjustment filter updating unit 82, a secondary path filter updating unit 84, and an extraction filter updating unit 85.

[0025] The basic signal generating unit 67 generates a basic signal  $x_c (= \cos(2\pi \times f_x \times t))$  and  $x_s (= \sin(2\pi \times f_x \times t))$ . The basic signal  $x_c$  is a cosine signal of a control target frequency  $f_x$ . The basic signal  $x_s$  is a sine signal of the control target frequency  $f_x$ . Here,  $t$  denotes time. The control target frequency  $f_x$  is each set in advance to the peak frequency of the drumming noise and a frequency near the peak frequency.

[0026] The control signal generating unit 68 generates control signals  $u0\_a$  and  $u1\_a$ . The control signals  $u0\_a$  and  $u1\_a$  are generated by performing signal processing on the basic signals  $x_c$  and  $x_s$  by a feedback filter FB and an extraction filter A. The control signal generating unit 68 includes a phase adjusting unit 86, a signal extraction unit 88, and a gain adjusting unit 90.

[0027] The feedback filter FB is indicated by  $FB = FBG(FBP0 + iFBP1)$  using a gain FBG, a filter coefficient FBP0,

and a filter coefficient FBP1. Here,  $i$  denotes an imaginary number. Further,  $FBP0^2 + FBP1^2 = 1$ . The feedback filter FB is set by the feedback filter setting unit 23. The setting of the feedback filter FB will be described later in detail. The extraction filter A will be described in detail together with an extraction signal generating unit 77 described later.

[0028] The phase adjusting unit 86 generates phase adjustment signals  $p0\_a$  and  $p1\_a$ . The phase adjustment signals  $p0\_a$  and  $p1\_a$  are generated by performing signal processing on the basic signals  $x_c$  and  $x_s$  by the phase adjustment filter FBP.

[0029] The phase adjusting unit 86 includes a first phase adjustment filter 86a, a second phase adjustment filter 86b, a third phase adjustment filter 86c, a fourth phase adjustment filter 86d, an inverting amplifier 86e, an adder 86f, and an adder 86g.

[0030] The first phase adjustment filter 86a has the filter coefficient FBP0. The second phase adjustment filter 86b has the filter coefficient FBP1. The third phase adjustment filter 86c has the filter coefficient FBP0. The fourth phase adjustment filter 86d has the filter coefficient FBP1.

[0031] The second phase adjustment filter 86b receives the basic signal  $-x_s$  whose polarity has been inverted by the inverting amplifier 86e. The basic signal  $x_c$  whose amplitude is adjusted by the first phase adjustment filter 86a and the basic signal  $-x_s$  whose amplitude is adjusted by the second phase adjustment filter 86b are added by the adder 86f. Thus, the phase adjustment signal  $p0\_a$  is generated.

[0032] The basic signal  $x_s$  whose amplitude is adjusted by the third phase adjustment filter 86c and the basic signal  $x_c$  whose amplitude is adjusted by the fourth phase adjustment filter 86d are added by the adder 86g. Thus, the phase adjustment signal  $p1\_a$  is generated.

[0033] The signal extraction unit 88 performs signal processing on the phase adjustment signal  $p0\_a$  and the phase adjustment signal  $p1\_a$  using the extraction filter A. Thus, the extraction signals  $a0\_a$  and  $a1\_a$  are generated.

[0034] The signal extraction unit 88 includes a first extraction filter 88a, a second extraction filter 88b, a third extraction filter 88c, a fourth extraction filter 88d, an inverting amplifier 88e, an adder 88f, and an adder 88g.

[0035] The first extraction filter 88a has a filter coefficient A0. The second extraction filter 88b has a filter coefficient A1. The third extraction filter 88c has filter the coefficient A0. The fourth extraction filter 88d has the filter coefficient A1.

[0036] The phase adjustment signal  $p0\_a$  whose amplitude has been adjusted by the first extraction filter 88a and the phase adjustment signal  $p1\_a$  whose amplitude has been adjusted by the second extraction filter 88b are added by the adder 88f. Thus, the extraction signal  $a0\_a$  is regenerated.

[0037] The phase adjustment signal  $-p1\_a$  whose polarity is inverted by the inverting amplifier 88e is input to the third extraction filter 88c. The phase adjustment signal  $-p1\_a$  whose amplitude is adjusted by the third extraction filter 88c and the phase adjustment signal  $p0\_a$  whose amplitude is adjusted by the fourth extraction filter 88d are added by the adder 88g. Thus, an extraction signal  $a1\_a$  is generated.

[0038] The gain adjusting unit 90 performs signal processing on the extraction signals  $a0\_a$  and  $a1\_a$  using the gain filters FBG. Thus, control signals  $u0\_a$  and  $u1\_a$  are generated.

[0039] The gain adjusting unit 90 includes a first gain adjustment filter 90a and a second gain adjustment filter 90b.

The first gain adjustment filter **90a** has the gain FBG. The second gain adjustment filter **90b** has the gain FBG.

**[0040]** The amplitude of the extraction signal  $a0\_a$  is adjusted by the first gain adjustment filter **90a**. Thus, the control signal  $u0\_a$  is generated. The amplitude of the extraction signal  $a1\_a$  is adjusted by the second gain adjustment filter **90b**. Thus, the control signal  $u1\_a$  is generated. The control signal  $u0\_a$  is converted into an analog signal by a digital-to-analog converter **69** and output to the speaker **18**.

**[0041]** In the estimated canceling sound signal generating unit **70** described below, the control signal  $u0\_a$  is used as a real component, and the control signal  $u1\_a$  is used as an imaginary component.

**[0042]** The estimated canceling sound signal generating unit **70** performs signal processing on the control signals  $u0\_a$  and  $u1\_a$  by a secondary path filter  $C^\wedge$ . Thus, an estimated canceling sound signal  $y\_a^\wedge$  is generated.

**[0043]** In the estimated canceling sound signal generating unit **70**, an adaptive notch filter (for example, a SAN (Single-frequency Adaptive Notch) filter) is used as the secondary path filter  $C^\wedge$ . The secondary path filter  $C^\wedge$  is updated by the secondary path filter updating unit **84** described later. As a result, the secondary path filter  $C^\wedge$  converges on the sound transfer characteristic  $C$  in the secondary path. The secondary path filter  $C^\wedge$  is indicated by  $C^\wedge=C0^\wedge+iC1^\wedge$  using filter coefficients  $C0^\wedge$  and  $C1^\wedge$ . Here,  $i$  denotes an imaginary number.

**[0044]** The estimated canceling sound signal generating unit **70** includes a first secondary path filter **70a**, a second secondary path filter **70b**, and an adder **70c**.

**[0045]** The first secondary path filter **70a** has the filter coefficient  $C0^\wedge$ . The second secondary path filter **70b** has the filter coefficient  $C1^\wedge$ . The control signal  $u0\_a$  whose amplitude is adjusted by the first secondary path filter **70a** and the control signal  $u1\_a$  whose amplitude is adjusted by the second secondary path filter **70b** are added by the adder **70c**. Thus, the estimated canceling sound signal  $y\_a^\wedge$  is generated.

**[0046]** The estimated noise signal generating unit **76** performs signal processing on the basic signal  $xc$  and the basic signal  $xs$  by an adjustment filter  $P$ . Thus, an estimated noise signal  $d\_a^\wedge$  is generated. In the estimated noise signal generating unit **76**, an adaptive notch filter (for example, a SAN filter) is used as the adjustment filter  $P$  for adjusting characteristics of the basic signal  $xc$  and the basic signal  $xs$ . The adjustment filter  $P$  is updated by the adjustment filter updating unit **82** described later. The adjustment filter  $P$  is indicated by  $P=P0+iP1$  using a filter coefficient  $P0$  and a filter coefficient  $P1$ . Here,  $i$  denotes an imaginary number.

**[0047]** The estimated noise signal generating unit **76** includes a first adjustment filter **76a**, a second adjustment filter **76b**, an inverting amplifier **76c**, and an adder **76d**. The first adjustment filter **76a** has the filter coefficient  $P0$ . The second adjustment filter **76b** has the filter coefficient  $P1$ .

**[0048]** The second adjustment filter **76b** receives the basic signal  $-xs$  whose polarity has been inverted by the inverting amplifier **76c**. The basic signal  $xc$  whose amplitude is adjusted by the first adjustment filter **76a** and the basic signal  $-xs$  whose amplitude is adjusted by the second adjustment filter **76b** are added by the adder **76d**. Thus, the estimated noise signal  $d\_a^\wedge$  is generated.

**[0049]** The extraction signal generating unit **77** performs signal processing on the basic signal  $xc$  and the basic signal  $xs$  using an extraction filter  $A$ . Thus, an extraction signal  $efr$

is generated. In the extraction signal generating unit **77**, an adaptive notch filter (for example, a SAN filter) is used as the extraction filter  $A$ . The extraction filter  $A$  is updated and optimized by the extraction filter updating unit **85** described later. The extraction filter  $A$  has filter coefficients  $A0$  and  $A1$  which match the basic signals  $xc$  and  $xs$  to the amplitude and phase of the drumming noise.

**[0050]** The extraction signal generating unit **77** includes a first extraction filter **77a**, a second extraction filter **77b**, and an adder **77c**. The first extraction filter **77a** has the filter coefficient  $A0$ . The second extraction filter **77b** has the filter coefficient  $A1$ .

**[0051]** The basic signal  $xc$  whose amplitude is adjusted by the first extraction filter **77a** and the basic signal  $xs$  whose amplitude is adjusted by the second extraction filter **77b** are added by the adder **77c**. Thus, the extraction signal  $efr$  is generated.

**[0052]** The virtual error signal generating unit **78** generates a virtual error signal  $e1$  based on the error signal  $e$ , the estimated noise signal  $d\_a^\wedge$ , and the estimated canceling sound signal  $y\_a^\wedge$ . The virtual error signal generating unit **78** includes an inverting amplifier **78a**, an inverting amplifier **78b**, and an adder **78c**.

**[0053]** The error signal  $e$  converted into a digital signal by an analog-to-digital converter **79**, the estimated noise signal  $-d\_a^\wedge$  whose polarity is inverted by the inverting amplifier **78a**, and the estimated canceling sound signal  $-y\_a^\wedge$  whose polarity is inverted by the inverting amplifier **78b** are added by the adder **78c**. Thus, the virtual error signal  $e1$  is generated.

**[0054]** The differential signal generating unit **81** generates a differential signal  $e0$  based on the error signal  $e$  and the extraction signal  $efr$ . The differential signal generating unit **81** includes an adder **81a**. The error signal  $e$  and the extraction signal  $efr$  are added by the adder **81a**. As a result, the differential signal  $e0$  is generated.

**[0055]** The adjustment filter updating unit **82** sequentially and adaptively updates the adjustment filter  $P$  by an adaptive algorithm (for example, an LMS (Least Mean Square) algorithm) so that the virtual error signal  $e1$  is minimized.

**[0056]** The adjustment filter updating unit **82** includes a first adjustment filter coefficient updating unit **82a** and a second adjustment filter coefficient updating unit **82b**. The first adjustment filter coefficient updating unit **82a** and the second adjustment filter coefficient updating unit **82b** update the filter coefficient  $P0$  and the filter coefficient  $P1$  based on the following expressions. In the expressions,  $n$  denotes the number of time steps (time step number,  $n=0, 1, 2, \dots$ ). The signal processing unit **22** performs signal processing at predetermined periods. The time step indicates the length of each period. The time step number indicates how many periods (times) the signal processing is performed. In the expressions,  $\mu0_P$  and  $\mu1_P$  indicate step size parameters.

$$P0_{n+1}=P0_n-\mu0_P \times e1_n \times xc_n$$

$$P1_{n+1}=P1_n-\mu1_P \times e1_n \times xs_n$$

**[0057]** The secondary path filter updating unit **84** sequentially and adaptively updates the secondary path filter  $C^\wedge$  by an adaptive algorithm (for example, LMS algorithm) so that the virtual error signal  $e1$  is minimized.

**[0058]** The secondary path filter updating unit **84** includes a first secondary path filter coefficient updating unit **84a** and a second secondary path filter coefficient updating unit **84b**. The first secondary path filter coefficient updating unit **84a**



and the second secondary path filter coefficient updating unit **84b** update the filter coefficient  $\hat{C}0$  and the filter coefficient  $\hat{C}1$  based on the following expressions. In the expressions,  $n$  denotes the time step number ( $n=0, 1, 2, \dots$ ), and  $\mu_{0C}$  and  $\mu_{1C}$  denotes step size parameters.

$$C0_{n+1} = C0_n - \mu_{0C} \times e1_n \times u_{0\_a_n}$$

$$C1_{n+1} = C1_n - \mu_{1C} \times e1_n \times u_{1\_a_n}$$

[0059] The extraction filter updating unit **85** sequentially and adaptively updates the extraction filter  $A$  using an adaptive algorithm (for example, an LMS algorithm) so that the differential signal  $e0$  is minimized.

[0060] The extraction filter updating unit **85** includes a first extraction filter coefficient updating unit **85a** and a second extraction filter coefficient updating unit **85b**. The first extraction filter coefficient updating unit **85a** and the second extraction filter coefficient updating unit **85b** update the filter coefficient  $A0$  and the filter coefficient  $A1$  based on the following expressions. In the expressions,  $n$  denotes the time step number ( $n=0, 1, 2, \dots$ ), and  $\mu_{0A}$  and  $\mu_{1A}$  denote step size parameters.

$$A0_{n+1} = A0_n - \mu_{0A} \times e0_n \times xc_n$$

$$A1_{n+1} = A1_n - \mu_{1A} \times e0_n \times xs_n$$

[Setting of Feedback Filter FB]

[0061] The feedback filter setting unit **23** sets the feedback filter  $FB$  based on the secondary path filter  $\hat{C}$ . Hereinafter, setting of the feedback filter  $FB$  will be described.

[0062] A sensitivity function  $S$ , which is a transfer function of the error signal  $e$  and the noise  $d$ , is expressed by the following expression. The sensitivity function  $S$  indicates a reduction amount of noise  $d$ .

$$S = \frac{E}{D} = \frac{1}{1 + C \cdot FB}$$

[0063] In the expression,  $E$  is a frequency characteristic of the error signal  $e$ , and  $D$  is a frequency characteristic of the noise  $d$ . When the secondary path filter  $\hat{C}$  is substituted for the transfer characteristic  $C$  of the secondary path, the feedback filter  $FB$  is expressed by the following expression.

$$FB = \frac{1 - S}{S} \cdot \frac{1}{\hat{C}}$$

[0064] The value of the sensitivity function  $S$  is predetermined. For example, when the acoustic pressure of drumming noise is reduced by approximately 6 dB, the sensitivity function  $S$  is approximately 0.5. When the sensitivity function  $S=0.5$ , the feedback filter setting unit **23** sets the filter coefficient  $FBP0$  to a value obtained by normalizing the real part of  $1/\hat{C}$  with  $1/|\hat{C}|$ , and sets the filter coefficient  $FBP1$  to a value obtained by normalizing the imaginary part of  $1/\hat{C}$  with  $1/|\hat{C}|$ .

[0065] The feedback filter setting unit **23** sets the gain  $FBG$  so as to gradually increase from the initial value to  $1/|\hat{C}|$ . In a state in which the number of updating of the secondary path filter  $\hat{C}$  is small and learning has not progressed, the value of  $1/|\hat{C}|$  may rapidly increase. There-

fore, by gradually increasing the gain  $FBG$ , it is possible to prevent a sound that the vehicle occupant feels uncomfortable from being output from the speaker **18** at a high sound pressure. Here, the initial value of the gain  $FBG$  is not 0, but is set to a value small enough to prevent the speaker **18** from emitting a sound that the vehicle occupant feels uncomfortable. This is because if the initial value of the gain  $FBG$  is set to 0, the learning of the secondary path filter  $\hat{C}$  does not proceed much.

[0066] Further, the feedback filter setting unit **23** may set the gain  $FBG$  to have an initial value when the gain  $|\hat{C}|$  of the secondary path filter  $\hat{C}$  is equal to or smaller than a predetermined value. Since the gain  $FBG$  is set to have the initial value until the learning of the secondary path filter  $\hat{C}$  proceeds, it is possible to prevent the speaker **18** from emitting a sound that the vehicle occupant feels uncomfortable.

[0067] Further, when the amount of change in gain or the amount of change in phase due to the updating of the secondary path filter  $\hat{C}$  is equal to or larger than a predetermined amount, the feedback filter setting unit **23** may return the gain  $FBG$  to the initial value. When the position of the microphone **32** changes, the transfer characteristic  $C$  of the secondary path may change greatly. In this case, the secondary path filter  $\hat{C}$  is relearned. Therefore, by once setting the gain  $FBG$  to have an initial value and gradually increasing the gain  $FBG$  from the initial value to  $1/|\hat{C}|$ , it is possible to prevent a sound that the vehicle occupant feels uncomfortable from being output from the speaker **18** at a high sound pressure.

[Operational Effects]

[0068] In the active noise control device **10** according to the present embodiment, the control signal generating unit **68** performs signal processing on the basic signal  $xc$  and the basic signal  $xs$  by the feedback filter  $FB$  and the extraction filter  $A$ . Thus, the control signal  $u_{0\_a}$  for controlling the speaker **18** is generated. Further, the feedback filter setting unit **23** sets the feedback filter  $FB$  based on the secondary path filter  $\hat{C}$ . Furthermore, the secondary path filter updating unit **84** sequentially and adaptively updates the secondary path filter  $\hat{C}$ . As a result, even when the transfer characteristic  $C$  of the secondary path changes, the secondary path filter  $\hat{C}$  can follow the transfer characteristic  $C$ . As a result, the control signal  $u_{0\_a}$  is generated in accordance with the change in the transfer characteristic  $C$ , so that the sound pressure of drumming noise can be reduced.

[0069] Further, in the active noise control device **10** according to the present embodiment, the feedback filter setting unit **23** sets the feedback filter  $FB$  based on the secondary path filter  $\hat{C}$  and a predetermined noise reduction amount (sensitivity function  $S$ ). As a result, it is possible to reduce the amount of calculation when setting the feedback filter  $FB$ , and to suppress the load on the computation unit.

[0070] In the active noise control device **10** according to the present embodiment, the feedback filter setting unit **23** gradually increases the gain  $FBG$  of the feedback filter  $FB$  from a predetermined initial value to a gain  $1/|\hat{C}|$ . As a result, it is possible to prevent a sound that the vehicle occupant feels uncomfortable from being output from the speaker **18** at a high sound pressure.

[0071] Further, in the active noise control device **10** according to the present embodiment, the feedback filter setting unit **23** sets the gain  $FBG$  of the feedback filter  $FB$

to a predetermined initial value when the gain  $|C^{\wedge}|$  of the secondary path filter  $C^{\wedge}$  is equal to or smaller than a predetermined value. As a result, the gain FBG is set to have the initial value until the learning of the secondary path filter  $C^{\wedge}$  proceeds, and thus it is possible to prevent the speaker **18** from emitting a sound that the vehicle occupant feels uncomfortable.

[0072] Further, in the active noise control device **10** according to the present embodiment, the feedback filter setting unit **23** sets the gain FBG of the feedback filter FB to have a predetermined initial value when the amount of change in the gain of the secondary path filter  $C^{\wedge}$  or the amount of change in the phase of the secondary path filter  $C^{\wedge}$  is equal to or greater than a predetermined amount. As a result, it is possible to prevent a sound that the vehicle occupant feels uncomfortable from being output from the speaker **18** at a high sound pressure.

#### Second Embodiment

[0073] In the active noise control device **10** according to the present embodiment, the configuration of the signal processing unit **22** is partially different from that of the signal processing unit **22** according to the first embodiment. In addition, a method of setting the feedback filter FB by the feedback filter setting unit **23** is different from the feedback filter setting unit **23** of the first embodiment.

#### [Configuration of Signal Processing Unit]

[0074] The signal processing unit **22** performs feedback signal processing. In the feedback signal processing, a control signal  $u0\_b$  is generated. The control signal  $u0\_b$  is a signal for causing the speaker **18** to output a canceling sound that cancels the drumming noise. The control signal  $u0\_b$  is generated on the basis of an error signal  $e$  output from the microphone **32** provided at the control point. Hereinafter, a sound transfer path from the wheel **16** to the microphone **32** is referred to as a primary path, and a transfer characteristic of the primary path is denoted by  $H$ . Further, a sound transfer path from the speaker **18** to the microphone **32** is referred to as a secondary path, and a transfer characteristic of the secondary path is denoted by  $C$ .

[0075] FIG. 4 is a control block diagram of the signal processing unit **22**. The signal processing unit **22** includes a basic signal generating unit **67**, a control signal generating unit **68**, an estimated canceling sound signal generating unit **70**, an estimated noise signal generating unit **75**, an extraction signal generating unit **77**, a virtual error signal generating unit **78**, a differential signal generating unit **81**, a primary path filter updating unit **83**, a secondary path filter updating unit **84**, and an extraction filter updating unit **85**.

[0076] The basic signal generating unit **67** generates basic signals  $xc (= \cos(2\pi \times fx \times t))$  and  $xs (= \sin(2\pi \times fx \times t))$ . The basic signal  $xc$  is a cosine signal of the control target frequency  $fx$ . The basic signal  $xs$  is a sine signal of the control target frequency  $fx$ . Here,  $t$  denotes time. The control target frequency  $fx$  is set near the peak frequency of the drumming noise in advance.

[0077] The control signal generating unit **68** performs signal processing on the basic signal  $xc$  and the basic signal  $xs$  by the feedback filter FB and the extraction filter A. Thus, the control signals  $u0\_b$  and  $u1\_b$  are generated. The control signal generating unit **68** includes a signal extraction unit **92**, a phase adjusting unit **94**, and a gain adjusting unit **96**.

[0078] The feedback filter FB is indicated by  $FB = FBG(FBP0 + iFBP1)$  using the gain FBG, a filter coefficient FBP0, and a filter coefficient FBP1. Here,  $i$  denotes an imaginary number. Further,  $FBP0^2 + FBP1^2 = 1$ . The feedback filter FB is set by the feedback filter setting unit **23**. The setting of the feedback filter FB will be described later in detail.

[0079] The signal extraction unit **92** performs signal processing on the basic signal  $xc$  and the basic signal  $xs$  by an extraction filter A. Thus, the extraction signals  $a0\_b$  and  $a1\_b$  are generated.

[0080] The signal extraction unit **92** includes a first extraction filter **92a**, a second extraction filter **92b**, a third extraction filter **92c**, a fourth extraction filter **92d**, an inverting amplifier **92e**, an adder **92f**, and an adder **92g**.

[0081] The first extraction filter **92a** has a filter coefficient A0. The second extraction filter **92b** has a filter coefficient A1. The third extraction filter **92c** has the filter coefficient A0. The fourth extraction filter **92d** has the filter coefficient A1.

[0082] The second extraction filter **92b** receives the basic signal  $-xs$  whose polarity is inverted by the inverting amplifier **92e**. The basic signal  $xc$  whose amplitude is adjusted by the first extraction filter **92a** and the basic signal  $-xs$  whose amplitude is adjusted by the second extraction filter **92b** are added by the adder **92f**. Thus, the extraction signal  $a0\_b$  is generated.

[0083] The basic signal  $xs$  whose amplitude is adjusted by the third extraction filter **92c** and the basic signal  $xc$  whose amplitude is adjusted by the fourth extraction filter **92d** are added by the adder **92g**. Thus, the extraction signal  $a1\_b$  is generated.

[0084] The phase adjusting unit **94** performs signal processing on the extraction signals  $a0\_b$  and  $a1\_b$  by the phase adjustment filter FB. As a result, the phase adjustment signals  $p0\_b$  and  $p1\_b$  are generated.

[0085] The phase adjusting unit **94** includes a first phase adjustment filter **94a**, a second phase adjustment filter **94b**, a third phase adjustment filter **94c**, a fourth phase adjustment filter **94d**, an inverting amplifier **94e**, an adder **94f**, and an adder **94g**.

[0086] The first phase adjustment filter **94a** has a filter coefficient FBP0. The second phase adjustment filter **94b** has a filter coefficient FBP1. The third phase adjustment filter **94c** has the filter coefficient FBP0. The fourth phase adjustment filter **94d** has the filter coefficient FBP1.

[0087] The extraction signal  $a0\_b$  whose amplitude is adjusted by the first phase adjustment filter **94a** and the extraction signal  $a1\_b$  whose amplitude is adjusted by the second phase adjustment filter **94b** are added in the adder **94f**. Thus, the phase adjustment signal  $p0\_b$  is generated.

[0088] The third phase adjustment filter **94c** receives the extraction signal  $-a1\_b$  whose polarity is inverted by the inverting amplifier **94e**. The extracted signal  $-a1\_b$  whose amplitude is adjusted by the third phase adjustment filter **94c** and the extraction signal  $a0\_b$  whose amplitude is adjusted by the fourth phase adjustment filter **94d** are added by the adder **94g**. Thus, the phase adjustment signal  $p1\_b$  is generated.

[0089] The gain adjusting unit **96** performs signal processing on the phase adjustment signals  $p0\_b$  and  $p1\_b$  by the gain filter FBG. Thus, the control signals  $u0\_b$  and  $u1\_b$  are generated.

[0090] The gain adjusting unit **96** includes a first gain adjustment filter **96a** and a second gain adjustment filter **96b**.

The first gain adjustment filter **96a** has a gain FBG. The second gain adjustment filter **96b** has the gain FBG.

**[0091]** The amplitude of the phase adjustment signal  $p0\_b$  is adjusted by the first gain adjustment filter **96a**. Thus, the control signal  $u0\_b$  is generated. The amplitude of the phase adjustment signal  $p1\_b$  is adjusted by the second gain adjustment filter **96b**. Thus, the control signal  $u1\_b$  is generated. The control signal  $u0\_b$  is converted into an analog signal by the digital-to-analog converter **69** and output to the speaker **18**.

**[0092]** In the estimated canceling sound signal generating unit **70** described below, the control signal  $u0\_b$  is used as a real component, and the control signal  $u1\_b$  is used as an imaginary component.

**[0093]** The estimated canceling sound signal generating unit **70** performs signal processing on the control signals  $u0\_b$  and  $u1\_b$  by a secondary path filter  $C^\wedge$ . Thus, the estimated canceling sound signal  $y\_b^\wedge$  is generated.

**[0094]** In the estimated canceling sound signal generating unit **70**, an adaptive notch filter (for example, a SAN filter) is used as the secondary path filter  $C^\wedge$ . The secondary path filter  $C^\wedge$  is updated by the secondary path filter updating unit **84**, which will be described later, so as to converge on a sound transfer characteristic  $C$  of the secondary path. The secondary path filter  $C^\wedge$  is indicated by  $C^\wedge=C0^\wedge+iC1^\wedge$  using the filter coefficients  $C0^\wedge$  and  $C1^\wedge$ . Here,  $i$  denotes an imaginary number.

**[0095]** The estimated canceling sound signal generating unit **70** includes a first secondary path filter **70a**, a second secondary path filter **70b**, and an adder **70c**.

**[0096]** The first secondary path filter **70a** has a filter coefficient  $C0^\wedge$ . The second secondary path filter **70b** has a filter coefficient  $C1^\wedge$ . The control signal  $u0\_b$  whose amplitude is adjusted by the first secondary path filter **70a** and the control signal  $u1\_b$  whose amplitude is adjusted by the second secondary path filter **70b** are added by the adder **70c**. Thus, the estimated canceling sound signal  $y\_b^\wedge$  is generated.

**[0097]** The estimated noise signal generating unit **75** performs signal processing on the extraction signals  $a0\_b$  and  $a1\_b$  by a primary path filter  $H^\wedge$ . As a result, an estimated noise signal  $d\_b^\wedge$  is generated.

**[0098]** In the estimated noise signal generating unit **75**, an adaptive notch filter (for example, a SAN filter) is used as the primary path filter  $H^\wedge$ . The primary path filter  $H^\wedge$  is updated by the primary path filter updating unit **83**, which will be described later, so as to converge on a sound transfer characteristic  $H$  of the primary path. The primary path filter  $H^\wedge$  is indicated by  $H^\wedge=H0^\wedge+iH1^\wedge$  using the filter coefficients  $H0^\wedge$  and  $H1^\wedge$ . Here,  $i$  denotes an imaginary number.

**[0099]** The estimated noise signal generating unit **75** includes a first primary path filter **75a**, a second primary path filter **75b**, an inverting amplifier **75c**, and an adder **75d**. The first primary path filter **75a** has a filter coefficient  $H0^\wedge$ . The second primary path filter **75b** has a filter coefficients  $H1^\wedge$ .

**[0100]** The second primary path filter **75b** receives the extraction signal  $-a1\_b$  whose polarity is inverted by the inverting amplifier **75c**. The extracted signal  $a0\_b$  whose amplitude is adjusted by the first primary path filter **75a** and the extraction signal  $-a1\_b$  whose amplitude is adjusted by the second primary path filter **75b** are added by the adder **75d**. As a result, an estimated noise signal  $d\_b^\wedge$  is generated.

**[0101]** The extraction signal generating unit **77** performs signal processing on the basic signal  $xc$  and the basic signal

$xs$  by an extraction filter  $A$ . Thus, an extraction signal  $efr$  is generated. In the extraction signal generating unit **77**, an adaptive notch filter (for example, a SAN filter) is used as the extraction filter  $A$ . The extraction filter  $A$  is updated and optimized by the extraction filter updating unit **85** described later. The extraction filter  $A$  has filter coefficients  $A0$  and  $A1$  which match the basic signals  $xc$  and  $xs$  to the amplitude and phase of the drumming noise.

**[0102]** The extraction signal generating unit **77** includes a first extraction filter **77a**, a second extraction filter **77b**, and an adder **77c**. The first extraction filter **77a** has the filter coefficient  $A0$ . The second extraction filter **77b** has the filter coefficient  $A1$ .

**[0103]** The basic signal  $xc$  whose amplitude is adjusted by the first extraction filter **77a** and the basic signal  $xs$  whose amplitude is adjusted by the second extraction filter **77b** are added by the adder **77c**. Thus, an extraction signal  $efr$  is generated.

**[0104]** The virtual error signal generating unit **78** generates a virtual error signal  $e2$  based on the error signal  $e$ , the estimated noise signal  $d\_b^\wedge$ , and the estimated canceling sound signal  $y\_b^\wedge$ . The virtual error signal generating unit **78** includes an inverting amplifier **78a**, an inverting amplifier **78b**, and an adder **78c**.

**[0105]** The error signal  $e$  converted into a digital signal by an analog-to-digital converter **79**, the estimated noise signal  $-d\_b^\wedge$  whose polarity is inverted by the inverting amplifier **78a**, and the estimated canceling sound signal  $-y\_b^\wedge$  whose polarity is inverted by the inverting amplifier **78b** is added by the adder **78c**. Thus, the virtual error signal  $e2$  is generated.

**[0106]** The differential signal generating unit **81** generates a differential signal  $e0$  based on the error signal  $e$  and the extraction signal  $efr$ . The differential signal generating unit **81** includes an adder **81a**. The error signal  $e$  and the extraction signal  $efr$  are added by the adder **81a** to generate the differential signal  $e0$ .

**[0107]** The primary path filter updating unit **83** sequentially and adaptively updates the primary path filter  $H^\wedge$  by an adaptive algorithm (for example, an LMS algorithm) so that the virtual error signal  $e2$  is minimized.

**[0108]** The primary path filter updating unit **83** includes a first primary path filter coefficient updating unit **83a** and a second primary path filter coefficient updating unit **83b**. The first primary path filter coefficient updating unit **83a** and the second primary path filter coefficient updating unit **83b** update the filter coefficient  $H0^\wedge$  and the filter coefficient  $H1^\wedge$  based on the following expressions. In the expressions,  $n$  denotes the time step number ( $n=0, 1, 2, \dots$ ), and  $\mu0_H$  and  $\mu1_H$  denote step size parameters.

$$H0^\wedge_{n+1}=H0^\wedge_n-\mu0_H \times e2_n \times a0\_b_n$$

$$H1^\wedge_{n+1}=H1^\wedge_n-\mu1_H \times e2_n \times a1\_b_n$$

**[0109]** The secondary path filter updating unit **84** sequentially and adaptively updates the secondary path filter  $C^\wedge$  by an adaptive algorithm (for example, LMS algorithm) so that the virtual error signal  $e2$  is minimized.

**[0110]** The secondary path filter updating unit **84** includes a first secondary path filter coefficient updating unit **84a** and a second secondary path filter coefficient updating unit **84b**. The first secondary path filter coefficient updating unit **84a** and the second secondary path filter coefficient updating unit **84b** update the filter coefficient  $C0^\wedge$  and the filter coefficient  $C1^\wedge$  based on the following expressions. In the expressions,

$n$  denotes the time step number ( $n=0, 1, 2, \dots$ ), and  $\mu 0_C$  and  $\mu 1_C$  denotes step size parameters.

$$C0_{n+1} = C0_n - \mu 0_C \times e 2_n \times u 0_b_n$$

$$C1_{n+1} = C1_n - \mu 1_C \times e 2_n \times u 1_b_n$$

[0111] The extraction filter updating unit 85 sequentially and adaptively updates the extraction filter A using an adaptive algorithm (for example, an LMS algorithm) so that the differential signal  $e 0$  is minimized.

[0112] The extraction filter updating unit 85 includes a first extraction filter coefficient updating unit 85a and a second extraction filter coefficient updating unit 85b. The first extraction filter coefficient updating unit 85a and the second extraction filter coefficient updating unit 85b update the filter coefficient A0 and the filter coefficient A1 based on the following expressions. In the expressions,  $n$  denotes the time step number ( $n=0, 1, 2, \dots$ ), and  $\mu 0_A$  and  $\mu 1_A$  denote step size parameters.

$$A0_{n+1} = A0_n - \mu 0_A \times e 0_n \times x c_n$$

$$A1_{n+1} = A1_n - \mu 1_A \times e 0_n \times x s_n$$

[Setting of Feedback Filter FB]

[0113] The feedback filter setting unit 23 sets the feedback filter FB based on the primary path filter  $H^$  and the secondary path filter  $C^$ . Hereinafter, setting of the feedback filter FB will be described.

[0114] When the primary path filter  $H^$  converges on the transfer characteristic  $H$  of the primary path and the secondary path filter  $C^$  converges on the transfer characteristic  $C$  of the secondary path, the primary path filter  $H^$  is expressed by the following expression.

$$H^ = C^ \cdot FB$$

[0115] When this expression is solved for the feedback filter FB, the feedback filter FB is expressed by the following expression.

$$FB = H^ / C^$$

[0116] The feedback filter setting unit 23 sets the filter coefficient FBP0 to a value obtained by normalizing the real part of  $H^ / C^$  with  $|H^ / C^|$ . The feedback filter setting unit 23 sets the filter coefficient FBP1 to a value obtained by normalizing the imaginary part of  $H^ / C^$  with  $|H^ / C^|$ .

[0117] The feedback filter setting unit 23 gradually increases the gain FBG from the initial value to  $|1 / C^|$ . In a state where the number of updating of the primary path filter  $H^$  and the secondary path filter  $C^$  is small and learning has not progressed, the value of  $|1 / C^|$  may rapidly increase. Therefore, by gradually increasing the gain FBG, it is possible to prevent a sound that the vehicle occupant feels uncomfortable from being output from the speaker 18 at a high sound pressure. Here, the initial value of the gain FBG is not 0, but is set to a value small enough to prevent the speaker 18 from emitting a sound that the vehicle occupant feels uncomfortable. This is because if the initial value of the gain FBG is set to 0, the learning of the secondary path filter  $C^$  does not proceed much.

[0118] The feedback filter setting unit 23 may set the gain FBG to an initial value when the gain  $|H^|$  of the primary path filter  $H^$  or the gain  $|C^|$  of the secondary path filter  $C^$  is equal to or less than a predetermined value. Since the gain FBG is set to the initial value until the learning of the

primary path filter  $H^$  and the secondary path filter  $C^$  proceeds, it is possible to prevent the speaker 18 from emitting a sound that the vehicle occupant feels uncomfortable.

[0119] When at least one of the following four conditions is satisfied, the feedback filter setting unit 23 may return the gain FBG to the initial value. The four conditions are the following (1) to (4).

[0120] (1) The amount of change in gain due to the updating of the primary path filter  $H^$  is equal to or greater than a predetermined amount.

[0121] (2) The amount of change in phase due to the updating of the primary path filter  $H^$  is equal to or greater than a predetermined amount.

[0122] (3) The amount of change in gain due to the updating of the secondary path filter  $C^$  is equal to or greater than a predetermined amount.

[0123] (4) The amount of change in phase due to the updating of the secondary path filter  $C^$  is equal to or greater than a predetermined amount.

[0124] When the position of the microphone 32 changes, the transfer characteristic  $C$  of the secondary path may change greatly. In this case, the secondary path filter  $C^$  is relearned. Then, by once setting the gain FBG to have an initial value and gradually increasing the gain FBG from the initial value to  $|H^ / C^|$ , it is possible to prevent a sound that the vehicle occupant feels uncomfortable from being output from the speaker 18 at a high sound pressure.

[Advantageous Effects]

[0125] In the active noise control device 10 according to the present embodiment, the control signal generating unit 68 performs signal processing on the basic signal  $x c$  and the basic signal  $x s$  by the feedback filter FB and the extraction filter A. Thus, the control signal  $u 0_b$  for controlling the speaker 18 is generated. Further, the feedback filter setting unit 23 sets the feedback filter FB based on the secondary path filter  $C^$ . Furthermore, the secondary path filter updating unit 84 sequentially and adaptively updates the secondary path filter  $C^$ . As a result, even when the transfer characteristic  $C$  of the secondary path changes, the secondary path filter  $C^$  can follow the transfer characteristic  $C$ . As a result, the control signal  $u 0_b$  can be generated in accordance with the change in the transfer characteristic  $C$ , so that the sound pressure of drumming noise can be reduced.

[0126] In the active noise control device 10 according to the present embodiment, the feedback filter setting unit 23 sets the feedback filter FB based on the primary path filter  $H^$  and the secondary path filter  $C^$ . As a result, it is possible to reduce the amount of calculation when setting the feedback filter FB, and to suppress the load on the computation unit.

[Technical Concepts Obtained from Embodiments]

[0127] A description will be given below concerning technical concepts that are capable of being grasped from the above-described embodiments.

[0128] The active noise control device (10) controls the speaker (18) based on a component of a frequency band around a predetermined frequency of an error signal output from the detector (32) that detects, at a control point, a synthetic sound of a noise transmitted from a vibration source and a canceling sound output from the speaker to cancel the noise, and includes the basic signal generating unit (67) configured to generate a basic signal corresponding

to the predetermined frequency, the control signal generating unit (68) configured to perform signal processing on the basic signal by a feedback filter and an extraction filter, which is an adaptive notch filter, to generate a control signal that controls the speaker, the estimated canceling sound signal generating unit (70) configured to perform signal processing on the control signal by a secondary path filter, which is an adaptive notch filter, to generate an estimated canceling sound signal, the extraction signal generating unit (77) configured to perform signal processing on the basic signal by the extraction filter to generate an extraction signal, the virtual error signal generating unit (78) configured to generate a virtual error signal from the error signal and the estimated canceling sound signal, the differential signal generating unit (81) configured to generate a differential signal from the error signal and the extraction signal, the secondary path filter updating unit (84) configured to update sequentially and adaptively the secondary path filter based on the control signal and the virtual error signal in a manner that a magnitude of the virtual error signal is minimized, the extraction filter updating unit (85) configured to update sequentially and adaptively the extraction filter based on the basic signal and the differential signal in a manner that a magnitude of the differential signal is minimized, and the feedback filter setting unit (23) configured to set the feedback filter based on the secondary path filter.

**[0129]** In the above active noise control device, the feedback filter setting unit may increase a gain of the feedback filter gradually from a predetermined initial value.

**[0130]** In the above active noise control device, the feedback filter setting unit may set a gain of the feedback filter to a predetermined initial value when a gain of the secondary path filter is equal to or less than a predetermined value.

**[0131]** In the above active noise control device, the feedback filter setting unit may set a gain of the feedback filter to a predetermined initial value when an amount of change in gain or an amount of change in phase of the secondary path filter is equal to or greater than a predetermined amount.

**[0132]** In the above active noise control device, the feedback filter setting unit may set the feedback filter based on the secondary path filter and a predetermined noise reduction amount.

**[0133]** The active noise control device may further include the estimated noise signal generating unit (75) configured to perform signal processing on the extraction signal by a primary path filter, which is an adaptive notch filter, to generate an estimated noise signal, and the primary path filter updating unit (83) configured to update the primary path filter based on the basic signal and the virtual error signal in a manner that the magnitude of the virtual error signal is minimized, wherein the virtual error signal generating unit may generate the virtual error signal from the error signal, the estimated noise signal, and the estimated canceling sound signal, and the feedback filter setting unit may calculate the feedback filter from the primary path filter and the secondary path filter.

**[0134]** The present invention is not particularly limited to the embodiments described above, and various modifications are possible without departing from the essence and gist of the present invention.

What is claimed is:

1. An active noise control device that controls a speaker based on a component of a frequency band around a predetermined frequency of an error signal output from a detector that detects, at a control point, a synthetic sound of a noise transmitted from a vibration source and a canceling sound output from the speaker to cancel the noise, the active noise control device comprising one or more processors that execute computer-executable instructions stored in a memory, wherein the one or more processors execute the computer-executable instructions to cause the active noise control device to:

- generate a basic signal corresponding to the predetermined frequency;
- perform signal processing on the basic signal by a feedback filter and an extraction filter, which is an adaptive notch filter, to generate a control signal that controls the speaker;
- perform signal processing on the control signal by a secondary path filter, which is an adaptive notch filter, to generate an estimated canceling sound signal;
- perform signal processing on the basic signal by the extraction filter to generate an extraction signal;
- generate a virtual error signal from the error signal and the estimated canceling sound signal;
- generate a differential signal from the error signal and the extraction signal;
- update sequentially and adaptively the secondary path filter based on the control signal and the virtual error signal in a manner that a magnitude of the virtual error signal is minimized;
- update sequentially and adaptively the extraction filter based on the basic signal and the differential signal in a manner that a magnitude of the differential signal is minimized; and
- set the feedback filter based on the secondary path filter.

2. The active noise control device according to claim 1, wherein the one or more processors cause the active noise control device to increase a gain of the feedback filter gradually from a predetermined initial value.

3. The active noise control device according to claim 1, wherein the one or more processors cause the active noise control device to set a gain of the feedback filter to a predetermined initial value when a gain of the secondary path filter is equal to or less than a predetermined value.

4. The active noise control device according to claim 1, wherein the one or more processors cause the active noise control device to set a gain of the feedback filter to a predetermined initial value when an amount of change in gain or an amount of change in phase of the secondary path filter is equal to or greater than a predetermined amount.

5. The active noise control device according to claim 1, wherein the one or more processors cause the active noise control device to set the feedback filter based on the secondary path filter and a predetermined noise reduction amount.

6. The active noise control device according to claim 1, wherein the one or more processors cause the active noise control device to:

- perform signal processing on the extraction signal by a primary path filter, which is an adaptive notch filter, to generate an estimated noise signal;
- update the primary path filter based on the basic signal and the virtual error signal in a manner that the magnitude of the virtual error signal is minimized;

generate the virtual error signal from the error signal, the estimated noise signal, and the estimated canceling sound signal; and  
calculate the feedback filter from the primary path filter and the secondary path filter.

\* \* \* \* \*