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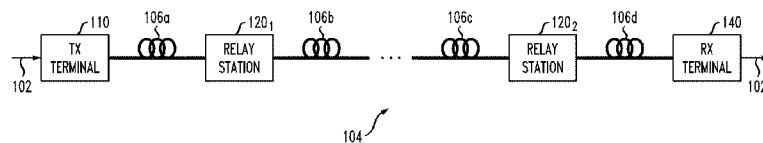
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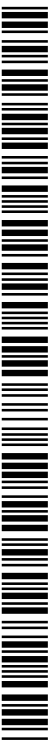
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- (54) Title: OPTICAL SYSTEM FOR SIGNAL AMPLIFICATION USING A MULTIMODE FIBER

FIG. 1  
100



- (57) Abstract: An optical coupler for coupling optical-pump power into a multimode fiber configured to transport an optical space-division-multiplexed (SDM) signal, the coupling being performed in a manner that enables amplification of the SDM signal in the multimode fiber via a stimulated-emission process or a stimulated Raman-scattering process. The optical coupler can be a part of an optical transmitter configured for co-directional pumping, an optical receiver configured for contra-directional pumping, or a relay station disposed within an optical communication link and configured for either type of pumping. The optical coupler can advantageously be used, e.g., to offset the different degrees of attenuation to which the SDM-signal components corresponding to different guided modes of the multimode fiber are subjected to therein.



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## OPTICAL SYSTEM FOR SIGNAL AMPLIFICATION USING A MULTIMODE FIBER

### CROSS-REFERENCE TO RELATED APPLICATIONS

5           The subject matter of this application is related to that of U.S. Patent Application No. 13/200,072, by Roland Ryf, attorney docket reference 810270, filed on the same date as the present application, and entitled "OPTICAL MODE COUPLERS FOR MULTI-MODE OPTICAL FIBERS," which is incorporated herein by reference in its entirety.

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### BACKGROUND

#### Field of the Invention

The present invention relates to optical equipment and, more specifically but not exclusively, to optical fiber amplifiers.

15

#### Description of the Related Art

This section introduces aspects that may help facilitate a better understanding of the invention(s). Accordingly, the statements of this section are to be read in this light and are not to be understood as admissions about what is in the prior art or what is not in the prior art.

20

An optical amplifier is a device that amplifies an optical signal directly in the optical domain without converting the optical signal into a corresponding electrical signal. Optical amplifiers are widely used, for example, in the fields of optical communications and laser physics.

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One type of an optical amplifier is a doped-fiber amplifier, with a well-known example being the Erbium-doped fiber amplifier (EDFA). In operation, a signal to be amplified and a pump beam are multiplexed into the doped fiber. The pump beam excites the doping ions, and amplification of the signal is achieved by stimulated emission of photons from the excited dopant ions.

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Another type of an optical amplifier is a Raman amplifier, which relies on stimulated Raman scattering (SRS) for signal amplification. More specifically, when a signal to be amplified and a pump beam are multiplexed into an optical fiber made

of an appropriate material, a lower-frequency signal photon induces SRS of a higher-frequency pump photon, which causes the pump photon to pass some of its energy to the vibrational states of the fiber material, thereby converting the pump photon into an additional signal photon. The pump beam may be coupled into the fiber in the same  
5 direction as the signal (co-directional pumping) or in the opposite direction (contra-directional pumping).

### SUMMARY

Disclosed herein are various embodiments of an optical coupler for coupling  
10 optical-pump power into a multimode fiber configured to transport an optical space-division-multiplexed (SDM) signal, said coupling being performed in a manner that enables amplification of the SDM signal in the multimode fiber via, for example, a stimulated-emission process or a stimulated Raman-scattering process. The optical coupler can be, for example, a part of an optical transmitter configured for co-  
15 directional pumping, an optical receiver configured for contra-directional pumping, or a relay station disposed within an optical communication link and configured for either type of pumping. The optical coupler can advantageously be used, e.g., to offset the different degrees of attenuation to which the SDM-signal components corresponding to different guided modes of the multimode fiber are subjected to  
20 therein.

According to one embodiment, provided is an apparatus comprising a first optical coupler that is configured to pass an optical beam carrying an optical signal corresponding to a set of guided modes of a first multimode fiber and couple optical-pump power into the first multimode fiber so as to partition the optical-pump power  
25 among the guided modes of said set.

In some embodiments of the above apparatus, the apparatus may further comprise a segment of the first multimode fiber.

In some embodiments of any of the above apparatus, the segment of the first multimode fiber may be adapted to transfer optical-pump energy to the optical signal  
30 via a stimulated Raman-scattering process.

In some embodiments of any of the above apparatus, the segment of the first multimode fiber may be adapted to transfer optical-pump energy to the optical signal via a stimulated emission process.

5 In some embodiments of any of the above apparatus, the guided modes may comprise a fundamental mode and a higher-order mode; and the first optical coupler may be configured to couple a greater portion of the optical-pump power into the higher-order mode than into the fundamental mode.

10 In some embodiments of any of the above apparatus, the first optical coupler may comprise a phase mask configured to phase-filter a first optical-pump beam to generate a first phase-filtered beam whose phase varies over a transverse cross section thereof; and the first optical coupler may be configured to apply the first phase-filtered beam to an end of the first multimode fiber.

15 In some embodiments of any of the above apparatus, the first optical coupler may further comprise a beam combiner configured to spatially overlap the first phase-filtered beam and the optical beam carrying the optical signal.

In some embodiments of any of the above apparatus, the first optical coupler may further comprise a polarization scrambler configured to cause the first optical-pump beam to have scrambled polarization.

20 In some embodiments of any of the above apparatus, the first optical coupler may further comprises an array of waveguides, wherein a first waveguide of the array is configured to output the first optical-pump beam; and a second waveguide of the array is configured to output a second optical-pump beam; the phase mask may be further configured to phase-filter the second optical-pump beam to generate a second phase-filtered beam whose phase varies over a transverse cross section thereof; and  
25 the first optical coupler may be further configured to apply the second phase-filtered beam to the end of the first multimode fiber.

In some embodiments of any of the above apparatus, the first optical coupler may be configured to apply the second phase-filtered beam to a substantially separate region on said end than the first phase-filtered beam.

30 In some embodiments of any of the above apparatus, the apparatus may further comprise an optical-pump source configured to cause the first optical-pump

beam to have a first wavelength, and to cause the second optical-pump beam to have a second wavelength different from the first wavelength.

In some embodiments of any of the above apparatus, the first optical coupler may further comprise an adjustable mechanical structure reconfigurable to change a relative position of the first optical-pump beam and the phase mask.

In some embodiments of any of the above apparatus, the first optical coupler may further comprise at least one of: a module including a bulk optical element and a mechanically adjustable element configured to change location of a spot illuminated by the first phase-filtered beam on said end; and a module including a bulk optical element and a mechanically adjustable element for changing a size of said spot.

In some embodiments of any of the above apparatus, the optical phase mask may comprise: a first area configured to impose a first constant phase shift on light propagating therethrough; and a second area configured to impose a second constant phase shift on light propagating therethrough, wherein the second phase shift is different from the first phase shift.

In some embodiments of any of the above apparatus, the apparatus may comprise an optical receiver, wherein the first optical coupler is a part of the receiver.

In some embodiments of any of the above apparatus, the apparatus may comprise an optical transmitter, wherein the first optical coupler is a part of the transmitter.

In some embodiments of any of the above apparatus, the apparatus may comprise a fiber amplifier, wherein the first optical coupler is a part of the fiber amplifier.

In some embodiments of any of the above apparatus, the apparatus may comprise a relay station adapted to transport the optical beam carrying the optical signal between said end of the first multimode fiber and an end of a second multimode fiber, wherein the first optical coupler is a part of the relay station.

In some embodiments of any of the above apparatus, the relay station may comprise a second optical coupler configured to couple optical-pump power of a second optical pump into the second multimode fiber through the end thereof, wherein the second optical coupler is configured to partition the optical-pump power

of the second optical pump among guided modes of the second multimode fiber populated therein by the optical signal.

In some embodiments of any of the above apparatus, the first optical coupler and the second optical coupler may include a shared beam combiner configured to  
5 direct in opposite directions the optical power of the first optical pump and the optical power of the second optical pump.

#### BRIEF DESCRIPTION OF THE DRAWINGS

Other aspects, features, and benefits of various embodiments of the invention  
10 will become more fully apparent, by way of example, from the following detailed description and the accompanying drawings, in which:

FIG. 1 shows a block diagram of an optical transport system according to one embodiment of the invention;

FIG. 2 shows representative intensity distributions and polarizations for the  
15 three lowest linearly polarized (LP) modes of a multimode fiber that can be used in the system of FIG. 1 according to one embodiment of the invention;

FIG. 3 shows representative phase/field-strength (PFS) patterns for several LP modes of a multimode fiber that can be used in the system of FIG. 1 according to another embodiment of the invention;

20 FIG. 4 shows a block diagram of an optical module that can be used in the transmitter terminal of the transport system shown in FIG. 1 according to one embodiment of the invention;

FIG. 5 shows an end facet of a multimode fiber with a pump-beam spot and a corresponding phase pattern according to a representative configuration of the optical  
25 module shown in FIG. 4;

FIG. 6 shows an end-facet view of a waveguide array that can be used in the optical module of FIG. 4 according to one embodiment of the invention;

FIG. 7 shows an end facet of a multimode fiber with two pump-beam spots and a corresponding phase pattern according to another representative configuration  
30 of the optical module shown in FIG. 4;

FIG. 8 shows an alternative configuration of the optical module shown in FIG.  
4;

FIG. 9 shows a block diagram of an optical-pump coupler that can be used in a relay station of the transport system shown in FIG. 1 according to one embodiment of the invention; and

FIG. 10 shows a block diagram of a Raman amplifier that can be used in the optical link of the transport system shown in FIG. 1 according to one embodiment of the invention.

#### DETAILED DESCRIPTION

A multimode fiber can provide a higher transmission capacity than a single-mode fiber by means of space-division multiplexing (SDM), wherein different guided modes of the multimode fiber are populated with different modulated optical signals or different combinations of a given set of modulated optical signals. Long-distance transport of SDM signals over multimode fibers can greatly benefit from the use of multimode-fiber amplifiers. However, a typical prior-art doped-fiber or Raman amplifier employs, as an optical-gain medium, a single-mode fiber and, as such, is unsuitable for SDM signals.

These and other pertinent problems in the prior art are addressed by various embodiments of a multimode-fiber (MMF) amplifier that can be used, e.g., to amplify SDM optical signals transported through a multimode-fiber link. Depending on the material of the fiber and configuration of the optical pumps, the MMF amplifier can amplify optical signals via a stimulated-emission process or a stimulated Raman-scattering (SRS) process. Advantageously, various embodiments of the invention provide a cost-effective solution for long-distance transport of optical-communication signals over MMF links.

FIG. 1 shows a block diagram of an optical transport system **100** according to one embodiment of the invention. System **100** has a transmitter terminal **110** and a receiver terminal **140** connected to one another via an optical transport link **104**. Link **104** is illustratively shown as having four sections **106a-106d** of multimode optical fiber and two relay stations **120<sub>1</sub>-120<sub>2</sub>**. In alternative embodiments, link **104** may have a different number of fiber sections **106** and/or a different number of relay stations **120**. Various additional components, such as optical routing elements, variable optical attenuators, lumped optical amplifiers, optical add-drop multiplexers,

optical filters, and the like, may be incorporated into link **104** as appropriate or necessary.

In one embodiment, one or more of the multimode fiber of sections **106** comprise(s) a segment of doped multimode fiber, such as an Erbium-doped multimode fiber. When appropriately pumped by pump light from transmitter terminal **110** and/or relay station(s) **120**, fiber section **106** operates as a distributed fiber amplifier, e.g., a distributed Erbium-doped MMF amplifier.

In another embodiment, the multimode fiber of section **106** comprises a multimode fiber suitable for Raman amplification of optical signals. When appropriately pumped by pump light from transmitter terminal **110**, receiver terminal **140**, and/or relay station(s) **120**, fiber section **106** operates as a distributed MMF Raman amplifier.

In some embodiments, the above-described MMF amplifier(s) may be formed by multimode fiber segments located in the transmitter terminal **110**, receiver terminal **140**, and/or relay station(s) **120**,

Transmitter terminal **110** is configured to receive one or more input data streams **102** and generate a corresponding SDM optical output signal that is applied to fiber section **106a** to carry the data of the input data stream(s), via link **104**, to receiver terminal **140**. In one embodiment, transmitter terminal **110** includes an optical-pump coupler (not explicitly shown in FIG. 1) configured to couple one or more optical-pump beams into fiber section **106a** for co-directional pumping and amplification of the SDM signal in that fiber section. A representative optical-pump coupler that can be used in transmitter terminal **110** is described in more detail below in reference to FIGs. 4-7.

Receiver terminal **140** is configured to receive an SDM signal from fiber section **106d** and to process that signal to recover the data of data stream(s) **102**. In one embodiment, receiver terminal **140** includes an optical-pump coupler (not explicitly shown in FIG. 1) configured to couple one or more optical pump beams into fiber section **106d** for contra-directional pumping and amplification of the SDM signal in that fiber section. A representative optical-pump coupler that can be used in receiver terminal **140** is described in more detail below in reference to FIG. 8.



Each relay station **120** may include an optical-pump coupler (not explicitly shown in FIG. 1) configured to couple one or more optical pump beams into one or both of adjacent fiber sections **106**. For example, the optical-pump coupler of relay station **120<sub>1</sub>** may be configured to couple one or more optical pump beams into fiber section **106a** for contra-directional pumping and amplification of the SDM signal in that fiber section. Alternatively or in addition, the optical-pump coupler of relay station **120<sub>1</sub>** may be configured to couple one or more optical pump beams into fiber section **106b** for co-directional pumping and amplification of the SDM signal in that fiber section. A representative optical-pump coupler that can be used in a relay station **120** is described in more detail below in reference to FIG. 9.

In general, there are two broad classes of fiber modes: radiation modes and guided modes. Radiation modes carry energy out of the fiber core, which is then quickly dissipated. Radiation modes will not be considered here. Guided modes are primarily confined to the fiber core, and propagate energy along the fiber, thereby transporting information and power. Each guided mode has its own distinct velocity and can be further decomposed into two orthogonally polarized components. Any field distribution within the optical fiber can generally be expressed as a combination of guided modes.

For a given wavelength  $\lambda$ , an optical fiber, such as that used in fiber sections **106** of system **100**, can typically support multiple guided modes if the normalized frequency parameter ( $V$ , also referred to as the  $V$  number) is greater than 2.405. Eq. (1) gives the expression for  $V$ :

$$V = \frac{2\pi a}{\lambda} NA \quad (1)$$

where  $a$  is the fiber-core radius, and  $NA$  is the numerical aperture. For a step-index fiber, the numerical aperture is given by Eq. (2):

$$NA = \sqrt{n_1^2 - n_2^2} \quad (2)$$

where  $n_1$  is the refractive index of the fiber core, and  $n_2$  is the refractive index of the fiber cladding.

The guided modes can be generally classified as (i) transverse electric (TE) modes, for which the axial component of the electric field is zero; (ii) transverse magnetic (TM) modes, for which the axial component of the magnetic field is zero;

and (iii) HE or EH modes, for which neither the axial component of the electric field nor the axial component of the magnetic field is zero. The designation of HE or EH depends on whether the electric or magnetic field component is dominant.

The order of the guided modes in a multimode fiber can be defined based on one or more of the following: (i) the number of intensity lobes in the transverse plane, (ii) group velocity, and (iii) the magnitude of the longitudinal wavevector. The lowest-order or fundamental mode typically has a single intensity lobe, the highest group velocity, and the largest longitudinal wavevector. The remaining (higher-order) modes are typically ordered based on the magnitude of their longitudinal wavevectors. For some waveguide cross-sections and V numbers, one of the remaining two criteria may need to be invoked to determine the relative order of some modes.

The refractive-index profiles of most step-index optical fibers used in communication links, such as link **104** in system **100**, have a relatively small (e.g., smaller than about 0.05) contrast  $\Delta$ , which makes these fibers only weakly guiding. Eq. (3) gives the definition of  $\Delta$  for a step-index fiber:

$$\Delta = \frac{n_1 - n_2}{n_1} \quad (3)$$

In the approximation of weak guidance for generally cylindrical fibers, the TE, TM, HE, and EH guided modes become the modes that are referred to as the linearly polarized (LP) modes.

The following notation is usually adhered to in the description of the LP modes. Each LP mode is designated using two integer indices, e.g., in the form of subscripts:  $LP_{jk}$ . The first integer index (j) gives the number of  $2\pi$ -sized phase increments in the electric field per one azimuthal rotation about the fiber axis (e.g., the Z-coordinate axis). The second integer index (k) gives the number of electric-field nodes in the radial dimension, with the zero field at the outer edge of the field distribution counted as a radial node. Some of the LP modes are also given a designating letter, e.g., a, b, etc., that follows the two integer indices to designate certain degenerate modes. As already indicated above, each LP mode can have two different polarizations, e.g., an X polarization and a Y polarization, where X and Y are the two transverse (i.e., orthogonal to the fiber axis) coordinate axes.

FIG. 2 graphically shows representative intensity distributions and polarizations for the three lowest LP modes of a multimode fiber that can be used in link **104** according to one embodiment of the invention. The intensity distributions are color-coded so that (i) the dark blue color corresponds to the zero intensity, (ii) the dark red color corresponds to the highest intensity, and (iii) the colors in between correspond to the intermediate intensities in the rainbow-like progression from blue to red. The dotted arrows indicate the respective electric-field polarizations for different modes. Each of the shown LP modes is doubly degenerate, with the same intensity distribution corresponding to each of two orthogonal (e.g., X and Y) polarizations.

10 The fundamental mode ( $LP_{01}$ ) has an intensity profile that is similar to that of a Gaussian beam. The  $LP_{01}$  mode corresponds to the  $HE_{11}$  mode of a strongly guiding fiber.

The next lowest-order mode ( $LP_{11}$ ) has an intensity profile comprising two intensity peaks characterized by a phase difference of 180 degrees between the corresponding electric fields. In the  $LP_{11a}$  mode, the intensity peaks are lined up along the X-axis. In the  $LP_{11b}$  mode, the intensity peaks are similarly lined up along the Y-axis. The different degenerate states of the  $LP_{11a}$  and  $LP_{11b}$  modes correspond to different linear combinations of the  $TE_{01}$ ,  $TM_{01}$ , and  $HE_{21}$  modes of a strongly guiding fiber. If the  $V$  number (see Eq. (1)) is in the range between 2.405 and about 3.9, then the  $LP_{01}$ ,  $LP_{11a}$ , and  $LP_{11b}$  modes are typically the only guided modes supported by the fiber. In this case, the fiber is referred to as a three-mode (3M) fiber.

FIG. 3 graphically shows representative phase/field-strength (PFS) patterns for several LP modes of a multimode fiber that can be used in link **104** according to another embodiment of the invention. Each PFS pattern is color-coded using a color scheme in which: (i) the degree of color saturation represents the optical-field strength and (ii) the color itself represents the phase of the electric field. For example, the light red color corresponds to lower optical-field strength than the dark red color. A rainbow-like change in color from blue to red represents a continuous change in the relative phase from  $-\pi$  to  $+\pi$ .

30 PFS patterns for different states of degenerate LP modes can be obtained by appropriately rotating the PFS patterns shown in FIG. 3. For example, the PFS pattern for the  $LP_{11b}$  mode (see FIG. 2) can be obtained by rotating by 90 degrees the

PFS pattern shown in the second-from-the-left panel in the top row of FIG. 3. The intensity distribution for the LP mode can be obtained by calculating a square of the absolute values of the corresponding PFS pattern. For example, the intensity distribution for the LP<sub>01</sub> mode shown in the left-most panel of FIG. 2 can be obtained  
5 by calculating a square of the absolute values of the PFS pattern shown in the left-most panel in the top row of FIG. 3. Similarly, the intensity distribution for the LP<sub>11a</sub> mode shown in the third-from-the-left panel of FIG. 2 can be obtained by calculating a square of the absolute values of the PFS pattern shown in the second-from-the-left panel in the top row of FIG. 3.

10 To efficiently and selectively couple light into a particular LP mode of a multimode fiber, the PFS pattern and polarization created by a light source at an end facet of the fiber should approximate closely the PFS pattern and polarization of that LP mode. In particular the light that does not match the appropriate PFS pattern and polarization may be coupled into a different LP mode, be coupled to a radiation mode,  
15 and/or be reflected back from the end facet of the multimode fiber. For example, to efficiently and selectively couple light into the X-polarized LP<sub>11a</sub> mode, the corresponding light source should be configured to create a PFS pattern that closely approximates the PFS pattern shown in the second-from-the-left panel in the top row of FIG. 3 and the polarization shown in the third-from-the-left panel of FIG. 2.

20 For brevity and clarity reasons, the description of various embodiments is presented below in reference to a 3M fiber and the corresponding LP modes. However, embodiments of the invention are not so limited. From the provided description, one of ordinary skill in the art will be able to make and use various  
25 embodiments of the invention with any suitable multimode fiber, including a strongly guiding multimode fiber whose guided modes are the corresponding TE, TM, HE, and EH modes, rather than the LP modes illustrated in FIGs. 2 and 3.

FIG. 4 shows a block diagram of an optical module **400** that can be used in transmitter terminal **110** (FIG. 1) according to one embodiment of the invention. Module **400** comprises an optical-signal coupler **410** and an optical-pump coupler  
30 **440**. Optical-signal coupler **410** is configured to generate an SDM signal and present that signal for coupling into an output 3M fiber **490**. Optical-pump coupler **440** is configured to couple an optical-pump signal into fiber **490** to provide optical power

for distributed amplification therein of the SDM signal generated by optical-signal coupler **410**. In one embodiment, 3M fiber **490** can be, e.g., a part of fiber section **106a** in system **100** (FIG. 1). The configuration of optical module **400** shown in FIG. 4 can be used for co-directional pumping of a stimulated-emission amplification process or an SRS amplification process.

Optical-signal coupler **410** has three fibers **412<sub>1</sub>-412<sub>3</sub>**, e.g., single mode optical fibers, each configured to deliver a corresponding one of independently modulated optical input signals **402<sub>1</sub>-402<sub>3</sub>**. Each of signals **402<sub>1</sub>-402<sub>3</sub>** can be, e.g., a polarization-division multiplexed (PDM) signal having two independently modulated polarization components. For each fiber **412**, coupler **410** has a respective lens **416** configured to collimate the respective diverging light beam produced by the fiber. Each of the resulting collimated beams passes through a respective one of phase masks **420<sub>1</sub>-420<sub>3</sub>** to create a corresponding phase-filtered beam.

Optical-signal coupler **410** further has two beam combiners **424<sub>1</sub>** and **424<sub>2</sub>**. Combiner **424<sub>2</sub>** is configured to spatially superimpose the phase-filtered beams produced by phase masks **420<sub>2</sub>** and **420<sub>3</sub>**, while combiner **424<sub>1</sub>** is configured to spatially superimpose the phase-filtered beam produced by phase mask **420<sub>1</sub>** with the superimposed beam from combiner **424<sub>2</sub>** and direct the resulting superimposed beam toward a lens **430**. Lens **430** together with lenses **416** and **480** (the latter located in optical-pump coupler **440**) form an optical relay system configured to (i) relay the superimposed beam to fiber **490** and (ii) appropriately image the beam onto the end facet of the fiber.

Depending on the LP modes assigned to signals **402<sub>1</sub>-402<sub>3</sub>**, each of phase masks **420<sub>1</sub>-420<sub>3</sub>** is configured to have a corresponding phase-shift pattern that produces an appropriate PFS pattern at the end facet of output fiber **490** to enable efficient and selective coupling of the signal into the assigned LP mode. For example, if signal **402<sub>1</sub>** is assigned the LP<sub>11a</sub> mode of fiber **490**, then phase mask **420<sub>1</sub>** is configured to have a phase-shift pattern that causes, at the end facet of fiber **490**, the appropriately oriented PFS pattern shown in the second-from-the-left panel in the top row of FIG. 3. If signal **402<sub>2</sub>** is assigned the LP<sub>11b</sub> mode of fiber **490**, then phase mask **420<sub>2</sub>** is configured to have a phase-shift pattern that causes, at the end facet of fiber **490**, a PFS pattern that is similar to the PFS pattern created by phase mask **420<sub>2</sub>**

for signal **402**<sub>1</sub> but rotated with respect to it by 90 degrees. If signal **402**<sub>3</sub> is assigned the LP<sub>01</sub> mode of fiber **490**, then phase mask **420**<sub>3</sub> may be omitted or configured to impose a constant phase shift. The latter characteristic is due to the spatial similarity of the PFS patterns corresponding to the fundamental mode of a single-mode fiber, such as single-mode fiber **412**<sub>3</sub>, and the LP<sub>01</sub> mode of a 3M fiber, such as fiber **490**.

Representative optical-signal couplers that can be used to implement (i) various embodiments and/or features of optical-signal coupler **410** and (ii) representative SDM transmitters that may be used to implement transmitter terminal **110** (FIG. 1) are disclosed, e.g., in U.S. Patent Application Publication No. 2010/0329670 and/or 2010/0329671 and/or U.S. Patent Application Serial No. 12/986,468, filed on 01-07-2011, and/or 12/827,284, filed on 06-30-2010, and/or in U.S. Patent Application, titled "OPTICAL MODE COUPLERS FOR MULTI-MODE OPTICAL FIBERS" by Roland Ryf, filed on 09-16-2011 (Docket No.: 810270-US-NP). All of the U.S. Patent Applications and U.S. Patent Application Publications listed in this paragraph are incorporated herein by reference in their entirety.

Different LP modes are generally subjected to different degrees of attenuation in a multimode fiber, with the higher-order modes typically being subjected to stronger attenuation than the lower-order modes. However, a desired characteristic of an optical link, such as link **104** (FIG. 1), is often about a 0-dB net gain. This dB number implies that it is often beneficial when signal attenuation in the link is substantially canceled or compensated to a significant degree by signal amplification in the link.

For efficient energy transfer from an optical-pump signal to a communication signal in a multimode fiber, the two signals should preferably populate the same LP mode of that fiber. This preferable condition is mostly due to the spatial orthogonality of different LP modes and/or their different group velocities. However, there is typically no particular relative phase condition that is strongly preferred for the optical-pump and communication signals by the underlying physics of the stimulated-emission process or the SRS process. The modal-amplification gain typically strongly depends on the partial power of the optical-pump signal residing in the mode. To offset the different degrees of attenuation of different LP modes, it is therefore desirable for an optical-pump coupler, such as optical-pump coupler **440**, to enable a

specified uneven partition of the optical-pump power between different LP modes while preferably about minimizing optical-pump reflections from the end facet of the fiber. It is also usually desirable for the optical-pump coupler to be relatively robust and inexpensive. These and other pertinent technical problems may be addressed  
5 herein by some of the different embodiments of optical-pump couplers, of which optical-pump coupler **440** is an example.

Optical-pump coupler **440** is configured to receive an optical-pump signal **438** from an external optical-pump source (e.g., a laser, not explicitly shown in FIG. 4). Signal **438** passes through a polarization scrambler **444** configured to evenly  
10 distribute the optical power of that signal between different polarizations. In various embodiments, polarization scrambler **444** can be fiber-based or implemented using free-space optics. In the various embodiments, polarization scrambler **444** may be optional and, as such, may be omitted.

A possibly diverging light beam exiting the output port of polarization  
15 scrambler **444** may be collimated by a lens **446**. The resulting collimated beam passes through a phase mask **450** to produce a corresponding phase-filtered beam. A dichroic beam combiner **464** or another wavelength dependent optical combiner turns the phase-filtered beam toward fiber **490** and also spatially superimposes it with the SDM signal that is being relayed from optical-signal coupler **410** toward the fiber. A  
20 lens **460** may optionally be disposed between phase mask **450** and combiner **464**, i.e., to perform a functionality similar to that of lens **430**. More specifically, lenses **446**, **460**, and **480** are usually used to form an optical-relay system configured to (i) relay the phase-filtered pump beam to fiber **490**, (ii) appropriately compress the diameter of that beam, and (iii) appropriately position the optically compressed-beam spot on the  
25 end facet for coupling the pump power into the fiber.

FIG. 5 shows an end facet **500** of fiber **490** together with a pump-beam spot **510** and a corresponding phase-shift pattern **550** according to a representative configuration of optical-pump coupler **440** (FIG. 4). End facet **500** typically has a circular shape and comprises a cladding area **502** and a core area **504**. The overlaid  
30 X- and Y-coordinate axes, shown in FIG. 5 by the dashed lines, provide a coordinate frame, with the origin of that frame being located at the geometric center of end facet **500** (although that origin is not explicitly represented in FIG. 5).

Pump-beam spot **510** usually has an about circular shape characterized by an approximately Gaussian intensity distribution within it. For such a profile, about 90% of the optical power of spot **510** is typically concentrated within diameter  $D$ , as indicated in FIG. 5. The geometric center of spot **510** may be offset by distance  $\Delta x_1$  from the geometric center of end facet **500** along the X-coordinate axis, but is typically not offset along the Y-coordinate axis. In another configuration, the geometric center of spot **510** can alternatively or additionally be offset by distance  $\Delta y_1$  (not shown in FIG. 5) from the geometric center of end facet **500** along the Y-coordinate axis.

Phase-shift pattern **550** is imposed by phase mask **450** (FIG. 4) and, as such, corresponds approximately to the phase-shift pattern of that phase mask. In this particular example, phase mask **450** is a binary phase mask having two portions, each imposing a corresponding constant phase shift with a phase-shift difference of about 180 degrees between the portions. As a result, phase-shift pattern **550** has two areas labeled **552<sub>1</sub>** and **552<sub>2</sub>**, respectively, e.g., rectangular areas, with one area corresponding to a relative phase shift of about 0 degrees, and the other area corresponding to a relative phase shift of about 180 degrees. Phase mask **450** is oriented so that a boundary **554** between areas **552<sub>1</sub>** and **552<sub>2</sub>** is parallel to the Y-coordinate axis and offset with respect to that axis by distance  $\Delta x_2$ . In an alternative configuration, phase mask **450** can be oriented so that boundary **554** is oriented at any desired angle with respect to the Y- (or X-) coordinate axis.

The configuration shown in FIG. 5 results in the power of the optical-pump beam being coupled primarily into the  $LP_{01}$  and  $LP_{11a}$  modes of fiber **490**. The relative power partition between these two LP modes depends on the values of  $D$ ,  $\Delta x_1$ , and  $\Delta x_2$ . The spot size ( $D$ ) is controlled by the magnification (or demagnification) provided by the optical-relay system having lenses **446**, **460**, and **480** (FIG. 4). The first offset distance ( $\Delta x_1$ ) is controlled by the relative alignment of the various optical elements within optical-pump coupler **440** (FIG. 4). The second offset distance ( $\Delta x_2$ ) is controlled by the position of the phase mask **450** with respect to the optical-pump beam. In one embodiment, optical-pump coupler **440** (FIG. 4) incorporates physical means for adjusting the size of spot **510** and/or changing the first and/or second offset distances. Such physical means may include, for example,



one or more translation and/or rotation stages (not explicitly shown in FIG. 4) that enable changes in the relative positions/orientations of polarization scrambler **444**, lenses **446**, **460**, and **480**, phase mask **450**, dichroic beam combiner **464**, and the mount of fiber **490**.

5           FIG. 6 shows an end-facet view of a waveguide array **600** that can be used in optical-pump coupler **440** (FIG. 4) according to one embodiment of the invention. More specifically, waveguide array **600** can be configured to direct multiple approximately parallel optical pump beams toward lens **446** (see FIG. 4). In an embodiment having polarization scrambler **444**, waveguide array **600** can serve as an  
10           output port of the polarization scrambler.

Waveguide array **600** is illustratively shown as having four optical fibers **610<sub>1</sub>-610<sub>4</sub>**. Each fiber **610** has a respective cladding **602** and a respective core **604**. The end facets of fibers **610<sub>1</sub>-610<sub>4</sub>** are arranged in a two-dimensional array as indicated in FIG. 6. Each fiber **610** is configured to emit from its end facet a respective optical-  
15           pump beam. The individual optical-pump beams corresponding to different fibers **610** may be individually turned ON or OFF, e.g., by appropriately controlling the optical-pump source(s) coupled to the distal ends of those fibers. In one configuration, at least two of the optical-pump beams corresponding to different fibers **610** may have different respective wavelengths.

20           In an alternative embodiment, waveguide array **600** may have a different number of waveguides, not necessarily having circular shapes. The waveguides may be arranged in any desired manner, e.g., to form a linear array or a two-dimensional array. Different waveguides in the array may have different core sizes and/or shapes.

FIG. 7 shows end facet **500** of fiber **490** together with pump-beam spots **710<sub>1</sub>**  
25           and **710<sub>2</sub>** and a corresponding phase-shift pattern **750** according to another representative configuration of optical-pump coupler **440** (also see FIGs. 4 and 5). Spots **710<sub>1</sub>** and **710<sub>2</sub>** can be generated, e.g., using waveguide array **600** of FIG. 6. More specifically, the optical-pump sources coupled to the distal ends of fibers **610<sub>1</sub>** and **610<sub>2</sub>** are turned ON, while the optical-pump sources coupled to the distal ends of  
30           fibers **610<sub>3</sub>** and **610<sub>4</sub>** are turned OFF. As a result, the optical-pump beam emitted from the end facet of fiber **610<sub>1</sub>** generates spot **710<sub>1</sub>**, and the optical-pump beam emitted from the end facet of fiber **610<sub>2</sub>** similarly generates spot **710<sub>2</sub>**. In other

embodiments, the pump-beam spots **710<sub>1</sub>** and **710<sub>2</sub>** may be produced by an embodiment of waveguide array **600** having only two fibers, e.g., **610<sub>1</sub>** and **610<sub>2</sub>**. Similar to overlapping rectangular tiles, wherein each tile is configured to produce two phase-shift areas characterized by a relative phase-shift difference between them of about 180 degrees. One of the tiles produces the phase-shift pattern in the area labeled **750<sub>1</sub>**, and the other tile produces the phase-shift pattern in the area labeled **750<sub>2</sub>**. The relative phase shift between (i) a rectangular portion **752<sub>11</sub>** of area **750<sub>1</sub>** and (ii) a corresponding rectangular portion **752<sub>21</sub>** of area **750<sub>2</sub>** has a fixed value, which may or may not be zero degrees. The corresponding tiles of phase mask **450** may be configured, e.g., so that (i) a boundary **754<sub>1</sub>** between portions **752<sub>11</sub>** and **752<sub>12</sub>** of area **750<sub>1</sub>** is oriented at an angle of about 45 degrees with respect the X-coordinate axis and (ii) a boundary **754<sub>2</sub>** between portions **752<sub>21</sub>** and **752<sub>22</sub>** of area **750<sub>2</sub>** is orthogonal to boundary **754<sub>1</sub>**.

The configuration shown in FIG. 7 results in the power of the two optical-pump beams being coupled primarily into the LP<sub>11a</sub> and LP<sub>11b</sub> modes of fiber **490**. The relative power partition between these two LP modes depends on the relative intensities of the two beams, which can be controlled, e.g., by controlling the corresponding light sources.

In various alternative embodiments, phase mask **450** (FIG. 4) may have other tiled configurations. The tiles may or may not have rectangular shapes. The number of tiles may match the number of waveguides in the corresponding waveguide array, e.g., analogous to waveguide array **600** of FIG. 6. Either binary or continuous phase-shift patterns may be used for each tile. Representative phase-shift patterns that can be used to implement different tiles of the phase mask are shown, e.g., in FIG. 4B of the above-cited U.S. Patent Application Publication No. 2010/0329670. In various alternative embodiments, phase mask **450** may be designed to impose any desired phase-shift pattern, which can be based, e.g., on the desired partition of optical-pump power between different LP modes of the corresponding multimode fiber.

FIG. 8 shows an alternative configuration of optical module **400**. Optical module **400**, configured as indicated in FIG. 8, can be used, e.g., in receiver terminal **140** (FIG. 1) to implement contra-directional pumping of an SRS amplification process. In this case, fiber **490** can be a part of fiber section **106d** (FIG. 1).

One difference between the configurations of optical module **400** shown in FIGs. 4 and 8, respectively, is that, in the latter configuration, optical-signal coupler **410** is configured to operate with signals flowing in the direction that is opposite to that in the former configuration. As a result, in the configuration of FIG. 8, optical-signal coupler **410** decomposes the SDM signal relayed to it by lenses **480** and **430** from fiber **490** into three individual SDM components labeled as signals **802<sub>1</sub>-802<sub>3</sub>**, respectively. Each of these signals can then be directed to a corresponding optical detector (not explicitly shown in FIG. 8) for demodulation.

FIG. 9 shows a block diagram of an optical-pump coupler **900** that can be used in relay station **120** (FIG. 1) according to one embodiment of the invention. Optical-pump coupler **900** comprises two instances of optical-pump coupler **440** that share a dichroic beam combiner, which is labeled **964** in FIG. 9. Optical-pump coupler **440<sub>1</sub>** is configured to receive an optical-pump signal **938<sub>1</sub>** from an external optical-pump source (e.g., a laser, not explicitly shown in FIG. 9) and couple that pump signal into a multimode fiber **990<sub>1</sub>**, e.g., as already described above in reference to FIGs. 4-7. Optical-pump coupler **440<sub>2</sub>** is similarly configured to receive an optical-pump signal **938<sub>2</sub>** from an external optical-pump source and couple that pump signal into a multimode fiber **990<sub>2</sub>**. Lenses **480<sub>1</sub>** and **480<sub>2</sub>** (located in optical-pump couplers **440<sub>1</sub>** and **440<sub>2</sub>**, respectively) may be configured to relay an SDM signal from fiber **990<sub>2</sub>** to fiber **990<sub>1</sub>**. Due to this SDM-signal propagation direction, optical-pump coupler **440<sub>1</sub>** implements co-directional pumping while optical-pump coupler **440<sub>2</sub>** implements contra-directional pumping.

FIG. 10 shows a block diagram of a Raman amplifier **1000** that can be used in link **104** (FIG. 1) according to one embodiment of the invention. Raman amplifier **1000** comprises two instances of optical-pump coupler **440**, labeled **440a** and **440b**, respectively. Optical-pump coupler **440a** is configured to receive an optical-pump signal **1038a** from an external optical-pump source (e.g., a laser, not explicitly shown in FIG. 10) and couple that pump signal into an end facet **1092a** of a multimode fiber **1090**, e.g., as already described above in reference to FIGs. 4-7. Optical-pump coupler **440b** is similarly configured to receive an optical-pump signal **1038b** from an external optical-pump source and couple that pump signal into an end facet **1092b** of a multimode fiber **1090**. Fiber **1090** is made of a material (e.g., Ge-

doped silica) having a relatively high SRS cross-section. As a result, fiber **1090** can have a relatively short length, which enables amplifier **1000** to be implemented as a lumped amplifier.

An SDM signal may traverse amplifier **1000** in either direction, e.g., from a multimode fiber **1002a** to a multimode fiber **1002b**, or from multimode fiber **1002b** to multimode fiber **1002a**. Lenses **1004a** and **1004b** are configured to appropriately optically couple multimode fibers **1002a** and **1002b** to optical-pump couplers **440a** and **440b**, respectively. Regardless of the SDM-signal propagation direction, one of optical-pump couplers **440a** and **440b** implements co-directional pumping of fiber **1090** while the other one implements contra-directional pumping of the fiber.

In an alternative embodiment, one of optical-pump couplers **440a** and **440b** may be removed. One of ordinary skill in the art will also understand that an embodiment of amplifier **1000** having a single optical-pump coupler **440** configured for co-directional pumping of the SDM signal can be converted into an Erbium-doped fiber amplifier in a relatively straightforward manner, e.g., by replacing the above-described SRS-optimized fiber **1090** by an appropriate Erbium-doped multimode fiber.

While this invention has been described with reference to illustrative embodiments, this description is not intended to be construed in a limiting sense.

Although various embodiments were described in reference to SDM signals, they can also be practiced with other multimode signals, which may or may not be modulated with data.

Various modifications of the described embodiments, as well as other embodiments of the invention, which are apparent to persons skilled in the art to which the invention pertains are deemed to lie within the principle and scope of the invention as expressed in the following claims.

Unless explicitly stated otherwise, each numerical value and range should be interpreted as being approximate as if the word "about" or "approximately" preceded the value of the value or range.

It will be further understood that various changes in the details, materials, and arrangements of the parts which have been described and illustrated in order to

explain the nature of this invention may be made by those skilled in the art without departing from the scope of the invention as expressed in the following claims.

The use of figure numbers and/or figure reference labels in the claims is intended to identify one or more possible embodiments of the claimed subject matter in order to facilitate the interpretation of the claims. Such use is not to be construed  
5 as necessarily limiting the scope of those claims to the embodiments shown in the corresponding figures.

Although the elements in the following method claims, if any, are recited in a particular sequence with corresponding labeling, unless the claim recitations  
10 otherwise imply a particular sequence for implementing some or all of those elements, those elements are not necessarily intended to be limited to being implemented in that particular sequence.

Reference herein to "one embodiment" or "an embodiment" means that a particular feature, structure, or characteristic described in connection with the  
15 embodiment can be included in at least one embodiment of the invention. The appearances of the phrase "in one embodiment" in various places in the specification are not necessarily all referring to the same embodiment, nor are separate or alternative embodiments necessarily mutually exclusive of other embodiments. The same applies to the term "implementation."

Also for purposes of this description, the terms "couple," "coupling,"  
20 "coupled," "connect," "connecting," or "connected" refer to any manner known in the art or later developed in which energy is allowed to be transferred between two or more elements, and the interposition of one or more additional elements is contemplated, although not required. Conversely, the terms "directly coupled,"  
25 "directly connected," etc., imply the absence of such additional elements.

The description and drawings merely illustrate the principles of the invention. It will thus be appreciated that those of ordinary skill in the art will be able to devise various arrangements that, although not explicitly described or shown herein, embody the principles of the invention and are included within its spirit and scope.  
30 Furthermore, all examples recited herein are principally intended expressly to be only for pedagogical purposes to aid the reader in understanding the principles of the invention and the concepts contributed by the inventor(s) to furthering the art, and are

to be construed as being without limitation to such specifically recited examples and conditions. Moreover, all statements herein reciting principles, aspects, and embodiments of the invention, as well as specific examples thereof, are intended to encompass equivalents thereof.

CLAIMS

What is claimed is:

1. An apparatus, comprising a first optical coupler configured to:  
pass an optical beam carrying an optical signal corresponding to a set of guided  
5 modes of a first multimode fiber; and  
couple optical-pump power into the first multimode fiber so as to partition the  
optical-pump power among the guided modes of said set.
2. The apparatus of claim 1, further comprising a segment of the first multimode  
10 fiber, wherein the segment of the first multimode fiber is adapted to transfer optical-  
pump energy to the optical signal via a stimulated Raman-scattering process or via a  
stimulated emission process.
3. The apparatus of claim 1, wherein:  
15 the guided modes comprise a fundamental mode and a higher-order mode; and  
the first optical coupler is configured to couple a greater portion of the optical-  
pump power into the higher-order mode than into the fundamental mode.
4. The apparatus of claim 1, wherein:  
20 the first optical coupler comprises a phase mask configured to phase-filter a first  
optical-pump beam to generate a first phase-filtered beam whose phase varies over a  
transverse cross section thereof; and  
the first optical coupler is configured to apply the first phase-filtered beam to an  
end of the first multimode fiber.  
25
5. The apparatus of claim 4, wherein the first optical coupler further comprises:  
a beam combiner configured to spatially overlap the first phase-filtered beam and  
the optical beam carrying the optical signal; and  
a polarization scrambler configured to cause the first optical-pump beam to have  
30 scrambled polarization.
6. The apparatus of claim 4, wherein:

the first optical coupler further comprises an array of waveguides, wherein:

a first waveguide of the array is configured to output the first optical-pump beam; and

5 a second waveguide of the array is configured to output a second optical-pump beam;

the phase mask is further configured to phase-filter the second optical-pump beam to generate a second phase-filtered beam whose phase varies over a transverse cross section thereof; and

10 the first optical coupler is further configured to apply the second phase-filtered beam to the end of the first multimode fiber, wherein the first optical coupler is configured to apply the second phase-filtered beam to a substantially separate region on said end than the first phase-filtered beam.

7. The apparatus of claim 4, wherein the first optical coupler further comprises at least one of:

an adjustable mechanical structure reconfigurable to change a relative position of the first optical-pump beam and the phase mask;

20 a module including a bulk optical element and a mechanically adjustable element configured to change location of a spot illuminated by the first phase-filtered beam on said end; and

a module including a bulk optical element and a mechanically adjustable element for changing a size of said spot.

8. The apparatus of claim 4, wherein the optical phase mask comprises:

25 a first area configured to impose a first constant phase shift on light propagating therethrough; and

a second area configured to impose a second constant phase shift on light propagating therethrough, wherein the second phase shift is different from the first phase shift.

30

9. The apparatus of claim 1, comprising a relay station adapted to transport the optical beam carrying the optical signal between said end of the first multimode fiber



and an end of a second multimode fiber, wherein the first optical coupler is a part of the relay station.

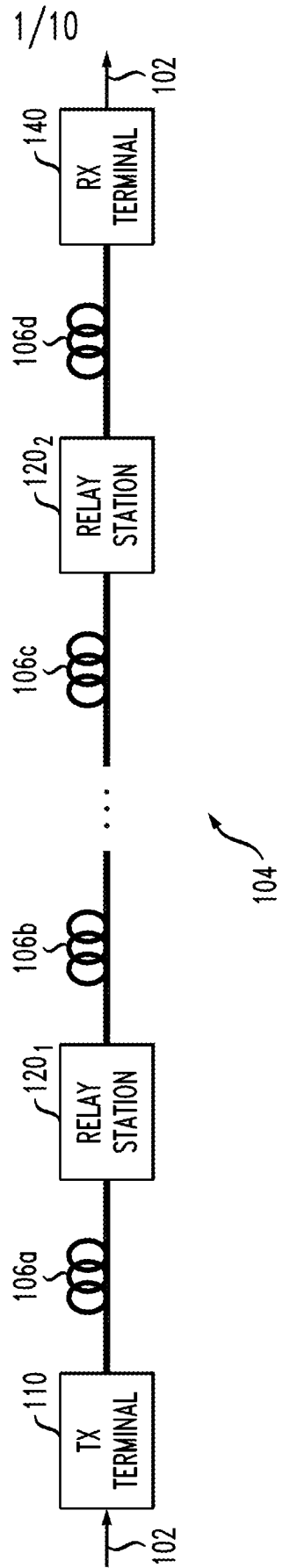
10. The apparatus of claim 9, wherein the relay station comprises a second optical  
5 coupler configured to couple optical-pump power of a second optical pump into the second multimode fiber through the end thereof, wherein:

the second optical coupler is configured to partition the optical-pump power of the second optical pump among guided modes of the second multimode fiber populated therein by the optical signal; and

10 the first optical coupler and the second optical coupler include a shared beam combiner configured to direct in opposite directions the optical power of the first optical pump and the optical power of the second optical pump.

FIG. 1

100



1/10

FIG. 2

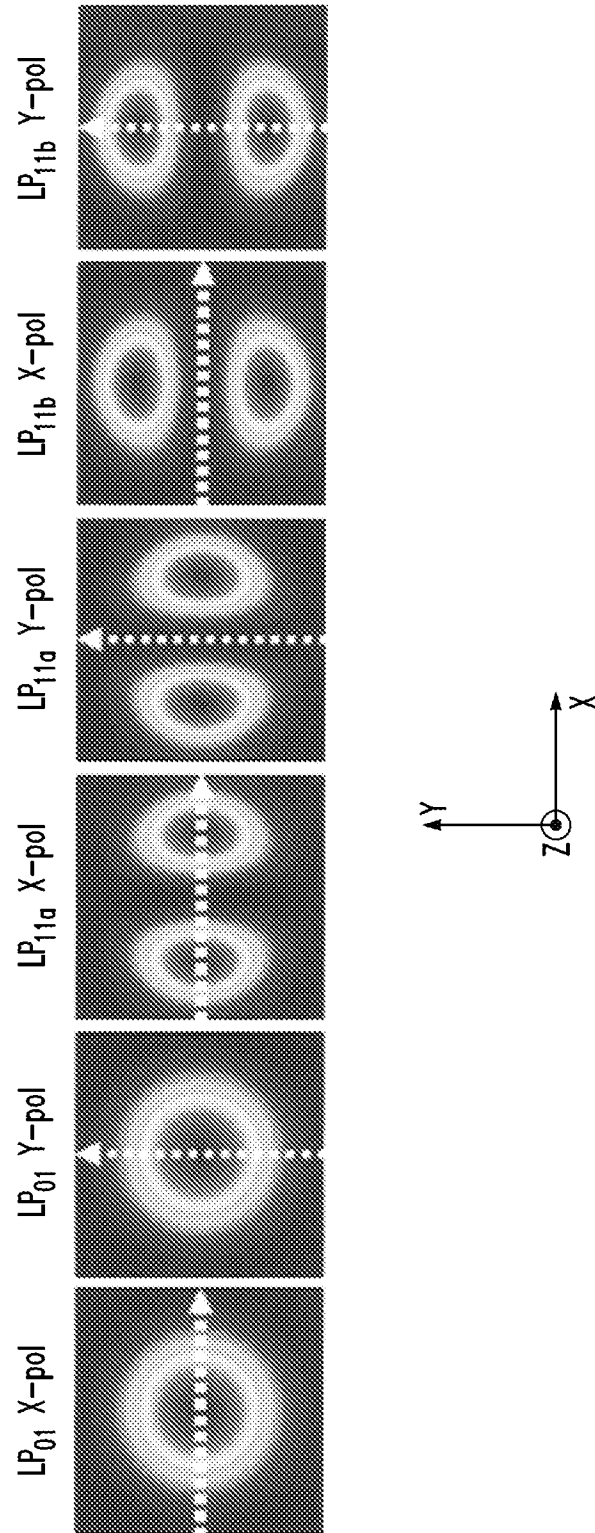
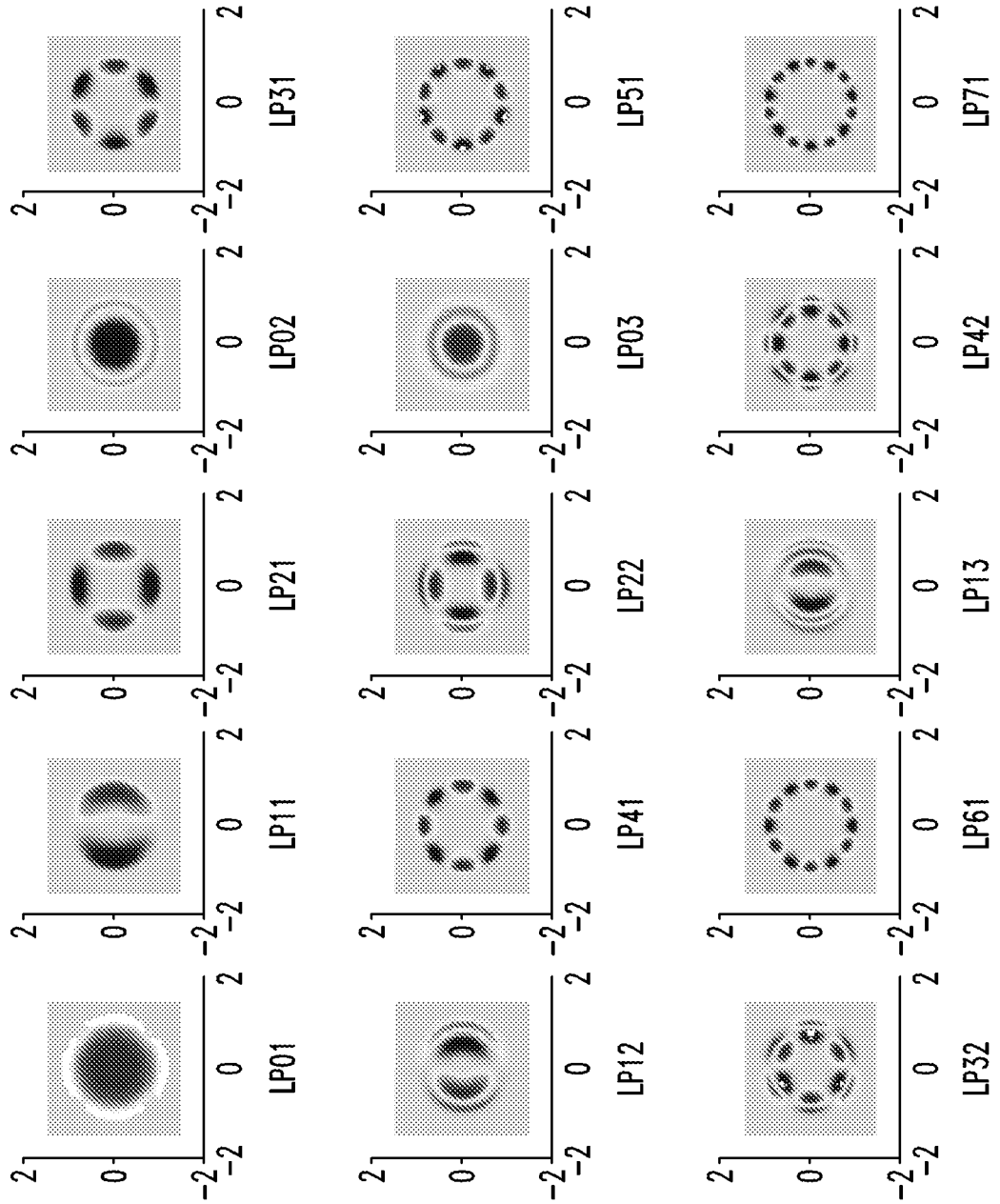


FIG. 3



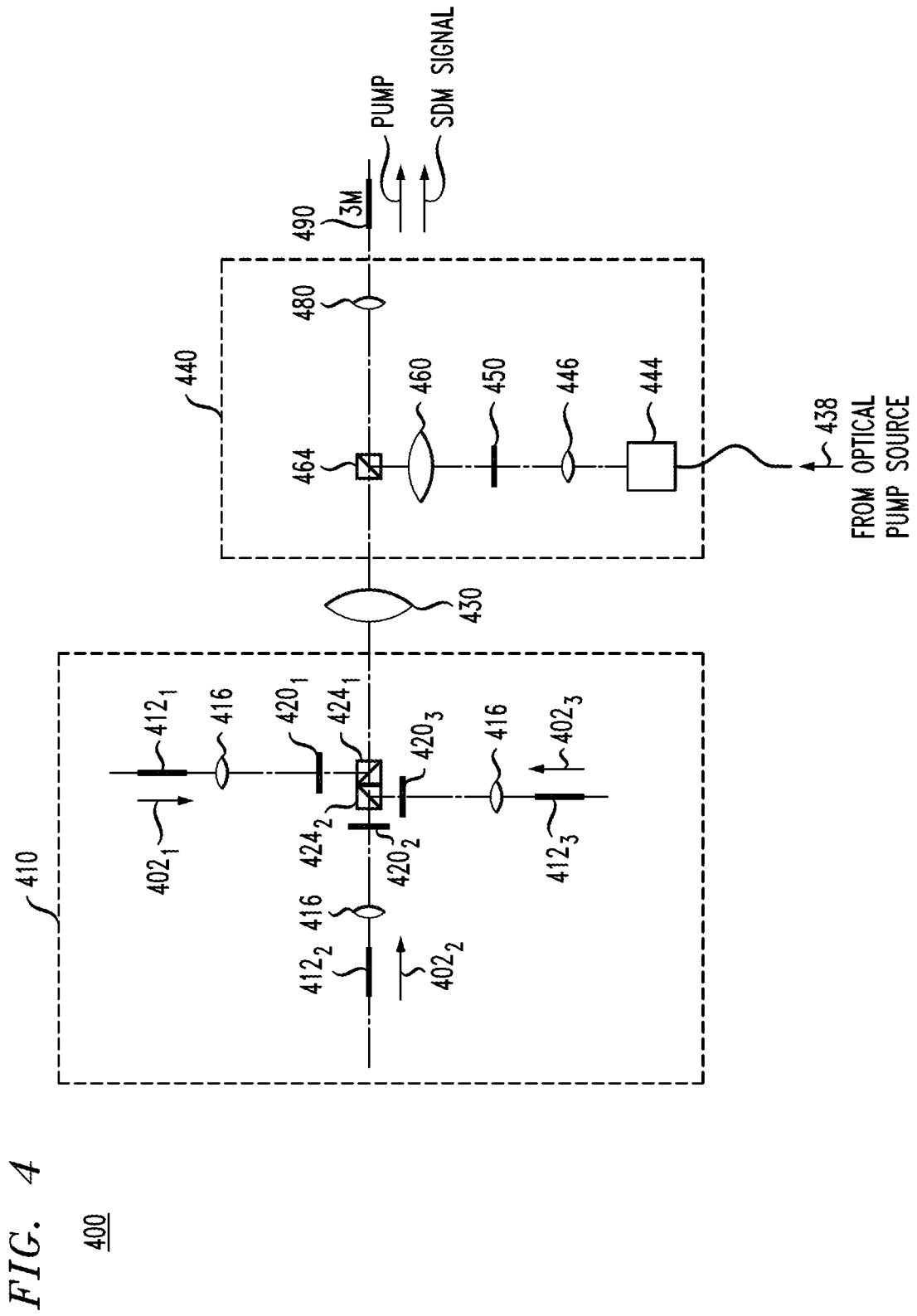
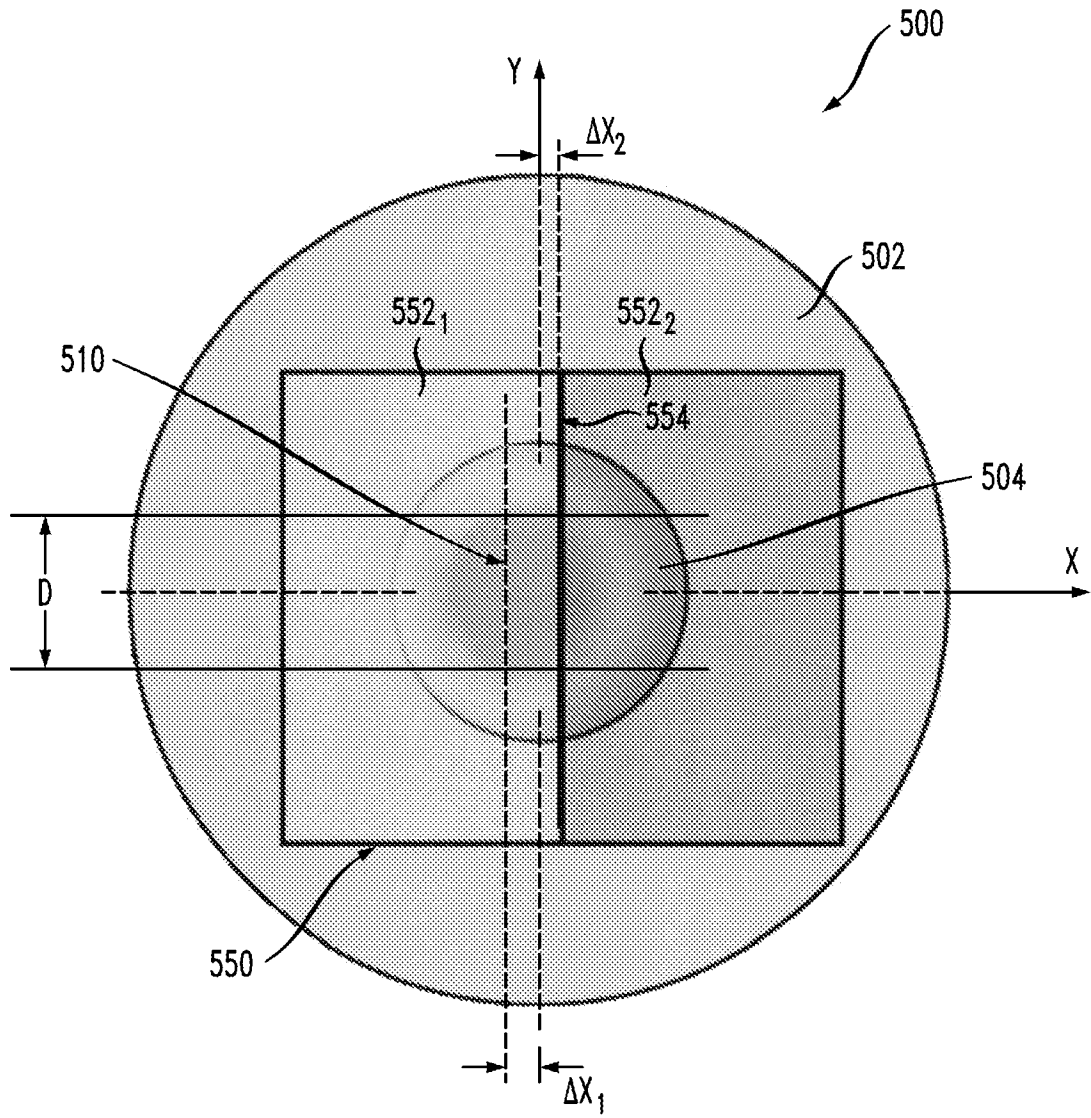


FIG. 5



*FIG. 6*

600

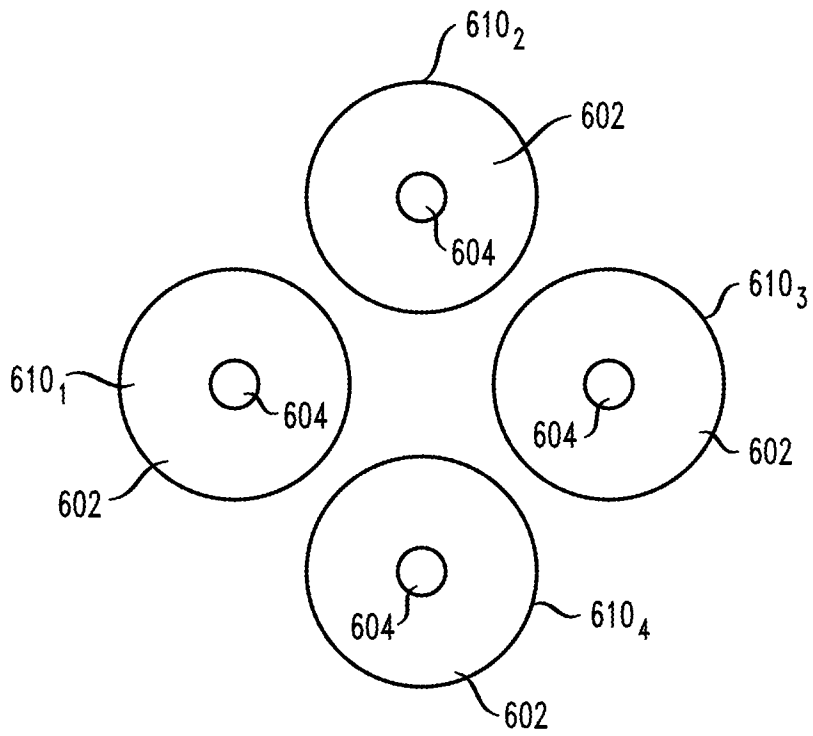
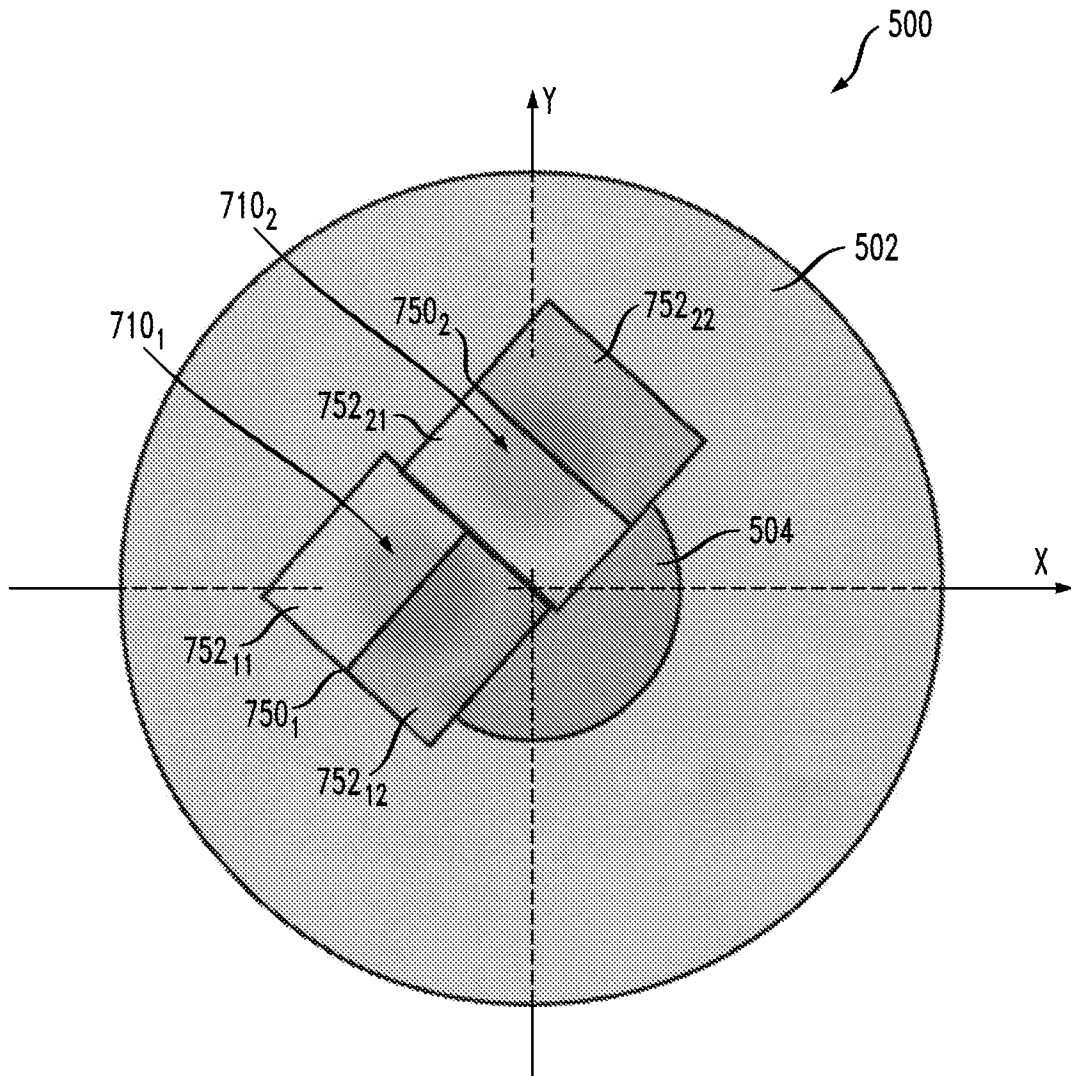


FIG. 7





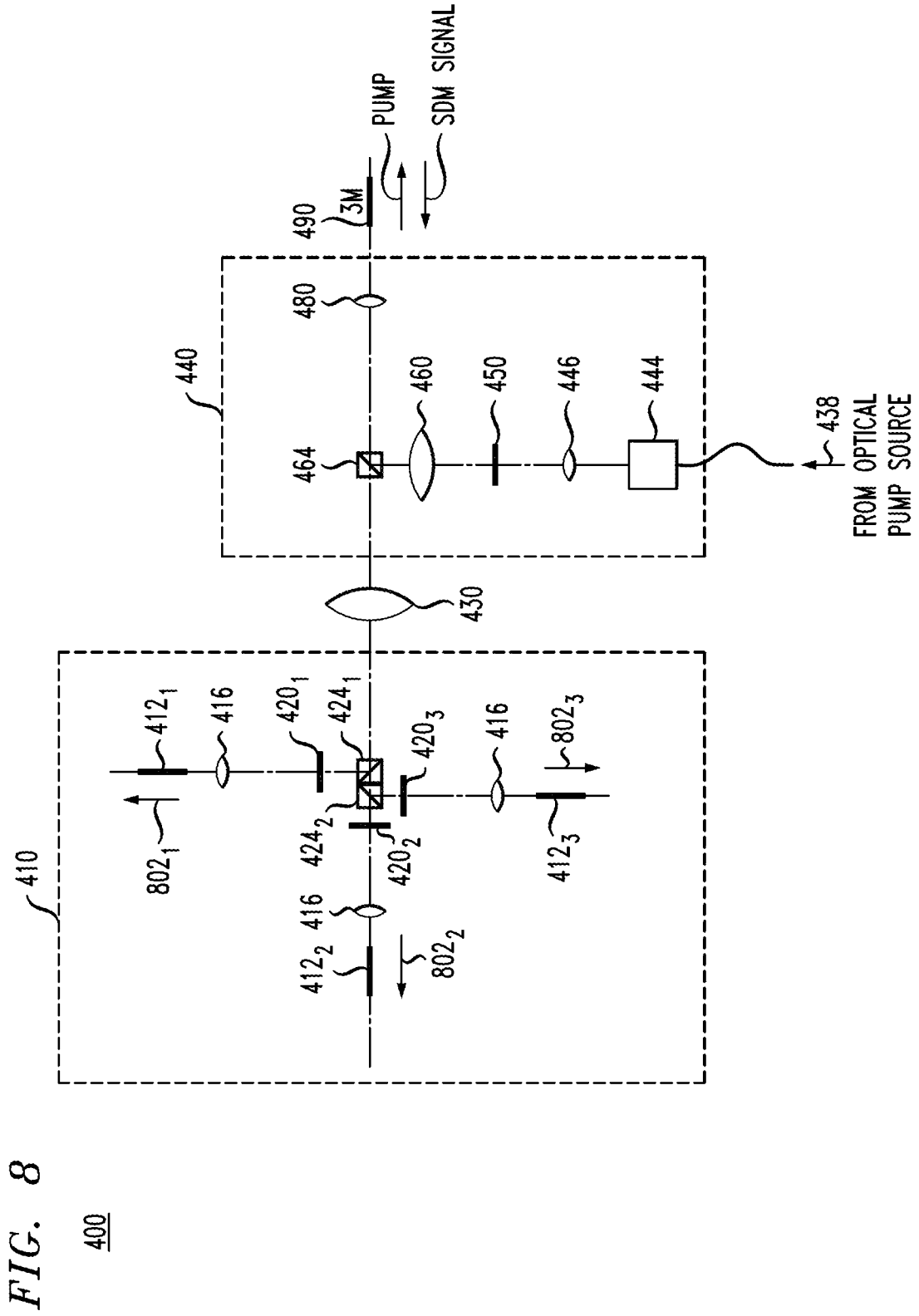
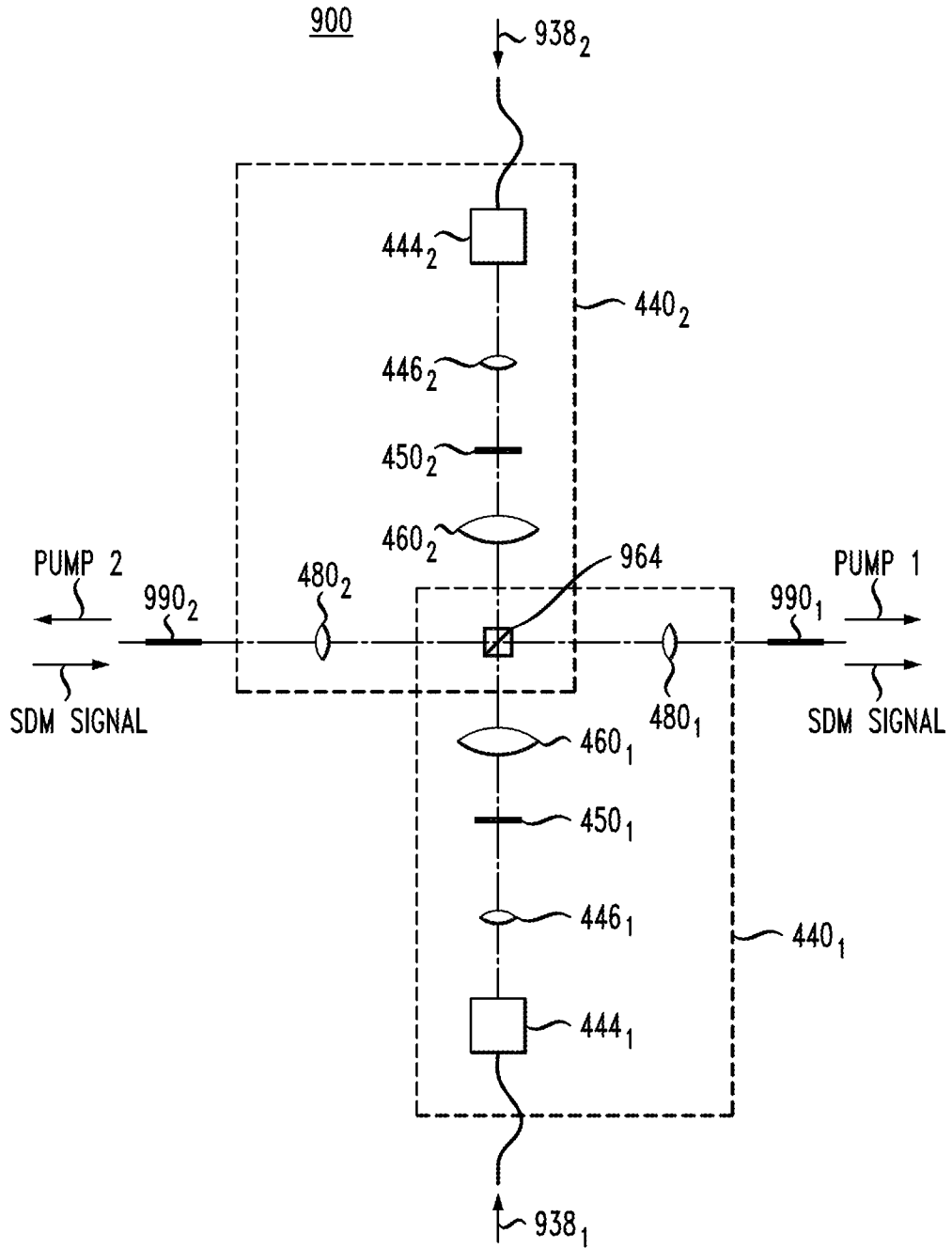


FIG. 8

400

FIG. 9



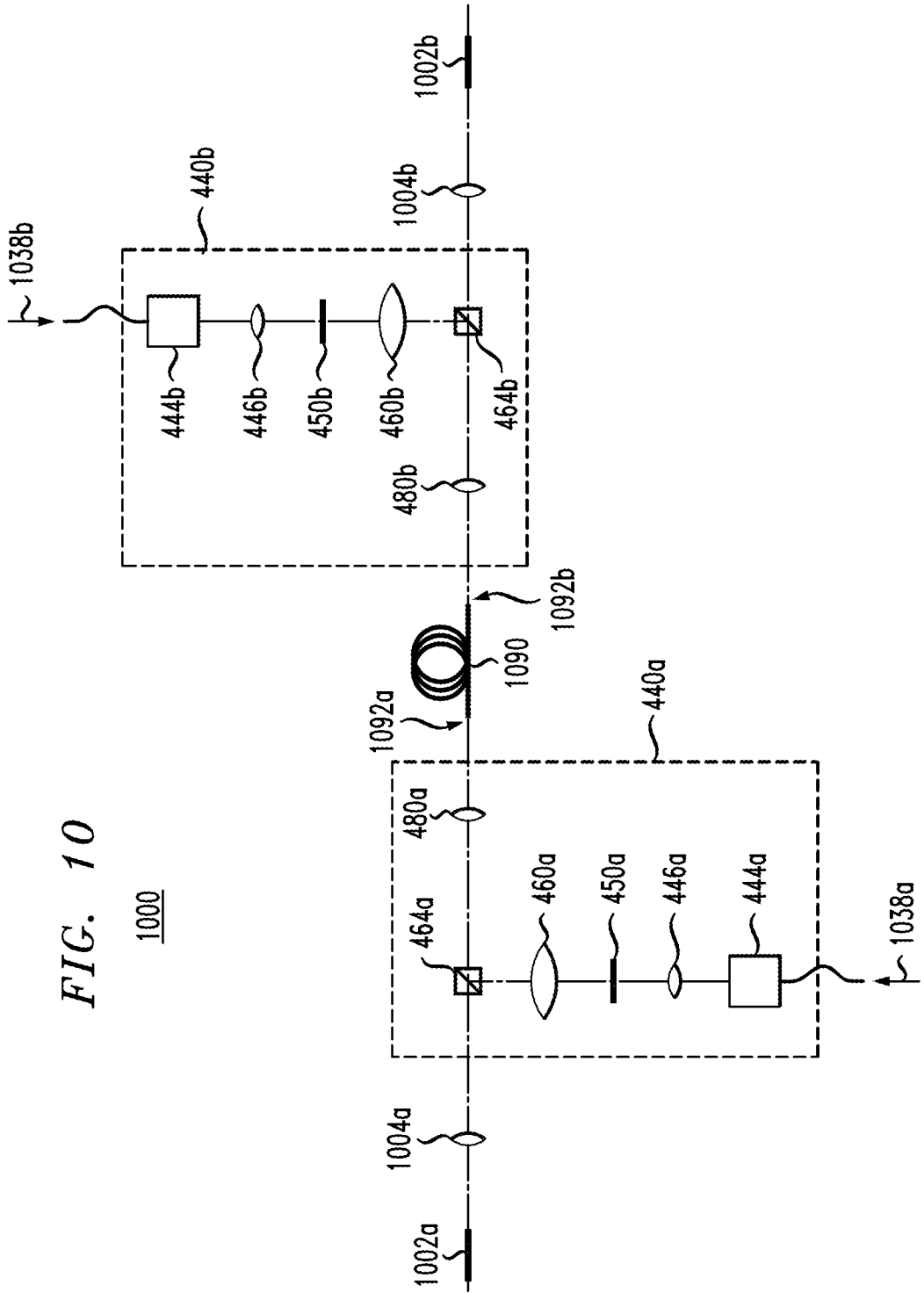


FIG. 10