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(54) **SURFACE-COATED CUTTING TOOL
HAVING HARD COATING LAYER THAT
EXHIBITS EXCELLENT CHIPPING
RESISTANCE**

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(57) **ABSTRACT**

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The hard coating layer includes at least a complex nitride or complex carbonitride layer expressed by the composition formula $(Ti_{1-x}Al_x)(C_yN_{1-y})$. The average Al content ratio x_{avg} , the average C content ratio y_{avg} satisfy $0.60 \leq x_{avg} \leq 0.95$ and $0 \leq y_{avg} \leq 0.005$, respectively, each of the x_{avg} and y_{avg} is in atomic ratio. The crystal grains constituting the complex nitride or complex carbonitride layer include a crystal grain having the cubic structure. Predetermined average crystal grain misorientation and inclined angle distribution exist in the crystal grains having the cubic structure.

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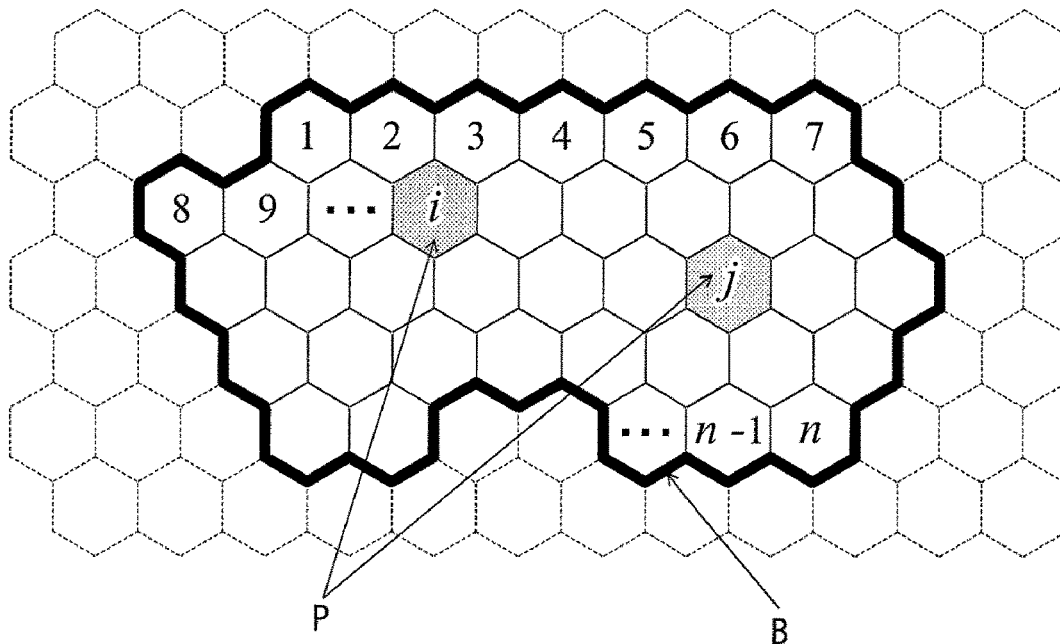


FIG. 1

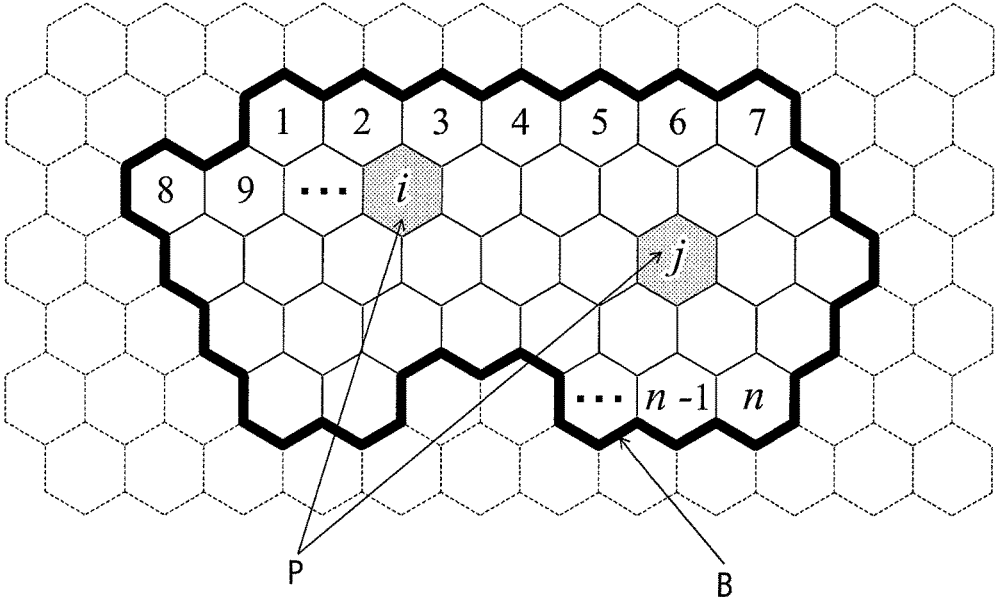


FIG. 2

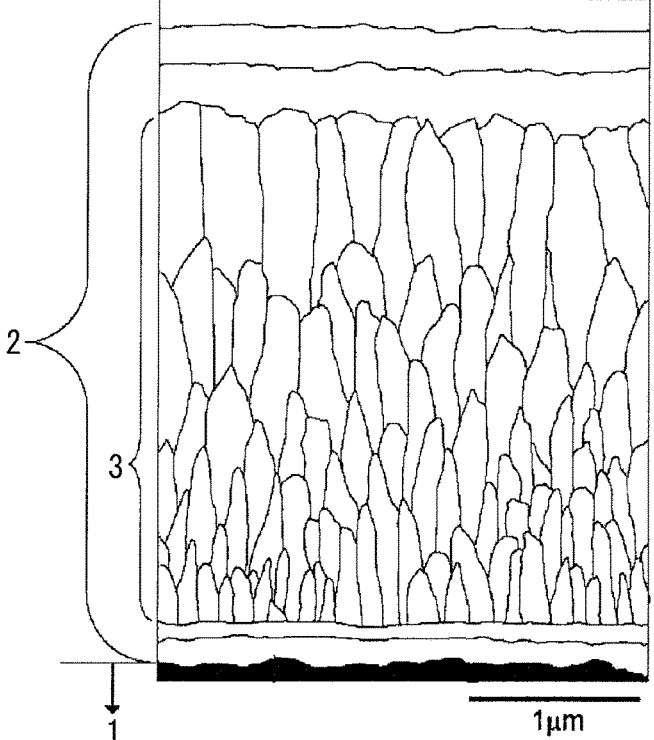


FIG. 3

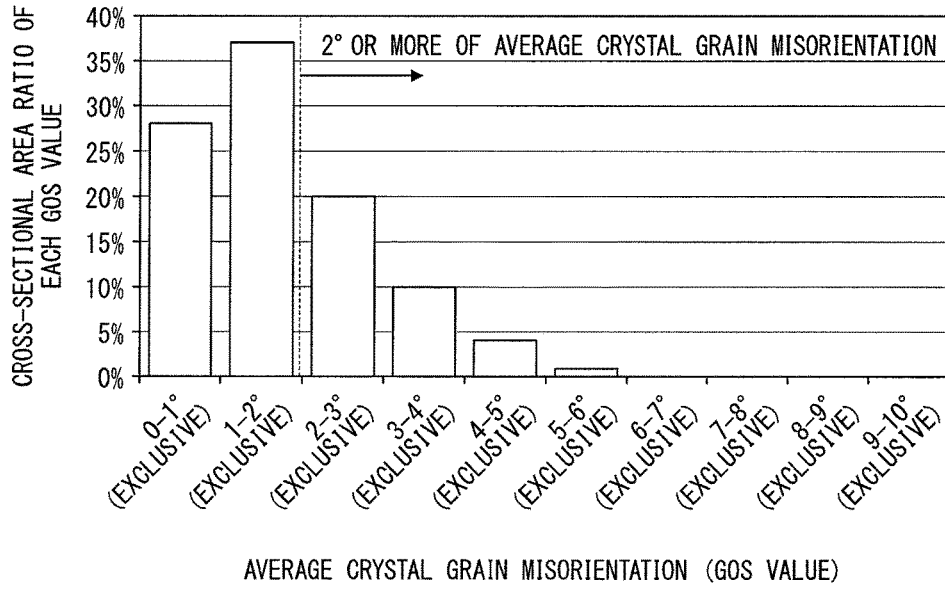


FIG. 4

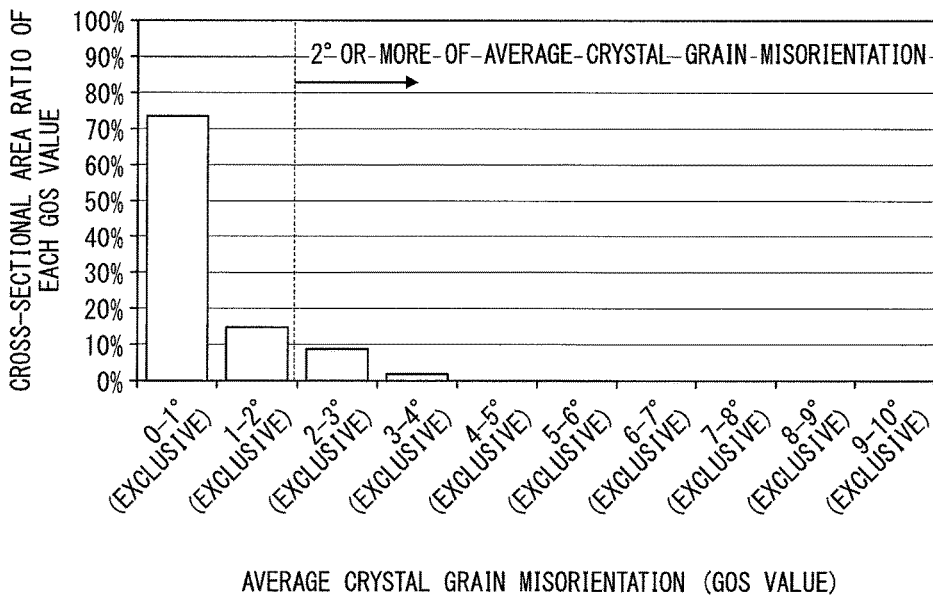


FIG. 5

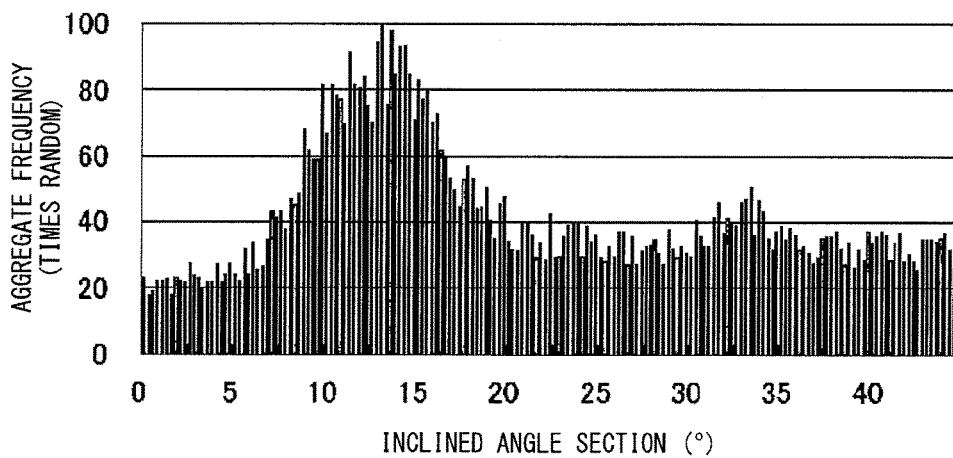
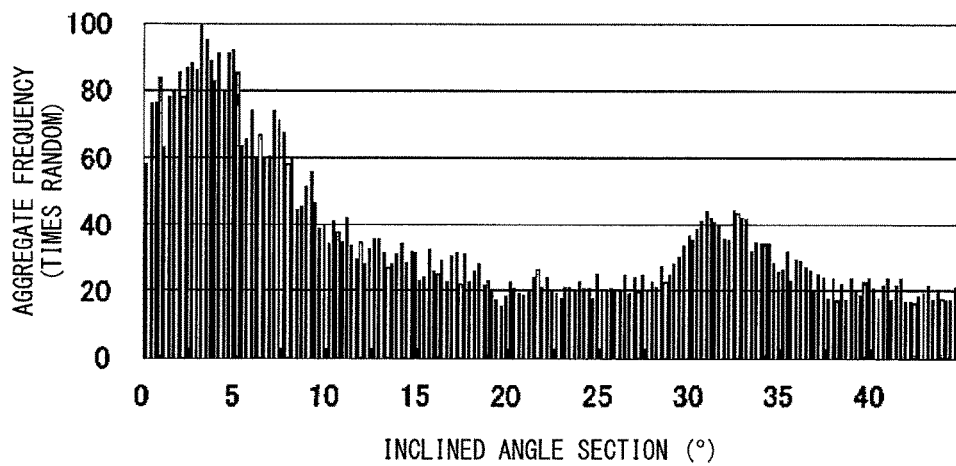


FIG. 6



**SURFACE-COATED CUTTING TOOL
HAVING HARD COATING LAYER THAT
EXHIBITS EXCELLENT CHIPPING
RESISTANCE**

CROSS-REFERENCE TO RELATED PATENT
APPLICATIONS

[0001] This application is a U.S. National Phase Application under 35 U.S.C. §371 of International Patent Application No. PCT/JP2015/065424, filed May 28, 2015, and claims the benefit of Japanese Patent Applications No. 2014-109881, filed May 28, 2014 and No. 2015-104042, filed May 21, 2015, all of which are incorporated by reference herein in their entireties. The International Application was published in Japanese on Dec. 3, 2015 as International Publication No. WO/2015/182711 under PCT Article 21(2).

FIELD OF THE INVENTION

[0002] The present invention relates to a surface-coated cutting tool (hereinafter, referred as coated tool) that exhibits excellent cutting performance for a long-term usage in a high-speed intermittent cutting work, in which high heat is generated on alloy steel or the like and impact load is exerted on the cutting edge, by having a hard coating layer with excellent chipping resistance.

BACKGROUND OF THE INVENTION

[0003] Conventionally, a coated tool, in which a surface of the tool body (hereinafter, collectively referred as the tool body) constituted from; tungsten carbide (hereinafter, referred as WC) based cemented carbide; titanium carbonitride (hereinafter, referred as TiCN) based cermet; or cubic boron nitride (hereinafter, referred as cBN) based ultra-high-pressure sintered material, is coated by a Ti—Al based complex nitride layer as a hard coating layer by the physical vapor deposition method, is known. In addition, it is known that such a hard coating layer exhibits excellent wear resistance.

[0004] However, several proposals for improving the hard coating layer are made since: the coated tool that the above-mentioned Ti—Al based complex nitride layer coated on has relatively excellent wear resistance; but abnormal abrasion such as chipping and the like is likely to be occurred in usage in the high-speed intermittent cutting condition.

[0005] For example, a surface-coated cutting tool, in which a hard coating layer is formed on the surface of the tool body, is disclosed in Patent Literature 1 (Japanese Unexamined Patent Application, First Publication No. 2012-20391 (A)). In the surface-coated cutting tool disclosed in Japanese Unexamined Patent Application, First Publication No. 2012-20391 (A), the hard coating layer is constituted from one or more layers. Then, in the case where T1 and T2 are defined as the thickness of the thinnest part of the hard coating layer in the ridgeline part of the cutting edge and the thickness of the hard coating layer in the location 1 mm apart from the ridgeline of the cutting edge toward the rake face side, respectively, in the cross section dissecting the cutting tool in a specific plane, the relationship of $T1 < T2$ is satisfied. In addition, Da and Db are set in specific parameter ranges, in the case where Da and Db are defined as the distance from the ridgeline of the cutting edge to the point a in the rake face

direction and the distance from the ridgeline of the cutting edge to the point b in the flank face direction, respectively, on the surface of the hard coating layer. In addition, the misalignment of the crystal orientations of the crystal grains constituting the hard coating layer is set to 5° or more and less than 10° in the region corresponding to 10% or more of the region E occupying the thick part of 0.1T1 to 0.9T1 from the surface in the hard coating layer from the point a to the point b. By having the configurations explained above, a surface-coated cutting tool having excellent wear resistance and defect resistance is obtained in Japanese Unexamined Patent Application, First Publication No. 2012-20391 (A).

[0006] In addition, it is disclosed that excellent defect resistance can be obtained in heavy cutting work by having a specifically-configured hard coating layer in Patent Literature 2 (Japanese Unexamined Patent Application, First Publication No. 2009-56540 (A)). In Japanese Unexamined Patent Application, First Publication No. 2009-56540 (A), the hard coating layer, which is constituted from an Al and Ti complex nitride layer satisfying the composition formula $(Al_{1-x}Ti_x)N$ (x is atomic ratio and in the range of 0.35 to 0.60), is provided on the surface of the tool body. When crystal orientation analysis is performed on the Al and Ti complex nitride layer with EBSD (Electron beam backward scattering diffraction device), the area ratio of crystal grains having the crystal orientation $\langle 100 \rangle$ in the range of 0 to 15° relative to the normal line direction of the polished surface of the tool body is 50% or more. In addition, the hard coating layer is constituted by the Al and Ti complex nitride layer showing the crystal alignment, in which the ratio of small angle grain boundaries ($0 < \theta < 15^\circ$) is 50% or more, when the angle between adjacent crystal grains is measured.

[0007] In the coated tool of Japanese Unexamined Patent Application, First Publication No. 2009-56540 (A), depositing TiAlN as the hard coating layer is disclosed. However, setting the Al content ratio to 0.65 or more is not disclosed or suggested.

[0008] From this point of view, a method to increase the Al content ratio x to about 0.9 by forming the hard coating layer by the chemical vapor deposition method is proposed.

[0009] For example, Patent Literature 3 (Japanese Unexamined Patent Application, First Publication No. 2011-516722 (A)) discloses that a $(Ti_{1-x}Al_x)N$ layer having the Al content ratio value x of 0.65 to 0.95 is deposited by performing chemical vapor deposition in the mixed reaction gas of $TiCl_4$; $AlCl_3$; and NH_3 , in the temperature range of $650^\circ C.$ to $900^\circ C.$ The purpose of Japanese Unexamined Patent Application, First Publication No. 2009-56540 (A) is improving the heat insulating effect by coating an extra Al_2O_3 layer on the above-mentioned $(Ti_{1-x}Al_x)N$ layer. Therefore, it is not clear what kind of influence on the cutting performance of the cutting tool can be obtained by forming the $(Ti_{1-x}Al_x)N$ layer having the Al content ratio value x increased to the level of 0.65 to 0.95.

[0010] In addition, for example, improving the heat resistance and fatigue strength of the coated tool by: coating the inner layer of a TiCN layer or a Al_2O_3 layer with an outer layer of a $(Ti_{1-x}Al_x)N$ layer (x is 0.65 to 0.90 in the atomic ratio), which is in a cubic structure or cubic structure including a hexagonal structure, by the chemical vapor deposition method; and having the outer layer with compressive stress of 100 to 1100 MPa, is proposed in Patent Literature 4 (Japanese Unexamined Patent Application, First Publication No. 2011-513594 (A)).

Problems to be Solved by the Present Invention

[0011] Recently, there is strong demand for power-saving and energy-saving in cutting work. Accordingly, the trend of cutting work is shifted toward even faster and highly efficient cutting. Thus, coated tools with even more excellent abnormal damage resistance such as chipping resistance; defect resistance; peeling resistance; and the like, is demanded. At the same time, coated tools with excellent wear resistance for a long-term usage is demanded.

[0012] However, the coated tools described in Japanese Unexamined Patent Application, First Publication No. 2012-20391 (A) and Japanese Unexamined Patent Application, First Publication No. 2009-56540 (A) have the problem that wear resistance and chipping resistance are not necessarily sufficient when it is applied to high-speed intermittent cutting of alloy steel, since Japanese Unexamined Patent Application, First Publication No. 2012-20391 (A) and Japanese Unexamined Patent Application, First Publication No. 2009-56540 (A) have no thought on increasing the Al content ratio in the hard coating layer made of the $(\text{Ti}_{1-x}\text{Al}_x)\text{N}$ layer.

[0013] On the other hand, the $(\text{Ti}_{1-x}\text{Al}_x)\text{N}$ layer deposited by the chemical vapor deposition method described in Japanese Unexamined Patent Application, First Publication No. 2011-516722 (A) has the problem that its toughness is inferior, even though a hard coating layer having a predetermined hardness and excellent wear resistance is obtained because: the Al content ratio x can be increased; and the cubic structure can be formed.

[0014] In addition, the coated tool described in Japanese Unexamined Patent Application, First Publication No. 2011-513594 (A) has the problem that abnormal damage resistance such as chipping, defect, peeling, and the like is likely to occur and the coated tool does not exhibit satisfactory cutting performance necessarily when it is applied to high-speed intermittent cutting of alloy steel or the like, since toughness of the coated tool in Japanese Unexamined Patent Application, First Publication No. 2011-513594 (A) is inferior, even though it has a predetermined hardness and excellent wear resistance.

[0015] Thus, the technical problem to be solved in the present invention, which is the purpose of the present invention, is to provide a coated tool that: has excellent toughness; and exhibits excellent chipping resistance and wear resistance for a long-term usage, even in the case where the coated tool is applied to high-speed intermittent cutting work or the like of alloy steel or the like.

SUMMARY OF THE INVENTION

Means to Solving the Problems

[0016] The inventors of the present invention conducted intensive studies in order to improve chipping resistance and wear resistance of the coated tool, on which a hard coating layer including at least a Ti and Al complex nitride or complex carbonitride (hereinafter, referred as “(Ti, Al)(C, N)” or “ $(\text{Ti}_{1-x}\text{Al}_x)(\text{C}_y\text{N}_{1-y})$ ”) is deposited by the chemical vapor deposition method, and obtained the following findings.

[0017] The conventional hard coating layer, which includes at least one layer of $(\text{Ti}_{1-x}\text{Al}_x)(\text{C}_y\text{N}_{1-y})$ layer and has a predetermined average layer thickness, has high wear resistance, in the case where the $(\text{Ti}_{1-x}\text{Al}_x)(\text{C}_y\text{N}_{1-y})$ layer is

formed in a columnar form perpendicular to the tool body. On the other hand, the higher the anisotropy of the $(\text{Ti}_{1-x}\text{Al}_x)(\text{C}_y\text{N}_{1-y})$ layer, the lower the toughness of the $(\text{Ti}_{1-x}\text{Al}_x)(\text{C}_y\text{N}_{1-y})$ layer. As a result, chipping resistance and defect resistance are lowered; and the coated tool cannot exhibit a sufficient wear resistance for a long-term usage. In addition, the service life of the tool is not satisfactory.

[0018] Under the circumstances described above, the inventors of the present invention further conducted intensive studies on the $(\text{Ti}_{1-x}\text{Al}_x)(\text{C}_y\text{N}_{1-y})$ layer constituting the hard coating layer, and succeeded to improve both hardness and toughness by introducing strain in crystal grains having the cubic crystal structure based on a completely novel idea, in which the $(\text{Ti}_{1-x}\text{Al}_x)(\text{C}_y\text{N}_{1-y})$ layer contains crystal grains having the cubic crystal structure and the average crystal grain misorientation of the crystal grains having the cubic crystal structure is set to 2° or more. As a result, a novel finding, which allows chipping resistance and defect resistance to be improved, is obtained.

[0019] In addition, they found that wear resistance is improved while toughness is retained by increasing the ratio of $\{100\}$ orientation on the surface side of the coating film compared to the surface side of the tool body in columnar crystal grains, as a novel finding.

[0020] Specifically, strain can be introduced in cubic crystal grains by satisfying the condition that: the hard coating layer includes at least a Ti and Al complex nitride or complex carbonitride layer, which is deposited by a chemical vapor deposition method; an average content ratio x_{avg} , which is an average content ratio of Al with respect to a total amount of Ti and Al, and an average content ratio y_{avg} , which is an average content ratio of C with respect to a total amount of C and N, satisfy $0.60 \leq x_{avg} \leq 0.95$, and $0 \leq y_{avg} \leq 0.005$, respectively, in a case where a composition formula of the Ti and Al complex nitride or complex carbonitride layer is expressed by $(\text{Ti}_{1-x}\text{Al}_x)(\text{C}_y\text{N}_{1-y})$, each of the x_{avg} and y_{avg} is in atomic ratio; there is a crystal grain with the cubic structure in the crystal grains constituting the complex nitride or complex carbonitride layer; and an area ratio of crystal grains having an average crystal grain misorientation of 2° or more relative to the Ti and Al complex nitride or complex carbonitride layer is 20% or more when crystal orientations of the crystal grains are analyzed along a vertical cross-sectional direction with an electron beam backward scattering diffraction device and the average crystal grain misorientation of the individual crystal grains is obtained. In addition, by setting a high ratio of the $\{100\}$ orientation of crystal grains on the surface side of the coating film compared to the surface side of the tool body, the wear resistance is improved while the toughness is retained. As a result, they found that chipping resistance and defect resistance are improved; and the cutting tool, on which the hard coating layer is formed, exhibits excellent wear resistance for a long-term usage.

[0021] The $(\text{Ti}_{1-x}\text{Al}_x)(\text{C}_y\text{N}_{1-y})$ layer configured as described above can be deposited by the chemical vapor deposition method explained below, in which the composition of the reaction gas is changed periodically on the surface of the tool body, for example.

[0022] To the chemical vapor deposition reaction apparatus used, each of the gas group A, which is made of NH_3 and H_2 , and the gas group B, which is made of TiCl_4 , $\text{Al}(\text{CH}_3)_3$, AlCl_3 , N_2 , and H_2 , is supplied through independent gas supplying pipes leading in the reaction apparatus. The gas

groups A and B are supplied in the reaction apparatus in such a way that the gas flows only in a shorter time than a specific period in a constant time interval in a constant period, for example. In this way, phase difference with the shorter time than the gas supplying time is formed in the gas supply of the gas groups A and B. Accordingly, the composition of the reaction gas on the surface of the tool body can be changed temporally, such as the gas group A (the first reaction gas), the mixed gas of the gas groups A and B (the second reaction gas), and the gas group B (the third reaction gas). In the present invention, there is no need to provide a long term exhausting process intending strict gas substitution. Thus, the temporal change of the composition of the reaction gas on the surface of the tool body can be changed among: a mixed gas, the major component of which is the gas group A (the first reaction gas); a mixed gas of the gas groups A and B (the second reaction gas); and a mixed, the major component of which is the gas group B (the third reaction gas) by: rotating the gas supply ports; rotating the tool bodies; or moving the tool body reciprocally as the gas supplying method, for example.

[0023] The $(\text{Ti}_{1-x}\text{Al}_x)(\text{C}_y\text{N}_{1-y})$ layer having a predetermined intended layer thickness is deposited, for example, by performing the thermal CVD method for a predetermined time on the surface of the tool body in the condition of: the gas group A including 4.0%-6.0% of NH_3 and 65%-75% of H_2 ; the gas group B including 0.6%-0.9% of AlCl_3 , 0.2%-0.3% of TiCl_4 , 0%-0.5% of $\text{Al}(\text{CH}_3)_3$, 12.5%-15.0% of N_2 , and balance H_2 ; the pressure of the reaction atmosphere being 4.5 kPa-5.0 kPa; the temperature of the reaction atmosphere being 700° C.-900° C.; the supply period being 1 second to 5 seconds; the gas supply time per one period being 0.15 second to 0.25 second; and the phase difference of the gas supply of the gas groups A and B being 0.10 second to 0.20 second.

[0024] By supplying the gas groups A and B in such a way that each of the gas groups A and B reach to the surface of the tool body in different timings with time difference as explained above; and by configuring the nitrogen raw material gas of the gas group A to 4.0% to 6.0% of NH_3 , and the metal chloride material gas or carbon material gas of the gas group B to 0.6% to 0.9% of AlCl_3 , 0.2% to 0.3% of TiCl_4 and 0% to 0.5% of $\text{Al}(\text{CH}_3)_3$, unevenness of the composition in the crystal grains and local strains of the crystal lattice by introduction of dislocation or point defect are formed. In addition, the extent of the $\{100\}$ orientation of the crystal grains on the surface side of the tool body and the surface side of the coating film can be varied. As a result, the inventors found that the toughness is improved significantly while the wear resistance is retained. As a result, they found that defect resistance and chipping resistance are improved particularly; and the hard coating layer exhibits excellent cutting performance for a long-term used even in high-speed intermittent cutting work of alloy steel or the like, in which intermittent and impact load is exerted on the cutting edge.

[0025] The present invention is made based on the above-described findings, and has aspects indicated below.

[0026] (1) A surface-coated cutting tool including: a tool body made of tungsten carbide-based cemented carbide, titanium carbonitride-based cermet, or cubic boron nitride-based ultra-high pressure sintered material; and a hard coating layer provided on a surface of the tool body, wherein

[0027] (a) the hard coating layer includes at least a Ti and Al complex nitride or complex carbonitride layer, which is

deposited by a chemical vapor deposition method and has an average layer thickness of 2 μm to 20 μm ; and an average content ratio x_{avg} , which is an average content ratio of Al with respect to a total amount of Ti and Al in the Ti and Al complex nitride or complex carbonitride layer in atomic ratio, and an average content ratio y_{avg} , which is an average content ratio of C with respect to a total amount of C and N in the Ti and Al complex nitride or complex carbonitride layer in atomic ratio, satisfy $0.60 \leq x_{avg} \leq 0.95$; and $0 \leq y_{avg} \leq 0.005$, respectively, in a case where a composition formula of the Ti and Al complex nitride or complex carbonitride layer is expressed by $(\text{Ti}_{1-x}\text{Al}_x)(\text{C}_y\text{N}_{1-y})$,

[0028] (b) the complex nitride or complex carbonitride layer includes at least a phase of Ti and Al complex nitride or complex carbonitride having a NaCl face-centered cubic structure,

[0029] (c) an area ratio of crystal grains having an average crystal grain misorientation of 2° or more relative to the Ti and Al complex nitride or complex carbonitride layer is 20% or more, when crystal orientations of crystal grains having the NaCl face-centered cubic structure in crystal grains constituting the complex nitride or carbonitride layer are analyzed along a vertical cross-sectional direction with an electron beam backward scattering diffraction device and the average crystal grain misorientation of the individual crystal grains is obtained, and

[0030] (d) when inclined angles of normal lines of $\{100\}$ plane as a crystal plane of the crystal grains relative to a normal line of a surface of the cutting tool body are measured dividing the complex nitride or complex carbonitride layer into two regions of an interface side region and a surface side region in a layer thickness direction; and frequencies in each of sections, in which measured inclined angles within a range of 0° to 45° relative to the normal line of the surface of the cutting tool among the measured inclined angles are divided in every 0.25° pitch, are tallied,

[0031] M_{deg} , which is the ratio of a sum of frequencies in a range of 0° to 12° in the interface side region to an overall frequency in an inclined angle distribution, is 10% to 40%, and

[0032] a highest peak is present in an inclined angles sections in a range of 0° to 12°, and in the surface side region and N_{deg} , which is the ratio of a sum of frequencies in a range of 0° to 12° in the surface side region to an overall frequency in an inclined angle distribution, is $M_{deg}+10\%$ to $M_{deg}+30\%$.

[0033] (2) The surface-coated cutting tool according to the above-described (1), wherein an area ratio of the Ti and Al complex nitride or complex carbonitride having the NaCl face-centered cubic structure in the Ti and Al complex nitride or complex carbonitride layer expressed by the $(\text{Ti}_{1-x}\text{Al}_x)(\text{C}_y\text{N}_{1-y})$ is 70% or more.

[0034] (3) The surface-coated cutting tool according to the above-described (1) or (2), wherein the complex nitride or complex carbonitride layer has a columnar structure, in which an average grain width W and an average aspect ratio A of each of the crystal grains having the cubic structure in the complex nitride or complex carbonitride layer are 0.1 μm to 2 μm and 2 to 10, respectively, when the complex nitride or complex carbonitride layer is observed along a vertical cross-sectional direction.

[0035] (4) The surface-coated cutting tool according to any one of the above-described (1) to (3), wherein a lower layer of a Ti compound layer, which is made of one or more

layers of: a Ti carbide layer; a Ti nitride layer; a Ti carbonitride layer; a Ti oxycarbide layer; and a Ti oxycarbonitride layer, is provided between the tool body and the Ti and Al complex nitride or complex carbonitride layer, an average total layer thickness of the lower layer being 0.1 μm to 20 μm .

[0036] (5) The surface-coated cutting tool according to any one of the above-described (1) to (4), wherein an upper layer including at least an aluminum oxide layer is formed on the complex nitride or complex carbonitride layer, an average total layer thickness of the upper layer being 1 μm to 25 μm .

[0037] (6) The surface-coated cutting tool according to any one of the above-described (1) to (5), wherein the complex nitride or complex carbonitride layer is deposited by a chemical vapor deposition method using at least trimethyl aluminum as a reaction gas component.

[0038] In the present application, "average crystal grain misorientation" means the GOS (Grain Orientation Spread) value, which is explained later.

Effects of the Invention

[0039] In the surface-coated cutting tool, which is an aspect of the present invention, (hereinafter, referred as "the surface-coated cutting tool of the present invention" or "the cutting tool of the present invention"), a surface-coated cutting tool includes: a tool body; and a hard coating layer provided on a surface of the tool body. In addition, the hard coating layer includes at least a Ti and Al complex nitride or complex carbonitride layer, which is deposited by a chemical vapor deposition method and has an average layer thickness of 2 μm to 20 μm ; and an average content ratio x_{avg} , which is an average content ratio of Al with respect to a total amount of Ti and Al, and an average content ratio y_{avg} , which is an average content ratio of C with respect to a total amount of C and N, satisfy $0.60 \leq x_{avg} \leq 0.95$; and $0 \leq y_{avg} \leq 0.005$, respectively, in a case where a composition formula of the Ti and Al complex nitride or complex carbonitride layer is expressed by $(\text{Ti}_{1-x}\text{Al}_x)(\text{C}_y\text{N}_{1-y})$, each of the x_{avg} and y_{avg} is in atomic ratio. In addition, there is a crystal grain with the cubic structure in the crystal grains constituting the complex nitride or complex carbonitride layer. In addition, an area ratio of crystal grains having an average crystal grain misorientation of 2° or more relative to the entire Ti and Al complex nitride or complex carbonitride layer is 20% or more, when crystal orientations of crystal grains are analyzed along a vertical cross-sectional direction with an electron beam backward scattering diffraction device and the average crystal grain misorientation of the individual crystal grains is obtained. In addition, when inclined angles of normal lines of $\{100\}$ plane as a crystal plane of the crystal grains relative to a normal line of a surface of the cutting tool body are measured dividing the complex nitride or complex carbonitride layer into two regions of an interface side region and a surface side region in a layer thickness direction; and frequencies in each of sections, in which measured inclined angles within a range of 0° to 45° relative to the normal line of the surface of the cutting tool among the measured inclined angles are divided in every 0.25° pitch, are tallied, M_{deg} , which is the ratio of a sum of frequencies in a range of 0° to 12° in the interface side region to an overall frequency in an inclined angle distribution, is 10% to 40%, and a highest peak is present in an inclined angles sections in a range of 0° to 12° , and in the

surface side region and N_{deg} , which is the ratio of a sum of frequencies in a range of 0° to 12° in the surface side region to an overall frequency in an inclined angle distribution, is $M_{deg}+10\%$ to $M_{deg}+30\%$. In addition, the complex nitride or complex carbonitride layer has a columnar structure, in which an average grain width W and an average aspect ratio A of each of the crystal grains having the cubic structure in the complex nitride or complex carbonitride layer are 0.1 μm to 2 μm and 2 to 10, respectively, when the complex nitride or complex carbonitride layer is observed from a direction perpendicular to the vertical cross-sectional side of the coating film. By having the configurations described above, strains are formed in the crystal grains having the cubic structure; and hardness and toughness of the crystal grains are improved. As a result, the technical effect improving chipping resistance without deteriorating wear resistance, is obtained; the hard coating layer exhibits excellent cutting performance for a long-term usage compared to the conventional hard coating layer; and lengthening the service life of the coated tool is achieved.

BRIEF DESCRIPTION OF THE DRAWINGS

[0040] FIG. 1 is a schematic illustration of the measurement method of the average crystal grain misorientation of crystal grains having the NaCl face-centered cubic structure (cubic) in the Ti and Al complex nitride or complex carbonitride layer of the coated tool of the present invention.

[0041] FIG. 2 is a schematic diagram of a film configuration showing the cross section of the Ti and Al complex nitride or complex carbonitride layer, which constitutes the hard coating layer of the surface-coated cutting tool of the present invention.

[0042] FIG. 3 shows an example of histogram of the area ratio of the average crystal grain misorientation (GOS value) in each of crystal grains having the cubic structure in a cross section of the Ti and Al complex nitride or complex carbonitride layer, which constitutes the hard coating layer of the coated tool of the present invention. The vertical dotted line in the histogram indicates the boundary line where the average crystal grain misorientation is 2° . Thus, bars on the right side of the vertical dotted line in FIG. 3 correspond to crystal grains having the average crystal grain misorientation of 2° or more.

[0043] FIG. 4 shows an example of histogram of the area ratio of the average crystal grain misorientation (GOS value) in each of crystal grains having the cubic structure in a cross section of the Ti and Al complex nitride or complex carbonitride layer, which constitutes the hard coating layer of Comparative Coated Tool. The vertical dotted line in the histogram indicates the boundary line where the average crystal grain misorientation is 2° . Thus, bars on the right side of the vertical dotted line in FIG. 4 correspond to crystal grains having the average crystal grain misorientation of 2° or more.

[0044] FIG. 5 is an example of the frequency distribution graph of the inclined angles of the $\{100\}$ plane drawn for the region on the interface side of the Ti and Al complex nitride or complex carbonitride layer, which constitutes the hard coating layer of the coated tool of the present invention. The tallied frequencies are shown as normalized relative values when the maximum tallied frequency is defined as 100.

[0045] FIG. 6 is an example of the frequency distribution graph of the inclined angles of the $\{100\}$ plane drawn for the region on the surface side of the Ti and Al complex nitride

or complex carbonitride layer, which constitutes the hard coating layer of the coated tool of the present invention. The tallied frequencies are shown as normalized relative values when the maximum tallied frequency is defined as 100.

DETAILED DESCRIPTION OF THE INVENTION

[0046] Embodiments of the present invention are explained below.

[0047] Average layer thickness of the complex nitride or complex carbonitride layer constituting the hard coating layer:

[0048] The hard coating layer of the surface-coated cutting tool of the present invention includes at least a Ti and Al complex nitride or complex carbonitride layer represented by the composition formula, $(\text{Ti}_{1-x}\text{Al}_x)(\text{C}_y\text{N}_{1-y})$, deposited by chemical vapor deposition. Although, this complex nitride or complex carbonitride layer has high hardness and excellent wear resistance, the complex nitride or complex carbonitride layer exhibits the traits particularly well when the average layer thickness of the complex nitride or complex carbonitride layer is 2 μm to 20 μm . The reason for that is: if the average layer thickness were less than 2 μm , sufficient wear resistance would not be obtained for a long-term usage due to the layer thickness being too thin; and if it exceeded 20 μm , chipping would likely occur because crystal grains of the Ti and Al complex nitride or complex carbonitride layer become easy to coarsen. Thus, the average layer thickness is set to 2 μm to 20 μm .

[0049] Composition of the complex nitride or complex carbonitride layer constituting the hard coating layer:

[0050] In the complex nitride or complex carbonitride layer constituting the hard coating layer of the surface-coated cutting tool of the present invention, x_{avg} , which is the average content ratio of Al with respect to a total amount of Ti and Al, and y_{avg} , which is an average content ratio of C with respect to a total amount of C and N, are adjusted to satisfy $0.60 \leq x_{avg} \leq 0.95$; and $0 \leq y_{avg} \leq 0.005$, respectively (each of the x_{avg} and y_{avg} is in atomic ratio).

[0051] The reason for these is that if the average Al content ratio x_{avg} were less than 0.60, hardness of the Ti and Al complex nitride or complex carbonitride layer would be deteriorated; and in the case where it is subjected to high-speed intermittent cutting of alloy steel or the like, its wear resistance would not be sufficient. On the other hand, if the average Al content ratio x_{avg} exceeded 0.95, the Ti content ratio would be decreased relatively. The reduction of the average Ti content ratio causes embrittlement to deteriorate chipping resistance. Thus, the average Al content ratio x_{avg} is set to $0.60 \leq x_{avg} \leq 0.95$.

[0052] In addition, when the content ratio y_{avg} (in the atomic ratio) of the C component included in the complex nitride or complex carbonitride layer is in the trace amount in the range of $0 \leq y_{avg} \leq 0.005$, adhesion of the complex nitride or complex carbonitride layer to the tool body or the lower layer is improved; and impact during cutting is absorbed by improvement of lubricity. As a result, defect resistance and chipping resistance of the complex nitride or complex carbonitride layer are improved. On the other hand, if the average content ratio of the C component y were deviated from the range of $0 \leq y_{avg} \leq 0.005$, defect resistance and chipping resistance would be deteriorated reversely due to reduction of toughness of the complex nitride or complex

carbonitride layer, and the deviation is not desirable. Thus, the average content ratio of the C component y is set to $0 \leq y_{avg} \leq 0.005$.

[0053] Average crystal grain misorientation of each of cubic crystal grains constituting the complex nitride or complex carbonitride layer (GOS value):

[0054] First, the complex nitride or complex carbonitride layer is analyzed along the vertical cross-sectional direction at the interval of 0.1 μm with an electron beam backward scattering diffraction device in the present invention. When there is crystal misorientation of 5° or more between adjacent measurement points P (hereinafter, referred as pixels), the mid-parting line is defined as the grain boundary B as shown in FIG. 1. The vertical cross-sectional direction means the direction perpendicular to the vertical cross-sectional direction. The vertical cross-section means the cross-section of the tool perpendicular to the surface of the tool body. Then, the region surrounded by a single crystal boundary is defined by one crystal grain. As an exemption, an independently-existing single pixel that has crystal misorientation of 5° or more to all of adjacent pixels is not regarded as a crystal grain. Only ones with connected pixels of 2 or more are regarded as a crystal grains.

[0055] Then, crystal misorientation is calculated in each of pixels in the crystal grain against to all of other pixels in the same crystal grain; and the averaged value of the calculated crystal misorientation is defined as the GOS value (Grain Orientation Spread). A schematic illustration is shown in FIG. 1. The GOS value is explained in detail in the document "Transactions of the Japan Society of Mechanical Engineers, Series A, Vol. 71, No. 712 (2005-12), Article No. 05-0367, p1722-1728", for example. The "average crystal grain misorientation" means this GOS value in the present specification. The mathematical formula expressing the GOS value is shown below. In the mathematical formula: n is the total number of pixels in the same crystal grain; i and j are unique numbers designated to each of different pixels in the crystal grains ($1 \leq i$, and $j \leq n$, in the example shown in FIG. 1); $\alpha_{ij(i \neq j)}$ is the crystal misorientation obtained from the crystal orientation in the pixel i and the crystal orientation in the pixel j .

$$GOS = \frac{\sum_{i,j=1}^n \alpha_{ij(i \neq j)}}{n(n-1)} \quad \text{[Mathematical formula 1]}$$

[0056] After analyzing in every 0.1 μm interval from the vertical cross-sectional direction with the electron beam backward scattering diffraction device, the histogram showing the area ratio of the average crystal grain misorientation can be made by: performing the measurement in the measurement range of 10 μm of the width and the layer thickness of the length, along the vertical cross-sectional direction in five different view fields; obtaining the total number of pixels belonging to the cubic crystal grain constituting the complex nitride or complex carbonitride layer; classing the average crystal grain misorientation with 1° incremental; tallying the number of pixels of crystal grains of each class of the average crystal grain misorientation; and dividing the each of tallied numbers by the above-mentioned total number of pixels. As a result, it is found that: crystal orientation in the crystal grain is not perfectly constant but varies

somewhat; and based on the obtained histogram, the area ratio of crystal grains having the average crystal grain misorientation of 2° or more relative to the entire Ti and Al complex nitride or complex carbonitride layer is 20% or more as in the area ratio in the coated tool of the present invention (see FIGS. 3 and 4.)

[0057] As explained above, in the crystal grains constituting the Al and Ti complex nitride or complex carbonitride layer of the surface-coated cutting tool of the present invention, there is a larger extent of variation (deviation) of crystal orientation within the crystal grain compared to the crystal grains constituting the conventional TiAlN layer. In other words, there are strains in the crystal grains. These strains contribute to improvement of hardness and toughness.

[0058] A preferable area ratio of crystal grains having the average crystal grain misorientation of 2° or more relative to the complex nitride or complex carbonitride layer is 30% to 60%. A more preferable area ratio of crystal grains having the average crystal grain misorientation of 2° or more relative to the complex nitride or complex carbonitride layer is 35% to 55%. An even more preferable area ratio of crystal grains having the average crystal grain misorientation of 2° or more relative to the complex nitride or complex carbonitride layer is 40% to 50%.

[0059] Crystal orientations in two regions on the interface side and the surface side equally dividing the complex nitride or complex carbonitride layer in the layer thickness direction:

[0060] The unique effect of the present invention, in which wear resistance is improved while toughness is retained, is obtained by crystal grains constituting the complex nitride or complex carbonitride layer being oriented to the normal line direction of the tool body surface, which is the $\{100\}$ plane, in a larger extent on the surface side of the complex nitride or complex carbonitride layer than the surface side of the tool body (the interface side).

[0061] However, if the increase rate of the orientation of the $\{100\}$ plane on the surface side relative to that on the interface side were less than 10%, the increase rate of the orientation of the $\{100\}$ plane would be too little. Thus, the effect of the present invention, in which wear resistance is improved while toughness is retained, cannot be obtained sufficiently. On the other hand, if it exceeded 30%, epitaxial growth of the crystal would be inhibited due to acute change of crystal orientations. Thus, toughness is reduced as a counter-productive result. In addition, it is found that if the orientation of the $\{100\}$ plane on the interface were less than 10%, the increase rate of the orientation of the $\{100\}$ plane on the surface side would be more than 30%; and if the orientation of the $\{100\}$ plane on the interface were more than 40%, the increase rate of the orientation of the $\{100\}$ plane on the surface side would be less than 10%. Therefore, it is configured in such a way that when inclined angles of normal lines of $\{100\}$ plane as a crystal plane of the crystal grains relative to a normal line of a surface of the cutting tool body are measured equally dividing the complex nitride or complex carbonitride layer into two regions of an interface side region and a surface side region in a layer thickness direction; and frequencies in each of sections, in which measured inclined angles within a range of 0° to 45° relative to the normal line of the surface of the cutting tool along the measured inclined angles are divided in every 0.25° pitch, are tallied: a) M_{deg} , which is the ratio of a sum of frequencies in a range of 0° to 12° in the interface side

region to an overall frequency in an inclined angle distribution, is 10% to 40%; and b) a highest peak is present in an inclined angles sections in a range of 0° to 12° , and in the surface side region and N_{deg} , which is the ratio of a sum of frequencies in a range of 0° to 12° in the surface side region to an overall frequency in an inclined angle distribution, is $M_{deg}+10\%$ to $M_{deg}+30\%$.

[0062] Area ratio of the Ti and Al complex nitride or complex carbonitride layer: The Ti and Al complex nitride or complex carbonitride layer represented by the formula $(Ti_{1-x}Al_x)(C_yN_{1-y})$ exhibits excellent wear resistance by having at least the phase of the Ti and Al complex nitride or complex carbonitride having the NaCl face-centered cubic structure. Particularly, when the area ratio exceeds 70%, excellent wear resistance is exhibited.

[0063] The average grain width W and the average aspect ratio A of each of the crystal grains having the cubic structure in the Ti and Al complex nitride or complex carbonitride layer:

[0064] The above-explained effect of improved toughness and wear resistance can be exhibited even more by configuring that the complex nitride or complex carbonitride layer has a columnar structure, in which the average grain width W and the average aspect ratio A of each of the crystal grains having the cubic structure in the complex nitride or complex carbonitride layer are $0.1 \mu\text{m}$ to $2 \mu\text{m}$ and 2 to 10, respectively.

[0065] The reasons for setting the average grain width W in the range of $0.1 \mu\text{m}$ to $2 \mu\text{m}$ is as follows. If it were less than $0.1 \mu\text{m}$, reactivity with the workpiece would be increased since the ratio of atoms belonging to the TiAlCN crystal grain boundaries among atoms exposed on the surface of the coating layer becomes larger. As a result, the hard coating layer cannot exhibit wear resistance sufficiently. On the other hand, if it exceeded $2 \mu\text{m}$, toughness is decreased since the ratio of atoms belonging to the TiAlCN crystal grain boundaries in the entire coating layer becomes a small value relatively. As a result, the hard coating layer cannot exhibit chipping resistance sufficiently. Thus, it is preferable that the average grain width W is set in the range of $0.1 \mu\text{m}$ to $2 \mu\text{m}$.

[0066] In addition, if the average aspect ratio A were less than 2, equiaxial crystals with a smaller aspect ratio would fall off since they do not have a sufficiently columnar structure. As a result, the hard coating layer cannot exhibit wear resistance sufficiently. On the other hand, if the average aspect ratio A exceeded 10, the strength of the crystal grain would not be retained; and chipping resistance is reduced as a counter-productive result. Thus, having the aspect ratio A exceeding 10 is not preferable. Therefore, it is preferable that the average aspect ratio A is set in the range of 2 to 10.

[0067] In the present invention, the average aspect ratio A is obtained as follows. First, the vertical cross-section of the hard coating layer is observed with a field-emission-type scanning electron microscope in the range of: $100 \mu\text{m}$ of the width and the height including the entire hard coating layer. The observation is performed from the vertical cross-section side perpendicular to the surface of the tool body. In the observation, the grain width "w" in the direction parallel to the surface of the body and the grain length "l" in the direction perpendicular to the surface of the body are measured. Then, the aspect ratio "a" of each of the crystal grains is calculated by the formula $a=l/w$. Then, the average value of the aspect ratio "a" obtained for each of the crystal

grains is calculated as the average aspect ratio A . Similarly, the average value of the grain width “ w ” obtained for each of the crystal grains is calculated as the average grain width W .

[0068] Lower and Upper Layers:

[0069] Essentially, a sufficient technical effect can be obtained by the complex nitride or complex carbonitride layer of the surface-coated cutting tool of the present invention. However, further more improved traits can be obtained by: providing the lower layer of a Ti compound layer, which is made of one or more layers of: a Ti carbide layer; a Ti nitride layer; a Ti carbonitride layer; a Ti oxycarbide layer; and a Ti oxycarbonitride layer, having the average total layer thickness of 0.1 μm to 20 μm ; or providing the upper layer including at least an aluminum oxide layer having the average layer thickness of 1 μm to 25 μm . In the case where the lower layer of a Ti compound layer, which is made of one or more layers of: a Ti carbide layer; a Ti nitride layer; a Ti carbonitride layer; a Ti oxycarbide layer; and a Ti oxycarbonitride layer, is provided, if the total average layer thickness of the lower layer were less than 0.1 μm , a sufficient effect of the lower layer would not be obtained. If it exceeded 20 μm , the crystal grains would become easy to coarsen; and chipping would likely occur. If the average total layer thickness of the upper layer including the aluminum oxide layer were less than 1 μm , a sufficient effect of the upper layer would not be obtained. On the other hand, if it exceeded 25 μm , the crystal grains would become easy to coarsen; and chipping would likely occur.

[0070] A schematic diagram of the cross section of the Ti and Al complex nitride or complex carbonitride layer constituting the hard coating layer of the surface-coated tool of the present invention is shown in FIG. 2.

[0071] Next, the coated tool of the present invention is explained with reference to Examples in detail.

Example 1

[0072] First, as raw material powders, the WC powder, the TiC powder, the TaC powder, the NbC powder, the Cr_3C_2 powder, and the Co powder, all of which had the average grain sizes of 1-3 μm , were prepared. Then, these raw material powders were blended in the blending composition shown in Table 1. Then, wax was added to the blended mixture, and further mixed in acetone for 24 hours with a ball mill. After drying under reduced pressure, the mixtures were press-molded into green compacts with a predetermined shape under pressure of 98 MPa. Then, the obtained green compacts were sintered in vacuum in the condition of 5 Pa vacuum at the predetermined temperature in the range of 1370-1470° C. for 1 hour retention. After sintering, the tool bodies A-C, which had the insert-shape defined by ISO-SEEN1203AFSN and made of WC-based cemented carbide, were produced.

[0073] In addition, as raw material powders, the TiCN powder (TiC/TiN=50/50 in mass ratio), the Mo_2C powder, the ZrC powder, the NbC powder, the WC powder, the Co powder, and the Ni powders, all of which had the average grain sizes of 0.5-2 μm , were prepared. These raw material powders were blended in the blending composition shown in Table 2. Then, with a ball mill, the obtained mixtures were subjected to wet-mixing for 24 hours. After drying, the mixtures were press-molded into green compacts under pressure of 98 MPa. The obtained green compacts were sintered in the condition of: in nitrogen atmosphere of 1.3

kPa; at a temperature of 1500° C.; and for 1 hour of the retention time. After sintering, the tool body D, which had the insert-shape defined by ISO-SEEN1203AFSN and made of TiCN-based cermet, was produced.

[0074] (a) Next, the coated tools of the present invention 1-15 were produced by forming the hard coating layers, which had the crystal grains having the cubic structure with the average crystal grain misorientation of 2° or more in the area ratios shown in Table 7, and were made of the $(\text{Ti}_{1-x}\text{Al}_x)(\text{C}_y\text{N}_{1-y})$ layers having the intended layer thicknesses shown in Table 7. The hard coating layers were formed by performing the thermal CVD method on the surfaces of the tool bodies A to D with a chemical vapor deposition apparatus in the forming conditions A to J shown in Tables 4 and 5 for a predetermined time. As the gas groups A and B, the gas group A made of NH_3 and H_2 included 4.0%-6.0% of NH_3 and 65%-75% of H_2 ; and the gas group B made of TiCl_4 , $\text{Al}(\text{CH}_3)_3$, AlCl_3 , N_2 , and H_2 included: 0.6%-0.9% of AlCl_3 , 0.2%-0.3% of TiCl_4 , 0%-0.5% of $\text{Al}(\text{CH}_3)_3$, 12.5%-15.0% of N_2 , and balance H_2 . The pressure of the reaction atmosphere was 4.5 kPa-5.0 kPa. The temperature of the reaction atmosphere was 700° C.-900° C. As the way to supply each of the gas groups A and B, the supply period was 1 second to 5 seconds; the gas supply time per one period was 0.15 second to 0.25 second; and the phase difference of the gas supply of the gas groups A and B was 0.10 second to 0.20 second.

[0075] In regard to the coated tools 6 to 13 of the present invention, the lower layer shown in Table 6 and/or the upper layer shown in Table 7 were formed in the forming conditions shown in Table 3.

[0076] In addition, for a comparison purpose, the hard coating layers including at least the Ti and Al complex nitride or complex carbonitride layer were deposited on the surfaces of the tool bodies A to D, in the conditions shown in Tables 3 to 5 and in the intended layer thicknesses (μm) shown in Table 8 as in the coated tools of the present invention 1-15. At this time, the hard coating layers were formed in such a way that the reaction gas composition on the surfaces of the tool bodies were not changed during deposition of the $(\text{Ti}_{1-x}\text{Al}_x)(\text{C}_y\text{N}_{1-y})$ layer to produce the coated tools 1 to 13 of Comparative Examples.

[0077] In regard to coated tools 6-13 of Comparative Example, the lower layer shown in Table 6 and/or the upper layer shown in Table 8 were formed in the forming condition shown in Table 3, as in the coated tools 6 to 13 of the present invention.

[0078] For purpose of reference, the reference coated tools 14 and 15 shown in Table 8 were produced by depositing the $(\text{Ti}_{1-x}\text{Al}_x)(\text{C}_y\text{N}_{1-y})$ layers of the reference examples on the surfaces of the tool bodies B and D in the intended layer thicknesses with a standard physical vapor deposition by arc-ion plating.

[0079] The conditions for the arc-ion plating used for deposition in the reference example were as explained below.

[0080] (a) The tool bodies B and C were subjected to ultrasonic cleaning in acetone. Then, the cleaned tool bodies B and C in a dried state were set along the outer peripheral part in positions spaced away from the central axis in a predetermined distance in the radius direction on the rotating table in the arc-ion plating apparatus. As the cathode electrode (vaporization source), an Al—Ti alloy with a predetermined composition was placed.

[0081] (b) Inside of the apparatus was heated to 500° C. by a heater while retaining vacuum less than 10^{-2} Pa by exhausting atmosphere in the apparatus. Then, direct current bias voltage of -1000V was applied to the tool bodies rotating and orbiting on the rotation table. At the same time, arc discharge was generated by flowing current of 200 A between the cathode electrode made of the Al—Ti alloy and the anode electrode. By following the procedure described above, Al and Ti ions were formed in the apparatus to perform bombard cleaning on the surfaces of the tool bodies.

[0082] (c) Next, direct current bias voltage of -50V was applied to the tool bodies rotating and orbiting on the rotating table while turning the atmosphere in the apparatus to the reaction atmosphere of 4 Pa by introducing nitrogen gas as a reaction gas in the apparatus. At the same time, arc discharge was generated by flowing current of 120 A between the cathode electrode (vaporization source) made of the Al—Ti alloy and the anode electrode. By following above-described procedure, the (Ti, Al)N layers with the intended compositions and the intended average layer thicknesses shown in Table 8 were deposited on the surfaces of the tool bodies and the coated tools of the reference example 14 and 15 were produced.

[0083] The vertical cross sections to the tool bodies of each constituent layer of: the coated tools of the present invention 1-15; cutting tools 1-13 of Comparative Example; and the reference coated tools 14 and 15, were measured by using a scanning electron microscope (magnifying power: $\times 5000$). The average layer thicknesses were obtained by averaging layer thicknesses measured at 5 points within the observation viewing field. In any measurement, the obtained average layer thickness was practically the same as the intended layer thicknesses shown in Tables 7 and 8.

[0084] In regard to the average Al content ratio, x_{avg} , of the complex nitride layer or the complex carbonitride layer, an electron beam was irradiated to the samples by using EPMA (Electron-Probe-Micro-Analyser). Then, the average Al content ratio, x_{avg} , was obtained from 10-point average of the analysis results of the characteristic X-ray in the surface-polished samples. The average C content ratio, y_{avg} , was obtained by secondary-ion-mass-spectroscopy (SIMS). An ion beam was irradiated on the range of $70\ \mu\text{m} \times 70\ \mu\text{m}$ from the front surface side of the sample. In regard to the components released by sputtering effect, concentration measurement in the depth direction was performed. The average C content ratio, y_{avg} , indicates the average value in the depth direction of the Ti and Al complex nitride layer or complex carbonitride layer. In the C content ratio, the C content ratio inevitably included without intended usage of the gas including C as the gas raw material was excluded. More specifically, the content ratio of the C component (in the atomic ratio) in the complex nitride or complex carbonitride layer when the supply amount of $\text{Al}(\text{CH}_3)_3$ was set to 0 was obtained as the inevitable C content ratio. Then, the value of the content ratio of the C component (in the atomic ratio) in the complex nitride or complex carbonitride layer obtained when $\text{Al}(\text{CH}_3)_3$ was intentionally supplied subtracted by the above-described inevitable C component ratio was obtained as y_{avg} .

[0085] Then, crystal orientation of each of crystal grains having the cubic structure constituting the Ti and Al complex nitride or complex carbonitride layer, was analyzed along the vertical cross-sectional direction with an electron beam backward scattering diffraction device. When there

was crystal misorientation of 5° or more between adjacent pixels, the mid-parting line was defined as the grain boundary, and the region surrounded by a single boundary was defined by one crystal grain. Then, the average crystal grain misorientation between a pixel in the crystal grain and all of other pixels in the same crystal grains was obtained. Mapping was performed by classing the obtained average crystal grain misorientation in every 1° in the range from 0° to 10°, such as: more than 0° to less than 1°; more than 1° to less than 2°; more than 2° to less than 3°; more than 3° to less than 4°; and the like. Based on the mapping diagram, the area ratio of the crystal grains having the average crystal grain misorientation of 2° or more occupying the entire Ti and Al complex nitride or complex carbonitride layer was obtained. The results are shown in Tables 7 and 8.

[0086] An example of the histogram of the average crystal gain misorientation (GOS value) measured in the coated tool 2 of the present invention is shown in FIG. 3. In addition, an example of the histogram of the average crystal gain misorientation measured in the coated tool 2 of Comparative Example is shown in FIG. 4.

[0087] In regard to the frequency distribution graph of the inclined angles in the hard coating layer, the frequencies in the range of 0° to 12° were obtained as follows. First, the cross sections of the hard coating layer made of the Ti and Al complex nitride or complex carbonitride layer in the cubic structure were set in the lens barrel of a field-emission-type scanning electron microscope in the state where the cross sections were polished. Then, analysis was performed on the polished surfaces dividing the analysis field in two regions, which were the region on the tool body side (interface side) and the region on the surface side, in the thickness direction. Electron beam was irradiated on each of crystal grains having the cubic lattice in the measurement field with the incident angle of 70°, the acceleration voltage of 10 kV, and the irradiation current of 1 nA in the interval of 0.1 μm /step, on five viewing fields covering: the interface side region and the surface side region in the measurement range in the direction perpendicular to the surface of the tool body; and the width of 10 μm in the direction parallel to the surface of the tool body. Then, by using an electron beam backward scattering diffraction device, the inclined angles of the normal line of the {100} plane, which was a crystal plane of the crystal grain, relative to the normal line of the surface of the tool body (the direction perpendicular to the surface of the tool body in the polished cross-sectional surface) were measured. Then, based on the measured results, the inclined angles in the range of 0 to 45° among the measured inclined angles were divided into sections in every 0.25° pitch; and the frequency in each section was tallied to draw the frequency distribution graph. The results are shown in Tables 7 and 8.

[0088] In addition, analysis was performed in the interval of 0.1 μm from the vertical cross-sectional direction with the electron beam backward scattering diffraction device. Measurement was performed in the field covering: the width of 10 μm ; and the measurement range of the layer thickness from the vertical cross-sectional direction on 5 viewing fields. Then, the number of all pixels belonging to the cubic grains constituting the complex nitride or complex carbonitride layer was obtained. Then, the area ratio of the cubic grains constituting the complex nitride or complex carbonitride layer was obtained based on the ratio of the number of the all pixels belonging to the cubic grains constituting the complex nitride or complex carbonitride layer to the number of all pixels measured in the measurement of the hard coating layer in the above-mentioned 5 viewing fields.

TABLE 1

Type	Blending composition (mass %)						
	Co	TiC	TaC	NbC	Cr ₃ C ₂	WC	
Tool body	A	8.0	1.5	—	3.0	0.4	balance
	B	8.5	—	1.8	0.2	—	balance
	C	7.0	—	—	—	—	balance

TABLE 2

Type	Blending composition (mass %)							
	Co	Ni	ZrC	NbC	Mo ₂ C	WC	TiCN	
Tool body	D	8	5	1	6	6	10	balance

TABLE 3

Layer constituting the hard coating layer			Forming condition (pressure and temperature of the reaction atmosphere are shown as kPa and ° C., respectively)			
Type	Formation		Reaction atmosphere			
	symbol	Reaction gas composition	Pressure	Temperature		
(Ti _{1-x} Al _x)(C _y N _{1-y}) layer	TiAlCN	TiAlCN	Refer Table 4	Refer Table 5	Refer Table 5	
Ti compound layer	TiC	TiC	TiCl ₄ : 4.2%, CH ₄ : 8.5%, H ₂ : balance	7	900	
	TiN	TiN-1	TiCl ₄ : 4.2%, N ₂ : 30%, H ₂ : balance	30	850	
		TiN-2	TiCl ₄ : 4.2%, N ₂ : 35%, H ₂ : balance	50	900	
		TiN-3	TiCl ₄ : 4.2%, N ₂ : 30%, H ₂ : balance	30	780	
		1-TiCN-1	TiCl ₄ : 2%, CH ₃ CN: 0.7%, N ₂ : 10%, H ₂ : balance	7	900	
		1-TiCN-2	TiCl ₄ : 2%, CH ₃ CN: 0.7%, N ₂ : 10%, H ₂ : balance	7	780	
		TiCN	TiCN	TiCl ₄ : 2%, CH ₄ : 1%, N ₂ : 15%, H ₂ : balance	13	900
		TiCO	TiCO	TiCl ₄ : 4.2%, CO: 4%, H ₂ : balance	7	900
		TiCNO	TiCNO	TiCl ₄ : 2%, CO: 1%, CH ₄ : 1%, N ₂ : 5%, H ₂ : balance	13	900
Al ₂ O ₃ layer	Al ₂ O ₃	Al ₂ O ₃	AlCl ₃ : 2.2%, CO ₂ : 5.5%, HCl: 2.2%, H ₂ S: 0.2%, H ₂ : balance	7	900	

TABLE 4

Process type	Formation of the hard coating layer	Forming condition (The reaction gas composition indicates the ratio to the sum of gas groups A and B)	
		Formation symbol	Reaction gas composition of the gas group B (volume %)
Deposition process in the present invention	A	NH ₃ : 5.0%, H ₂ : 70%	AlCl ₃ : 0.7%, TiCl ₄ : 0.2%, N ₂ : 13%, Al(CH ₃) ₃ : 0%, H ₂ : balance
	B	NH ₃ : 6.0%, H ₂ : 75%	AlCl ₃ : 0.7%, TiCl ₄ : 0.3%, N ₂ : 15%, Al(CH ₃) ₃ : 0%, H ₂ : balance
	C	NH ₃ : 4.0%, H ₂ : 65%	AlCl ₃ : 0.9%, TiCl ₄ : 0.3%, N ₂ : 14%, Al(CH ₃) ₃ : 0.5%, H ₂ : balance
	D	NH ₃ : 6.0%, H ₂ : 70%	AlCl ₃ : 0.6%, TiCl ₄ : 0.2%, N ₂ : 12.5%, Al(CH ₃) ₃ : 0%, H ₂ : balance
	E	NH ₃ : 4.0%, H ₂ : 75%	AlCl ₃ : 0.8%, TiCl ₄ : 0.3%, N ₂ : 13%, Al(CH ₃) ₃ : 0%, H ₂ : balance
	F	NH ₃ : 5.0%, H ₂ : 65%	AlCl ₃ : 0.7%, TiCl ₄ : 0.3%, N ₂ : 14.5%, Al(CH ₃) ₃ : 0.2%, H ₂ : balance
	G	NH ₃ : 5.0%, H ₂ : 70%	AlCl ₃ : 0.6%, TiCl ₄ : 0.2%, N ₂ : 13.5%, Al(CH ₃) ₃ : 0%, H ₂ : balance
	H	NH ₃ : 5.0%, H ₂ : 70%	AlCl ₃ : 0.9%, TiCl ₄ : 0.2%, N ₂ : 12.8%, Al(CH ₃) ₃ : 0%, H ₂ : balance
	I	NH ₃ : 5.0%, H ₂ : 70%	AlCl ₃ : 0.6%, TiCl ₄ : 0.3%, N ₂ : 13.5%, Al(CH ₃) ₃ : 0.4%, H ₂ : balance
Deposition process in Comparative Example	J	NH ₃ : 5.0%, H ₂ : 70%	AlCl ₃ : 0.8%, TiCl ₄ : 0.3%, N ₂ : 14%, Al(CH ₃) ₃ : 0%, H ₂ : balance
	A'	NH ₃ : 5.0%, H ₂ : 70%	AlCl ₃ : 0.7%, TiCl ₄ : 0.2%, N ₂ : 13%, Al(CH ₃) ₃ : 0%, H ₂ : balance
	B'	NH ₃ : 6.0%, H ₂ : 75%	AlCl ₃ : 0.7%, TiCl ₄ : 0.3%, N ₂ : 15%, Al(CH ₃) ₃ : 0%, H ₂ : balance
	C'	NH ₃ : 4.0%, H ₂ : 65%	AlCl ₃ : 0.9%, TiCl ₄ : 0.3%, N ₂ : 14%, Al(CH ₃) ₃ : 0.5%, H ₂ : balance
	D'	NH ₃ : 6.0%, H ₂ : 70%	AlCl ₃ : 0.6%, TiCl ₄ : 0.2%, N ₂ : 12.5%, Al(CH ₃) ₃ : 0%, H ₂ : balance
	E'	NH ₃ : 4.0%, H ₂ : 75%	AlCl ₃ : 0.8%, TiCl ₄ : 0.3%, N ₂ : 13%, Al(CH ₃) ₃ : 0%, H ₂ : balance
	F'	NH ₃ : 5.0%, H ₂ : 65%	AlCl ₃ : 0.7%, TiCl ₄ : 0.3%, N ₂ : 14.5%, Al(CH ₃) ₃ : 0.2%, H ₂ : balance
	G'	NH ₃ : 5.0%, H ₂ : 70%	AlCl ₃ : 0.6%, TiCl ₄ : 0.2%, N ₂ : 13.5%, Al(CH ₃) ₃ : 0%, H ₂ : balance
	H'	NH ₃ : 5.0%, H ₂ : 70%	AlCl ₃ : 0.9%, TiCl ₄ : 0.2%, N ₂ : 12.8%, Al(CH ₃) ₃ : 0%, H ₂ : balance
	I'	NH ₃ : 5.0%, H ₂ : 70%	AlCl ₃ : 0.6%, TiCl ₄ : 0.3%, N ₂ : 13.5%, Al(CH ₃) ₃ : 0.4%, H ₂ : balance
	J'	NH ₃ : 5.0%, H ₂ : 70%	AlCl ₃ : 0.8%, TiCl ₄ : 0.3%, N ₂ : 14%, Al(CH ₃) ₃ : 0%, H ₂ : balance

TABLE 5

Formation of the hard coating layer		Forming condition (Pressure and temperature of the reaction atmosphere are shown as kPa and ° C., respectively)					Phase difference between the gas groups A and B Reaction atmosphere	
		Gas group A		Gas group B				
Process type	Formation symbol	Supply period (second)	Supply time per one period (second)	Supply period (second)	Supply time per one period (second)	(second)	Pressure	Temperature
Deposition process in the present invention	A	1	0.2	1	0.2	0.1	4.7	800
	B	3	0.15	3	0.15	0.15	4.5	800
	C	2	0.25	2	0.25	0.2	5	700
	D	5	0.2	5	0.2	0.1	4.7	800
	E	4	0.2	4	0.2	0.15	5	850
	F	2.5	0.2	2.5	0.2	0.2	4.5	800
	G	1.5	0.15	1.5	0.15	0.2	4.7	700
	H	1.2	0.25	1.2	0.25	0.1	4.7	900
	I	4.5	0.2	4.5	0.2	0.15	4.7	800
	J	2.5	0.2	2.5	0.2	0.2	4.7	750
Deposition process in Comparative Example	A'	—	—	—	—	—	4.7	800
	B'	—	—	—	—	—	4.5	800
	C'	—	—	—	—	—	5	700
	D'	—	—	—	—	—	4.7	800
	E'	—	—	—	—	—	5	850
	F'	—	—	—	—	—	4.5	800
	G'	—	—	—	—	—	4.7	700
	H'	—	—	—	—	—	4.7	900
	I'	—	—	—	—	—	4.7	800
	J'	—	—	—	—	—	4.7	750

TABLE 6

Type	Tool body symbol	Hard coating layer (the number at the bottom indicates the intended average layer thickness (μm) of the layer)		
		1st layer	2nd layer	3rd layer
Coated tool of the present invention, coated tool of Comparative Example, and reference coated tool	1	A	—	—
	2	B	—	—
	3	C	—	—
	4	D	—	—
	5	A	—	—
	6	B	TiC (0.5)	—
	7	C	TiN-1 (0.3)	—
	8	D	TiN-1 (0.5)	1-TiCN-1 (4)

TABLE 6-continued

Type	Tool body symbol	Hard coating layer (the number at the bottom indicates the intended average layer thickness (μm) of the layer)			
		1st layer	2nd layer	3rd layer	
9	A	TiN-1 (0.3)	1-TiCN-1 (2)	TiCN (0.7)	
	B	—	—	—	
	10	C	TiN-1 (0.5)	—	—
		D	TiC (1)	—	—
	11	A	TiN-1 (0.1)	—	—
	12	B	—	—	—
	13	C	—	—	—
14	—	—	—	—	
15	—	—	—	—	

TABLE 7

		Ti and Al complex nitride, carbonitride layer (Ti _{1-x} Al _x (C _z N _{1-z}))										Upper layer	
		Hard coating layer											
Type	Tool body symbol	Formation symbol of TiAlCN deposition process (refer Table 4)	Al content x _{avg}	Area ratio of crystal grains having the average crystal grain misorientation of 2° or more (%)	Area ratio of cubic crystals (%)	Average grain width (μm)	Average aspect ratio of crystal grains	Frequency distribution ratio of inclined angle of the normal line of the {100} plane in the range of 0° to 12° in the interface side region M _{deg}	Frequency distribution ratio of inclined angle of the normal line of the {100} plane in the range of 0° to 12° in the surface side region N _{deg}	Inclined angle section showing the highest peak in the surface side region (°)	Intended thickness (μm)	Thickness 1st layer (μm)	Thickness 2nd layer
Coated tool of the present invention	1 A	A	0.93	46	100	0.8	5.0	15	30	5.25-5.50	5	—	—
	2 B	B	0.78	35	100	0.6	2.6	26	48	3.00-3.25	6	—	—
	3 C	C	0.72	20	100	0.2	3.2	21	40	4.00-4.25	2	—	—
	4 D	D	0.70	55	88	0.1	2.3	38	51	6.75-7.00	8	—	—
	5 A	E	0.95	41	77	1.1	1.5	32	54	2.75-3.00	3	—	—
	6 B	F	0.65	30	100	0.4	10.0	10	38	8.00-8.25	4.5	—	—
	7 D	G	0.86	51	100	1.1	2.0	29	59	4.75-5.00	6	—	—
	8 C	H	0.90	36	65	0.8	2.2	16	39	10.00-10.25	3.5	—	—
	9 A	I	0.60	63	100	0.3	2.3	27	45	4.50-4.75	7	—	—

TABLE 7-continued

		Hard coating layer											Upper layer	
		Ti and Al complex nitride, carbonitride layer (Ti _{1-x} Al _x C _z N _{1-y-z})												
Type	Tool body symbol	Formation symbol of deposition process	Al content ratio X _{avg}	C content ratio Y _{avg}	Area ratio of crystal grains having the average crystal grain misorientation of 2° or more (%)	Area ratio of the cubic crystals (%)	Average grain width W of crystal grains (μm)	Area ratio of the {100} plane in the range of 0° to 12° in crystal grains	Frequency distribution ratio of inclined angle of the normal line of the {100} plane in the range of 0° to 12° in the interface side region M _{deg}	Frequency distribution ratio of inclined angle of the normal line of the {100} plane in the range of 0° to 12° in the surface side region N _{deg}	Inclined angle showing the highest peak in the surface side region (°)	Intended layer thickness (μm)	1st layer thickness (μm)	2nd layer thickness (μm)
10	B	J	0.66	less than 0.0001	37	91	0.10	3.1	40	61	2.00-2.25	5	Al ₂ O ₃ (2.5)	—
11	C	A	0.94	less than 0.0001	43	96	1.1	3.1	17	29	4.50-4.75	4	TiCN (0.5)	Al ₂ O ₃ (3)
12	D	B	0.75	less than 0.0001	28	93	0.5	2.2	34	53	4.25-4.50	3	TiCO (1)	Al ₂ O ₃ (2)
13	A	C	0.69	less than 0.0025	23	95	0.7	2.1	29	58	2.75-3.00	2.5	TiCNO (0.3)	Al ₂ O ₃ (1)
14	B	D	0.68	less than 0.0001	58	92	0.4	5.1	37	52	6.00-6.25	6	—	—
15	C	E	0.94	less than 0.0001	44	83	0.9	3.2	24	44	2.50-2.75	3	—	—

TABLE 8

		Hard coating layer												
		Ti and Al complex nitride, carbonitride layer (Ti _{1-x} Al _x (C,N) _{1-y})												
Type	Tool body symbol	Formation of TiAlCN deposition process (refer Table)	Al content ratio x _{avg}	C content ratio y _{avg}	Area ratio of crystal grains having the average crystal grain misonorientation of 2° or more (%)	Area ratio of the average crystal grain width W of aspect ratio of 100 or more (%)	Average grain width W (μm)	Crystal grains ratio of aspect ratio of 100 or more (%)	Frequency distribution ratio of inclined angle of the normal line of the {100} plane in the range of 0° to 12° in the interface side region M _{deg}	Frequency distribution ratio of inclined angle of the normal line of the {100} plane in the range of 0° to 12° in the surface side region N _{deg}	Inclined section showing the highest peak in the surface side region (°)	Intended layer thickness (μm)	Upper layer (Numbers at the bottom indicate the average intended layer thickness (μm) of the layer)	
												1st layer thickness (μm)	2nd layer	
Coated tool of	1 A	A'	0.91	less than 0.0001	7	100	0.7	5.0	25	31	32.00-32.25	5	—	
Comparative Example	2 B	B'	0.80	less than 0.0001	5	100	0.4	0.8	24	28	23.25-23.50	6	—	
	3 C	C'	0.74	less than 0.0001	0	96	0.2	3.1	27	22	32.75-33.00	2	—	
	4 D	D'	0.58	less than 0.0001	6	85	0.2	1.2	34	28	16.25-16.50	8	—	
	5 A	E'	0.93	less than 0.0001	4	78	1.0	1.8	21	24	24.25-24.50	3	—	
	6 B	F'	0.54	less than 0.0001	5	100	0.4	1.5	22	17	41.50-41.75	4.5	—	
	7 D	G'	0.88	less than 0.0001	4	98	0.9	2.5	34	43	14.50-14.75	6	—	
	8 C	H'	0.91	less than 0.0001	4	63	0.8	1.5	19	23	28.25-28.50	3.5	—	
	9 A	I'	0.62	less than 0.0001	11	100	0.4	2.1	24	19	26.75-27.00	7	—	
	10 B	J'	0.67	less than 0.0001	5	93	0.08	0.5	33	37	14.25-14.50	5	Al ₂ O ₃ (2.5)	

TABLE 8-continued

		Ti and Al complex nitride, carbonitride layer (Ti _{1-x} Al _x (C,N) _{1-y})												
		Hard coating layer												
Type	Tool body symbol	Formation symbol of TiAlCN deposition process	Al content x _{avg}	ratio	C content y _{avg}	ratio	Area ratio of crystal grains having the average crystal grain misorientation of 2° or more (%)	Area ratio of the average crystal grain width W of aspect ratio of	Frequency distribution ratio of inclined angle of the normal line of the {100} plane in the range of 0° to 12° in the	Frequency distribution ratio of inclined angle of the normal line of the {100} plane in the range of 0° to 12° in the	Inclined angle section showing the highest peak in the surface side	Intended thickness (μm)	Upper layer (Numbers at the bottom indicate the average intended layer thickness (μm) of the layer)	
			x _{avg}	ratio	y _{avg}	ratio	of 2° or more (%)	Average grain width W of aspect ratio of	interface side region M _{deg}	surface side region N _{deg}	region (°)	thickness (μm)	1st layer	2nd layer
	11 C	A'	0.93	less than 0.0001		6	95	1.0	26	22	25.25-25.50	4	TiCN (0.5)	Al ₂ O ₃ (3)
	12 D	B'	0.78	less than 0.0001		4	89	0.5	27	31	13.75-14.00	3	TiCO (1)	Al ₂ O ₃ (2)
	13 A	C'	0.72	less than 0.0001		1	93	0.7	21	26	33.75-34.00	2.5	TiCNO (0.3)	Al ₂ O ₃ (1)
Reference coated tool	14 B	AIP	0.50	less than 0.0001		2	100	1.5	25	31	31.25-31.50	6	—	—
	15 C	AIP	0.59	less than 0.0001		3	100	0.6	19	24	32.25-32.50	3	—	—

AIP indicates deposition by using the arc ion plating.

[0089] Next, each of the coated tools described above was clamped on the face milling cutter made of tool steel with the cutter diameter of 125 mm by a fixing jig. Then, the center cut cutting test of high speed dry face milling was performed on the coated tools of the present invention **1-13**; the coated tools **1-8** and **11-15** of Comparative Example; and the reference coated tools **14** and **15**, in the clamped-state. The center cut cutting test of high speed dry face milling is a type of high speed intermittent cutting of alloy steel, and was performed under the condition shown below. After the test, width of flank wear of the cutting edge was measured. Results are shown in Table 9.

[0090] Tool body: Tungsten carbide-based cemented carbide; Titanium carbonitride-based cermet

[0091] Cutting test: High speed dry face milling; Center cut cutting test

[0092] Workpiece: Block material of JIS-SCM440 standard having width of 100 mm and length of 400 mm

[0093] Rotation speed: 955 min^{-1}

[0094] Cutting speed: 375 m/min

[0095] Cutting depth: 1.2 mm

[0096] Feed rate per tooth: 0.15 mm/tooth

[0097] Cutting time: 8 minutes

TABLE 9

Type	Width of flank wear (mm)	Type	Cutting test result (minute)
Coated tool of the present invention	1 0.10	Coated tool of Comparative Example	1 4.2*
	2 0.14		2 2.3*
	3 0.09		3 3.6*
	4 0.09		4 4.3*
	5 0.13		5 4.8*
	6 0.11		6 3.7*
	7 0.11		7 4.4*
	8 0.08		8 2.3*
	9 0.12		9 3.4*
	10 0.09		10 2.2*
	11 0.10		11 4.6*
	12 0.07		12 2.3*
	13 0.14		13 4.0*
14 0.08	Reference coated tool	14 1.7*	
15 0.07	15 1.9*		

Asterisk marks (*) in the column of coated tools of Comparative Example and reference coated tools indicate cutting time (min) until they reached to their service lives due to occurrence of chipping.

Example 2

[0098] First, as raw material powders, the WC powder, the TiC powder, the ZrC powder, the TaC powder, the NbC powder, the Cr_3C_2 powder, the TiN powder, and the Co powder, all of which had the average grain sizes of 1-3 μm , were prepared. Then, these raw material powders were blended in the blending composition shown in Table 10. Then, wax was added to the blended mixture, and further mixed in acetone for 24 hours with a ball mill. After drying under reduced pressure, the mixtures were press-molded into green compacts with a predetermined shape under pressure of 98 MPa. Then, the obtained green compacts were sintered in vacuum in the condition of 5 Pa vacuum at the predetermined temperature in the range of 1370-1470° C. for 1 hour retention. After sintering, by performing honing work of R: 0.07 mm on their cutting edge parts, the tool

bodies α - γ , which had the insert-shape defined by ISO-CNMG120412 and made of WC-based cemented carbide, were produced.

[0099] In addition, as raw material powders, the TiCN powder (TiC/TiN=50/50 in mass ratio), the NbC powder, the WC powder, the Co powder, and the Ni powders, all of which had the average grain sizes of 0.5-2 μm , were prepared. These raw material powders were blended in the blending composition shown in Table 11. Then, with a ball mill, the obtained mixtures were subjected to wet-mixing for 24 hours. After drying, the mixtures were press-molded into green compacts under pressure of 98 MPa. The obtained green compacts were sintered in the condition of: in nitrogen atmosphere of 1.3 kPa; at a temperature of 1500° C.; and for 1 hour of the retention time. After sintering, by performing honing work of R: 0.07 mm on their cutting edge parts, the tool body δ , which had the insert-shape defined by ISO-CNMG120412 and made of TiCN-based cermet, was produced.

[0100] Next, the coated tools of the present invention **16-30** shown in Table 13 were produced by depositing the hard coating layers including at least the $(\text{Ti}_{1-x}\text{Al}_x)(\text{C}_y\text{N}_{1-y})$ layer in the intended layer thicknesses on the surfaces of the tool bodies α - γ and the tool body δ in the conditions shown in Tables 3 and 4 with a chemical vapor deposition apparatus in the same manner as Example 1.

[0101] In regard to the cutting tools **34** to **38** of the present invention, the lower layer and/or the upper layer shown in Table 17 and/or Table 18, respectively, were formed in the conditions shown in Table 3.

[0102] In regard to the coated tools **19** to **28** of the present invention, the lower layer shown in Table 12 and/or the upper layer shown in Table 13 were formed in the forming conditions shown in Table 3.

[0103] In addition, for a comparison purpose, the coated tools **16** to **28** shown in Table 14 of Comparative Example were produced by depositing the hard coating layers on the surfaces of the tool bodies α - γ and the tool body δ with a standard chemical vapor deposition apparatus, in the conditions shown in Tables 3-4 and in the intended layer thicknesses shown in Table 14 in the same manner as the coated tools of the present invention.

[0104] In regard to coated tools **19-28** of Comparative Example, the lower layer shown in Table 12 and/or the upper layer shown in Table 14 were formed in the forming condition shown in Table 3, as in the coated tools **19** to **28** of the present invention.

[0105] For purpose of reference, the reference coated tools **29** and **30** shown in Table 14 were produced by depositing the $(\text{Ti}_{1-x}\text{Al}_x)(\text{C}_y\text{N}_{1-y})$ layers of the reference examples on the surfaces of the tool bodies β and γ in the intended layer thicknesses with a standard physical vapor deposition by arc-ion plating.

[0106] The conditions for the arc-ion plating used for deposition in the reference example were as in Example 1.

[0107] The cross sections of each constituent layer of: the coated tools of the present invention **16** to **30**; cutting tools **16-28** of Comparative Example; and the reference coated tools **29** and **30**, were measured by using a scanning electron microscope (magnifying power: $\times 5000$). The average layer thicknesses were obtained by averaging layer thicknesses

measured at 5 points within the observation viewing field. In any measurement, the obtained average layer thickness was practically the same as the intended layer thicknesses shown in Tables 13 and 14.

[0108] Then, crystal orientation of each of crystal grains having the cubic structure constituting the Ti and Al complex nitride or complex carbonitride layer, was analyzed along the vertical cross-sectional direction with an electron beam backward scattering diffraction device. Mapping was performed by classing the obtained average crystal grain misorientation in every 1° in the range from 0° to 10°, such as: more than 0° to less than 1°; more than 1° to less than 2°; more than 2° to less than 3°; more than 3° to less than 4°; and the like. Based on the mapping diagram, the area ratio of the crystal grains having the average crystal grain misorientation of 2° or more occupying the entire Ti and Al complex nitride or complex carbonitride layer was obtained. The results are shown in Tables 13 and 14.

[0109] In regard to the frequency distribution graph of the inclined angles in the hard coating layer, the frequencies in the range of 0° to 12° were obtained as follows. First, the cross sections of the hard coating layer made of the Ti and Al complex nitride or complex carbonitride layer in the cubic structure were set in the lens barrel of a field-emission-type scanning electron microscope in the state where the cross sections were polished. Then, analysis was performed on the polished surfaces dividing the analysis field in two regions, which were the region on the tool body side (interface side) and the region on the surface side, in the thickness direction. Electron beam was irradiated on each of crystal grains having the cubic lattice in the measurement field with the incident angle of 70°, the acceleration voltage of 10 kV, and the irradiation current of 1 nA in the interval of 0.1 μm/step, on five viewing fields covering: the interface side region and the surface side region in the measurement range in the direction perpendicular to the surface of the tool body; and the width of 10 μm in the direction parallel to the surface of the tool body. Then, by using an electron beam backward scattering diffraction device, the inclined angles of the normal line of the {100} plane, which was a crystal plane of the crystal grain, relative to the normal line of the surface of the tool body (the direction perpendicular to the surface of the tool body in the polished cross-sectional surface) were measured. Then, based on the measured results, the inclined angles in the range of 0 to 45° among the measured inclined angles were divided into sections in every 0.25° pitch; and the frequency in each section was tallied to draw the frequency distribution graph. The results are shown in Tables 13 and 14.

TABLE 10

		Blending composition (mass %)							
Type		Co	TiC	ZrC	TaC	NbC	Cr ₃ C ₂	TiN	WC
Tool	α	6.5	—	1.5	—	2.9	0.1	1.5	balance
body	β	7.6	2.6	—	4.0	0.5	—	1.1	balance
	γ	6.0	—	—	—	—	—	—	balance

TABLE 11

		Blending composition (mass %)				
Type		Co	Ni	NbC	WC	TiCN
Tool body	δ	11	4	6	15	balance

TABLE 12

		Hard coating layer (the number at the bottom indicates the intended average layer thickness (μm) of the layer)				
		Tool	Lower layer			
Type		body symbol	1st layer	2nd layer	3rd layer	4th layer
Coated tool of the present invention,	16	α	—	—	—	—
	17	β	—	—	—	—
coated tool of Comparative Example, and reference coated tool	18	γ	—	—	—	—
	19	δ	TiC (0.5)	—	—	—
	20	α	TiN-1 (0.1)	—	—	—
	21	β	TiN-1 (0.5)	1-TiCN-1 (7)	—	—
	22	γ	TiN-1 (0.3)	1-TiCN-1 (10)	TiN-2 (0.7)	—
	23	δ	TiN-1 (0.3)	1-TiCN-1 (4)	TiCN (0.4)	TiN-2 (0.3)
	24	α	—	—	—	—
	25	β	TiN-1 (0.5)	—	—	—
	26	γ	TiC (1)	—	—	—
	27	δ	TiN-1 (0.1)	—	—	—
	28	α	TiN-1 (0.1)	—	—	—
	29	β	—	—	—	—
	30	γ	—	—	—	—

TABLE 13

		Hard coating layer														
		Ti and Al complex nitride, carbonitride layer (Ti _{1-x} Al _x C _z N _{1-z})														
Type	Tool body symbol	Formation symbol of TiAlCN deposition process	Al content x _{avg}	C content y _{avg}	Area ratio of crystal grains having the average crystal grain misorientation of 2° or more (%)	Area ratio of the crystals (%)	Average grain width W of crystal grains (μm)	Average aspect ratio of crystal grains	Frequency distribution ratio of inclined angle of the normal line of the {100} plane in the range of 0° to 12° in the interface side region M _{avg}	Frequency distribution ratio of inclined angle of the normal line of the {100} plane in the range of 0° to 12° in the surface side region N _{avg}	Inclined angle section showing the highest peak in the surface side region (°)	Intended layer thickness (μm)	1st layer thickness (μm)	2nd layer thickness (μm)	3rd layer thickness (μm)	4th layer thickness (μm)
Coated tool of the present invention	16 α	A	0.94	less than 0.0001	45	100	0.2	2.5	21	40	3.00-3.25	6	—	—	—	—
	17 β	B	0.77	less than 0.0001	32	100	1.1	2.0	29	59	4.75-5.00	4	—	—	—	—
	18 γ	C	0.74	0.0031	22	100	0.4	5.1	37	52	6.00-6.25	7	—	—	—	—
	19 δ	D	0.71	less than 0.0001	56	90	0.8	5.0	15	30	5.25-5.50	12	—	—	—	—
	20 α	E	0.94	less than 0.0001	45	75	0.6	2.0	26	47	4.50-5.75	16	—	—	—	—
	21 β	F	0.66	0.0023	33	100	1.1	3.1	17	29	4.50-4.75	8	—	—	—	—
	22 γ	G	0.88	less than 0.0001	48	98	0.5	2.2	34	53	4.25-4.50	20	TiN-2 (0.7)	—	—	—
	23 δ	H	0.92	less than 0.0001	39	68	0.8	2.2	16	39	10.00-10.25	15	TiCN (0.4)	TiN-2 (0.3)	—	—
	24 α	I	0.63	0.0038	55	95	0.7	2.1	29	58	2.75-3.00	3	Al ₂ O ₃ (2)	—	—	—
	25 β	J	0.69	less than 0.0001	39	93	0.9	3.2	24	44	2.50-2.75	7	TiCN (0.5)	Al ₂ O ₃ (2.5)	—	—

(Numbers at the bottom indicate the average intended layer thickness (μm) of the layer)

TABLE 13-continued

		Ti and Al complex nitride, carbonitride layer (Ti _{1-x} Al _x)C _{1-y} N _{1-y}													
		Hard coating layer													
Type	Tool body symbol	Formation symbol of TiAlCN deposition process	Al content x _{avg}	C content y _{avg}	Area ratio of crystal grains having the average crystal grain misorientation of 2° or more (%)	Area ratio of the average grain width W of cubic crystals (%)	Average aspect ratio of crystal grains (μm)	Frequency distribution ratio of inclined angle of the normal line of the {100} plane in the range of 0° to 12° in the interface side region M _{avg}	Frequency distribution ratio of inclined angle of the normal line of the {100} plane in the range of 0° to 12° in the surface side region N _{avg}	Inclined angle showing the highest peak in the surface region (°)	Intended layer thickness (μm)	1st layer	2nd layer	3rd layer	4th layer
26	γ	A	0.94	less than 0.0001	46	96	1.1	1.5	32	54	4	TiCO (1)	Al ₂ O ₃ (2)	—	—
27	δ	B	0.78	less than 0.0001	24	93	0.4	10.0	10	38	11	TiCNO (0.3)	Al ₂ O ₃ (1)	—	—
28	α	C	0.68	0.0025	21	97	0.1	2.3	38	48	5	TiN-2 (0.3)	TiCN (0.8)	TiCNO (0.3)	Al ₂ O ₃ (3)
29	β	D	0.65	less than 0.0001	61	92	0.3	2.3	27	45	16	—	—	—	—
30	γ	E	0.91	less than 0.0001	44	83	0.10	3.1	40	61	9	—	—	—	—

TABLE 14

		Hard coating layer														
		Ti and Al complex nitride, carbonitride layer (Ti _{1-x} Al _x C _z N _{1-x-z})														
Type	Coated tool of Comparative Example	Tool body symbol	Formation symbol of TiAlCN deposition process	Al content x _{avg}	Area ratio of crystal grains having the average crystal grain misorientation of 2° or more (%)	Area ratio of the cubic crystals (%)	Average grain width (μm)	Average aspect ratio of crystal grains	Frequency distribution ratio of inclined angle of the normal line of the {100} plane in the range of 0° to 12°	Frequency distribution ratio of inclined angle of the normal line of the {100} plane in the range of 0° to 12°	Inclined angle section showing the highest peak in the surface side region (°)	Intended layer thickness (μm)	1st layer thickness (μm)	2nd layer thickness (μm)	3rd layer thickness (μm)	4th layer thickness (μm)
	16 α	A'		0.93	6	100	0.9	2.5	34	43	14.50-14.75	6	—	—	—	—
	17 β	B'		0.82	6	100	0.7	5.0	25	31	32.00-32.25	4	—	—	—	—
	18 γ	C'		0.72	1	100	1.0	1.6	26	22	15.25-15.50	7	—	—	—	—
	19 δ	D'		0.66	5	100	0.5	1.5	31	34	33.75-34.00	12	—	—	—	—
	20 α	E'		0.91	3	75	0.8	1.5	19	23	28.25-28.50	16	—	—	—	—
	21 β	F'		0.65	5	100	1.0	1.8	21	24	34.25-34.50	8	—	—	—	—
	22 γ	G'		0.85	5	95	0.4	1.5	22	17	41.50-41.75	20	TiN-2 (0.7)	—	—	—
	23 δ	H'		0.92	4	66	0.2	1.2	34	28	36.25-36.50	15	TiCN (0.4)	TiN-2 (0.3)	—	—
	24 α	I'		0.64	10	94	0.4	2.1	24	19	26.75-27.00	3	Al ₂ O ₃ (2)	—	—	—
	25 β	J'		0.70	4	96	0.4	0.8	15	18	33.25-33.50	7	TiCN (0.5)	Al ₂ O ₃ (2.5)	—	—

TABLE 14-continued

		Ti and Al complex nitride, carbonitride layer (Ti _{1-x} Al _x C _z N _{1-y-z})														
		Hard coating layer														
Type	Tool body symbol	Formation symbol of TiAlCN deposition process	Al content ratio X _{avg}	C content ratio Y _{avg}	Area ratio of crystal grains having the average crystal grain misorientation of 2° or more (%)	Area ratio of the cubic crystals (%)	Average grain width W of crystal grains (μm)	Average aspect ratio of crystal grains	Frequency distribution ratio of inclined angle of the normal line of the {100} plane in the range of 0° to 12° in the interface side region M _{deg}	Frequency distribution ratio of inclined angle of the normal line of the {100} plane in the range of 0° to 12° in the surface side region N _{deg}	Inclined angle section showing the highest peak in the surface side region (°)	Upper layer				
												Intended layer thickness (μm)	1st layer	2nd layer	3rd layer	4th layer
26 γ	A'		0.92	less than 0.0001	5	98	0.2	3.1	27	22	32.75-33.00	4	TiCO (1)	Al ₂ O ₃ (2)	—	—
27 δ	B'		0.77	less than 0.0001	4	90	0.7	1.2	21	26	33.75-34.00	11	TiCNO (0.3)	Al ₂ O ₃ (1)	—	—
28 α	C'		0.69	0.0019	1	94	0.08	0.5	33	37	34.25-34.50	5	TiN+2 (0.3)	TiCN (0.8)	TiCNO (0.3)	Al ₂ O ₃ (3)
29 β	AIP		0.49	less than 0.0001	2	100	1.5	3.3	25	31	31.25-31.50	5	—	—	—	—
30 γ	AIP		0.60	less than 0.0001	3	100	0.6	2.2	19	24	32.25-32.50	3	—	—	—	—

AIP indicates deposition by using the arc ion plating.

[0110] Next, each coated tool described above was screwed on the tip of the insert holder made of tool steel by a fixing jig. Then, the dry high speed intermittent cutting test of carbon steel and the wet high speed intermittent cutting test of cast iron explained below were performed on the coated tools of the present invention 16-30; the coated tools 16-28 of Comparative Example; and the reference coated tools 29 and 30. After the tests, width of flank wear of the cutting edge was measured in each test.

[0111] Cutting condition 1:

[0112] Workpiece: Round bar in JIS-545C standard with 4 evenly spaced slits in the longitudinal direction

[0113] Cutting speed: 370 m/min.

[0114] Cutting depth: 1.5 mm

[0115] Feed rate: 0.1 mm/rev.

[0116] Cutting time: 5 minutes

[0117] (the normal cutting speed is 220 m/min)

[0118] Cutting condition 2:

[0119] Workpiece: Round bar in JIS-FCD700 standard with 4 evenly spaced slits in the longitudinal direction

[0120] Cutting speed: 320 m/min.

[0121] Cutting depth: 1.2 mm

[0122] Feed rate: 0.2 mm/rev.

[0123] Cutting time: 5 minutes

[0124] (the normal cutting speed is 200 m/min)

[0125] Results of the cutting test are shown in Table 15.

bodies for the cutting edge pieces. The obtained preliminary sintered bodies were placed on separately prepared supporting pieces made of WC-based cemented carbide, which had the composition of: 8 mass % of Co; and the WC balance, and the dimension of: 50 mm of the diameter; and 2 mm of the thickness. They were inserted into a standard ultra-high pressure sintering apparatus in the stacked state. Then, they were subjected to ultra-high-pressure sintering in the standard condition of: 4 GPa of pressure; a predetermined temperature within the range of 1200–1400° C.; and 0.8 hour of the retention time. Then, the top and bottom surfaces of the sintered bodies were grinded by using a diamond grind tool. Then, they were divided into a predetermined dimension with a wire-electrical discharge machine. Then, they were brazed on the brazing portion (corner portion) of the insert body made of WC-based cemented carbide, which had the composition of: 5 mass % of Co; 5 mass % of TaC; and the WC balance, and the shape defined by ISO CNGA120408 standard (the 80° diamond shape of: thickness of 4.76 mm; and inscribed circle diameter of 12.7 mm) by using the brazing material made of Ti—Zr—Cu alloy having composition made of: 37.5% of Zr; 25% of Cu; and the Ti balance in volume %. Then, after performing outer peripheral machining into a predetermined dimension, the cutting edges of the brazed parts were subjected to a honing work of: 0.13 mm of the width; and 25° of the angle. Then,

TABLE 15

Type	Width of flank wear (mm)		Type	Cutting test result (minute)	
	Cutting condition 1	Cutting condition 2		Cutting condition 1	Cutting condition 2
Coated tool of the present invention	16	0.20	Coated tool of Comparative Example	16	3.1*
	17	0.19		17	4.7*
	18	0.20		18	4.8*
	19	0.21		19	4.3*
	20	0.23		20	4.3*
	21	0.19		21	3.8*
	22	0.19		22	3.4*
	23	0.22		23	3.6*
	24	0.10		24	2.2*
	25	0.22		25	4.3*
Reference coated tool	26	0.21	26	4.3*	
	27	0.19	27	2.9*	
	28	0.19	28	4.8*	
	29	0.22	29	2.2*	
	30	0.13	30	2.3*	

Asterisk marks (*) in the column of coated tools of Comparative Example and reference coated tools indicate cutting time (min) until they reached to their service lives due to occurrence of chipping.

Example 3

[0126] First, as raw material powders, the cBN powder, the TiN powder, the TiC powder, the Al powder, and the Al₂O₃ powder, all of which had the average grain sizes of 0.5-4 μm, were prepared. Then, these raw material powders were blended in the blending composition shown in Table 16. Then, the blended mixtures were wet-mixed for 80 hours with a ball mill. After drying, the mixtures were press-molded into green compacts having the dimension of: 50 mm of the diameter and 1.5 mm of the thickness under pressure of 120 MPa. Then, the obtained green compacts were sintered in vacuum in the condition of 1 Pa vacuum at the predetermined temperature in the range of 900–1300° C. for 60 minutes retention to obtain preliminary sintered

by performing the final polishing on them, the tool bodies 2A and 2B with the insert shape defined by ISO CNGA120408 standard were produced.

TABLE 16

Type	Blending composition (mass %)					
	TiN	TiC	Al	Al ₂ O ₃	cBN	
Tool body	2A	50	—	5	3	balance
	2B	—	50	4	3	balance

[0127] Next, the coated tools of the present invention 31-40 shown in Table 18 were produced by depositing the hard coating layers including at least the (Ti_{1-x}Al_x)(C_yN_{1-y})

layer in the intended layer thicknesses on the surfaces of the tool bodies **2A** and **2B** in the conditions shown in Tables 3 and 4 with a chemical vapor deposition apparatus in the same manner as Example 1.

[0128] In regard to the coated tools **34** to **38** of the present invention, the lower layer shown in Table 17 and/or the upper layer shown in Table 18 were formed in the forming conditions shown in Table 3.

[0129] In addition, for a comparison purpose, the coated tools **31** to **38** shown in Table 19 of Comparative Example were produced by depositing the hard coating layers including at least the $(\text{Ti}_{1-x}\text{Al}_x)(\text{C}_y\text{N}_{1-y})$ layer on the surfaces of the tool bodies **2A** and **2B** with a standard chemical vapor deposition apparatus, in the conditions shown in Tables 3-4 and in the intended layer thicknesses.

[0130] In regard to coated tools **34-38** of Comparative Example, the lower layer shown in Table 17 and/or the upper layer shown in Table 18 were formed in the forming condition shown in Table 3, as in the coated tools **34** to **38** of the present invention.

[0131] For purpose of reference, the reference coated tools **39** and **40** shown in Table 19 were produced by depositing the $(\text{Ti}_{1-x}\text{Al}_x)(\text{C}_y\text{N}_{1-y})$ layers of the reference examples on the surfaces of the cutting tool bodies **2A** and **2B** in the intended layer thicknesses with a standard physical vapor deposition by arc-ion plating.

[0132] The reference coated tools **39** and **40** were produced by depositing the (Al, Ti)N layer on the surfaces of the above-described tool bodies in the intended composition and the intended layer thicknesses with shown in Table 19 in the conditions for the arc-ion plating used for deposition in the reference example as in Example 1.

[0133] The cross sections of each constituent layer of: the coated tools of the present invention **31** to **40**; cutting tools **31** to **38** of Comparative Example; and the reference coated tools **39** and **40**, were measured by using a scanning electron microscope (magnifying power: $\times 5000$). The average layer thicknesses were obtained by averaging layer thicknesses measured at 5 points within the observation viewing field. In any measurement, the obtained average layer thickness was practically the same as the intended layer thicknesses shown in Tables 18 and 19.

[0134] On the coated tools **31** to **40** of the present invention; the coated tools **31** to **38** of Comparative Example; and the reference coated tools **39** and **40**, the average Al content ratio x_{avg} , the average C content ratio y_{avg} , the area ratio of the crystal grains having the average crystal grain misorientation of 2° or more in the crystal grains having the cubic structure constituting the $(\text{Ti}_{1-x}\text{Al}_x)(\text{C}_y\text{N}_{1-y})$ layer, the average grain width W, and the average aspect ratio A were calculated by using the same method as shown in Example 1. Results are shown in Tables 18 and 19.

TABLE 17

Tool body	Hard coating layer (the number at the bottom indicates the intended average layer thickness (μm) of the layer)			
	Lower layer			
Type	symbol	1st layer	2nd layer	3rd layer
Coated tool of the present invention,	31 2A	—	—	—
	32 2B	—	—	—
coated tool of	33 2A	—	—	—
Comparative Example, and	34 2B	TiN-3 (0.5)	—	—
		TiN-3 (0.5)	—	—
reference coated tool	35 2A	TiN-3 (0.5)	—	—
	36 2B	TiN-3 (0.1)	—	—
	37 2A	TiN-3 (0.5)	1-TiCN-2 (3)	—
	38 2B	TiN-3 (0.3)	1-TiCN-2 (7)	TiN-3 (0.7)
	39 2A	—	—	—
	40 2B	—	—	—

TABLE 18

		Hard coating layer											
		Ti and Al complex nitride, carbonitride layer (Ti _{1-x} Al _x (C,N) _{1-y})											
Type	Tool body symbol	Formation symbol of TiAlCN process (refer Table 4)	Al content ratio x_{avg}	C content ratio y_{avg}	Area ratio of crystal grains having the average crystal grain misorientation of 2° or more (%)	Area ratio of the cubic crystals (%)	Average grain width W of crystal grains (μm)	Average aspect ratio of crystal grains	Frequency distribution ratio of the normal line of the {100} plane in the range of 0° to 12° in the interface side region M_{deg}	Frequency distribution ratio of inclined angle of the normal line of the {100} plane in the range of 0° to 12° in the surface side region N_{deg}	Inclined angle section showing the highest peak in the surface side region (°)	Intended layer thickness (μm)	Upper layer (Numbers at the bottom indicate the average intended layer thickness (μm) of the layer)
Coated tool of the present invention	31 2A	G	0.87	less than 0.0001	53	100	0.7	2.6	28	46	4.50-4.75	6	—
	32 2B	J	0.65	less than 0.0001	61	100	0.9	3.2	18	38	8.00-8.25	3	—
	33 2A	C	0.79	0.0022	42	100	1.2	2.4	31	59	3.75-4.00	5	—
	34 2B	G	0.85	less than 0.0001	48	100	0.4	2.2	29	48	4.25-4.50	2	—
	35 2A	J	0.64	less than 0.0001	60	98	1.4	2.5	21	39	6.00-6.25	4	TIN-3 (0.5)
	36 2B	C	0.75	0.0031	45	100	0.8	3.0	17	32	4.25-4.50	3	—
	37 2A	G	0.83	less than 0.0001	49	100	1.8	2.9	25	44	2.50-2.75	6	—
	38 2B	J	0.63	less than 0.0001	56	96	0.4	4.8	38	54	7.00-7.25	4	—
	39 2A	C	0.77	0.0047	48	100	1.1	5.2	26	56	2.75-3.00	7	—
	40 2B	J	0.61	less than 0.0001	59	99	0.8	3.7	16	31	9.25-9.50	3	—

TABLE 19

		Hard coating layer Ti and Al complex nitride, carbonitride layer (Ti _{1-x} Al _x)(C _y N _{1-y})										
Type	Tool body symbol	Formation symbol of TiAlCN deposition process (refer Table 4)	Al content ratio x _{avg}	C content ratio y _{avg}	Area ratio of crystal grains having the average crystal grain misorientation of 2° or more (%)	Area ratio of the cubic crystals (%)	Average grain width of crystal grains (μm)	Average aspect ratio of crystal grains	Frequency distribution ratio of inclined plane in the range of 0° to 12° in the interface side region M _{avg}	Frequency distribution ratio of inclined plane of the {100} in the range of 0° to 12° in the surface side region N _{avg}	Inclined angle section showing the highest peak in the surface side region (°)	Intended layer thickness (μm)
Coated tool of Comparative Example	31 2A	G'	0.85 less than 0.0001		3	100	0.8	1.5	19	23	28.25-28.50	6
	32 2B	J'	0.63 less than 0.0001		5	100	0.9	2.5	34	43	14.50-15.75	3
	33 2A	C'	0.76 0.0022		0	100	0.4	1.5	22	17	41.50-41.75	5
	34 2B	G'	0.83 less than 0.0001		4	100	0.7	2.5	25	31	32.00-32.25	2
	35 2A	J'	0.65 less than 0.0001		4	98	0.5	1.5	31	34	33.75-34.00	4
	36 2B	C'	0.73 0.0031		1	100	1.0	1.6	26	22	15.25-15.50	3
	37 2A	G'	0.81 less than 0.0001		4	100	0.2	1.2	34	28	36.25-36.50	6
	38 2B	J'	0.61 less than 0.0001		4	96	1.0	1.8	21	24	34.25-34.50	4
Reference coated tool	39 2A	AIP	0.50 less than 0.0001		2	100	1.5	3.3	25	31	31.25-31.50	7
	40 2B	AIP	0.60 less than 0.0001		2	100	0.6	2.2	19	24	32.25-32.50	3

"AIP" indicates deposition by using the arc ion plating.

[0135] Next, each coated tool described above was screwed on the tip of the insert holder made of tool steel by a fixing jig. Then, the dry high speed intermittent cutting test of carbolized steel explained below were performed on the coated tools of the present invention 31-40; the coated tools 31 to 38 of Comparative Example; and the reference coated tools 39 and 40. After the tests, width of flank wear of the cutting edge was measured in each test.

[0136] Tool body: Cubic boron nitride-based ultra-high pressure sintered material

[0137] Cutting test: Dry high-speed intermittent cutting test of carbolized steel

[0138] Workpiece: Round bar in JIS-SCr420 standard (hardness: HRC60) with 4 evenly spaced slits in the longitudinal direction

[0139] Cutting speed: 240 m/min.

[0140] Cutting depth: 0.12 mm

[0141] Feed rate: 0.12 mm/rev.

[0142] Cutting time: 4 minutes

[0143] Results are shown in Table 20.

TABLE 20

Type	Width of flank wear (mm)	Type	Cutting test result (minute)	
Coated tool of the present invention	31 0.09	Coated tool of Comparative Example	31 2.6*	
	32 0.11		32 1.9*	
	33 0.09		33 2.2*	
	34 0.11		34 2.2*	
	35 0.08		35 2.3*	
	36 0.12		36 1.9*	
	37 0.10		37 2.5*	
	38 0.08		38 2.1*	
	39 0.09		Reference coated tool	39 1.8*
	40 0.10			40 1.6*

Asterisk marks (*) in the column of coated tools of Comparative Example and reference coated tools indicate cutting time (min) until they reached to their service lives due to occurrence of chipping.

[0144] Based on results shown in Tables 9, 15, and 20, it was demonstrated that the coated tools of the present invention had improved toughness, while high wear resistance is maintained, because there were strains in crystal grains to improve hardness by having: a predetermined average crystal grain misorientation in the cubic crystal grains constituting the Al and Ti complex nitride or complex carbonitride layer of the hard coating layer; and having a predetermined frequency distribution of the inclined angle of the normal line of the {100} plane in the regions on the interface side and on the surface side of the crystal grains. Furthermore, the coated tools of the present invention had excellent chipping resistance and defect resistance even in the case where they were used in high-speed intermittent cutting work where intermittent and impact load is exerted on the cutting edge. As a result, the coated tools of the present invention exhibit excellent wear resistance for a long-term usage evidently.

[0145] On the contrary, in regard to the coated tools 1-13, 16-28, 31-38 of Comparative Example, and the reference coated tools 14, 15, 29, 30, 39, and 40, which did not have the predetermined average crystal grain misorientation in the cubic crystal grains constituting the Al and Ti complex nitride or complex carbonitride layer of the hard coating layer; or did not the predetermined frequency distribution of the inclined angle of the normal line of the {100} plane in the regions on the interface side and on the surface side of

the crystal grains, it was demonstrated that high heat was generated during cutting; and they reached to the end of service lives in a short time due to chipping, defect, or the like when they were used in high-speed intermittent cutting work where intermittent and impact high load is exerted on the cutting edge, evidently.

INDUSTRIAL APPLICABILITY

[0146] As described above, the coated tool of the present invention can be used not only in the high speed intermittent cutting work of alloy steel, but can be used as coated tool for various workpieces. Moreover, since it exhibits excellent chipping resistance and wear resistance for a long-term usage, it satisfies the demands for adapting to a cutting apparatus with a higher performance; power-saving and energy-saving in cutting work; and cost-saving, sufficiently.

REFERENCE SIGNS LIST

[0147] P: Measurement point (Pixel)

[0148] B: Grain boundary

[0149] 1: Tool body

[0150] 2: Hard coating layer

[0151] 3: Complex nitride or complex carbonitride layer

1. A surface-coated cutting tool comprising: a tool body made of tungsten carbide-based cemented carbide, titanium carbonitride-based cermet, or cubic boron nitride-based ultra-high pressure sintered material; and a hard coating layer provided on a surface of the tool body, wherein

- the hard coating layer comprises at least a Ti and Al complex nitride or complex carbonitride layer, which is deposited by a chemical vapor deposition method and has an average layer thickness of 2 μm to 20 μm ; and an average content ratio x_{avg} , which is an average content ratio of Al with respect to a total amount of Ti and Al in the Ti and Al complex nitride or complex carbonitride layer in atomic ratio, and an average content ratio y_{avg} , which is an average content ratio of C with respect to a total amount of C and N in the Ti and Al complex nitride or complex carbonitride layer in atomic ratio, satisfy $0.60 \leq x_{avg} \leq 0.95$; and $0 \leq y_{avg} \leq 0.005$, respectively, in a case where a composition formula of the Ti and Al complex nitride or complex carbonitride layer is expressed by $(\text{Ti}_{1-x}\text{Al}_x)(\text{C}_y\text{N}_{1-y})$,
- the complex nitride or complex carbonitride layer comprises at least a phase of Ti and Al complex nitride or complex carbonitride having a NaCl face-centered cubic structure,
- an area ratio of crystal grains having an average crystal grain misorientation of 2° or more relative to the Ti and Al complex nitride or complex carbonitride layer is 20% or more, when crystal orientations of crystal grains having the NaCl face-centered cubic structure in crystal grains constituting the complex nitride or carbonitride layer are analyzed along a vertical cross-sectional direction with an electron beam backward scattering diffraction device and the average crystal grain misorientation of the individual crystal grains is obtained, and
- when inclined angles of normal lines of {100} plane as crystal plane of the crystal grains relative to a normal line of a surface of the cutting tool body are measured dividing the complex nitride or complex carbonitride

layer into two regions of an interface side region and a surface side region in a layer thickness direction; and frequencies in each of sections, in which measured inclined angles within a range of 0° to 45° relative to the normal line of the surface of the cutting tool among the measured inclined angles are divided in every 0.25° pitch, are tallied,

M_{deg} , which is the ratio of a sum of frequencies in a range of 0° to 12° in the interface side region to an overall frequency in an inclined angle distribution, is 10% to 40%, and

a highest peak is present in an inclined angles sections in a range of 0° to 12° , and in the surface side region and N_{deg} , which is the ratio of a sum of frequencies in a range of 0° to 12° in the surface side region to an overall frequency in an inclined angle distribution, is $M_{deg}+10\%$ to $M_{deg}+30\%$.

2. The surface-coated cutting tool according to claim 1, wherein an area ratio of the Ti and Al complex nitride or complex carbonitride having the NaCl face-centered cubic structure in the Ti and Al complex nitride or complex carbonitride layer expressed by the $(Ti_{1-x}Al_x)(C_yN_{1-y})$ is 70% or more.

3. The surface-coated cutting tool according to claim 1, wherein the complex nitride or complex carbonitride layer

has a columnar structure, in which an average grain width W and an average aspect ratio A of each of the crystal grains having the cubic structure in the complex nitride or complex carbonitride layer are $0.1 \mu\text{m}$ to $2 \mu\text{m}$ and 2 to 10, respectively, when the complex nitride or complex carbonitride layer is observed along a vertical cross-sectional direction.

4. The surface-coated cutting tool according to claim 1, wherein a lower layer of a Ti compound layer, which is made of one or more layers of: a Ti carbide layer; a Ti nitride layer; a Ti carbonitride layer; a Ti oxycarbide layer; and a Ti oxycarbonitride layer, is provided between the tool body and the Ti and Al complex nitride or complex carbonitride layer, an average total layer thickness of the lower layer being $0.1 \mu\text{m}$ to $20 \mu\text{m}$.

5. The surface-coated cutting tool according to claim 1, wherein an upper layer including at least an aluminum oxide layer is formed on the complex nitride or complex carbonitride layer, an average total layer thickness of the upper layer being $1 \mu\text{m}$ to $25 \mu\text{m}$.

6. The surface-coated cutting tool according to claim 1, wherein the complex nitride or complex carbonitride layer is deposited by a chemical vapor deposition method using at least trimethyl aluminum as a reaction gas component.

* * * * *