



US 20140305124A1

(19) **United States**
(12) **Patent Application Publication**
Kobayashi et al.

(10) **Pub. No.: US 2014/0305124 A1**
(43) **Pub. Date: Oct. 16, 2014**

(54) **SOLAR HEAT RECEIVER AND SOLAR HEAT POWER GENERATION DEVICE**

Publication Classification

(71) Applicant: **MITSUBISHI HEAVY INDUSTRIES, LTD.**, Minato-ku, Tokyo (JP)

(51) **Int. Cl.**
F03G 6/04 (2006.01)
F24J 2/24 (2006.01)

(72) Inventors: **Kazuta Kobayashi**, Tokyo (JP); **Masashi Tagawa**, Tokyo (JP); **Toshiyuki Osada**, Tokyo (JP); **Takeshi Okubo**, Tokyo (JP)

(52) **U.S. Cl.**
CPC .. **F03G 6/04** (2013.01); **F24J 2/245** (2013.01)
USPC **60/641.11**; **126/663**

(73) Assignee: **MITSUBISHI HEAVY INDUSTRIES, LTD.**, Minato-ku, Tokyo (JP)

(57) **ABSTRACT**

(21) Appl. No.: **14/353,169**

A solar heat receiver includes a casing having an aperture, and a piping system provided in the casing and discharging a heat medium, which is sent from a fluid supply source, to a fluid supply destination after the heat medium is heated by the solar light. The piping system includes: heat receiver tubes that heat the heat medium flowing therein; an inlet header tube that distributes the heat medium, which is introduced from the fluid supply source, to each of the heat receiver tubes, and an outlet header tube that collects the heat medium passing through each of the heat receiver tubes, and leads the heat medium to the fluid supply destination. The inlet header tube and the outlet header tube have a larger inner diameter than each of the heat receiver tubes.

(22) PCT Filed: **Nov. 22, 2012**

(86) PCT No.: **PCT/JP2012/080328**

§ 371 (c)(1),
(2), (4) Date: **Apr. 21, 2014**

(30) **Foreign Application Priority Data**

Nov. 25, 2011 (JP) 2011-257882

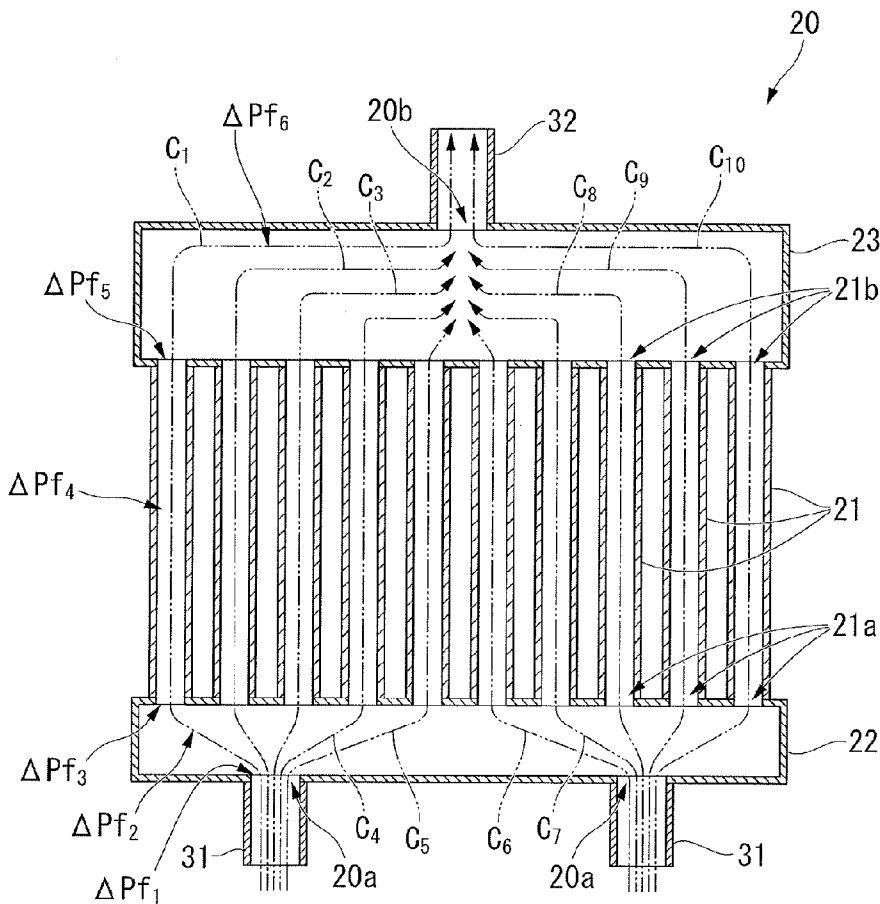


FIG. 1

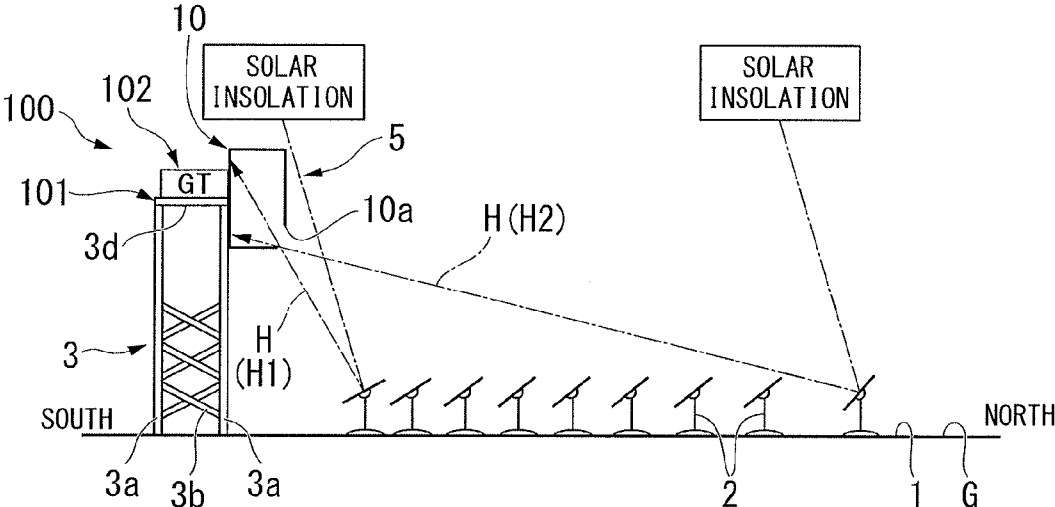


FIG. 2

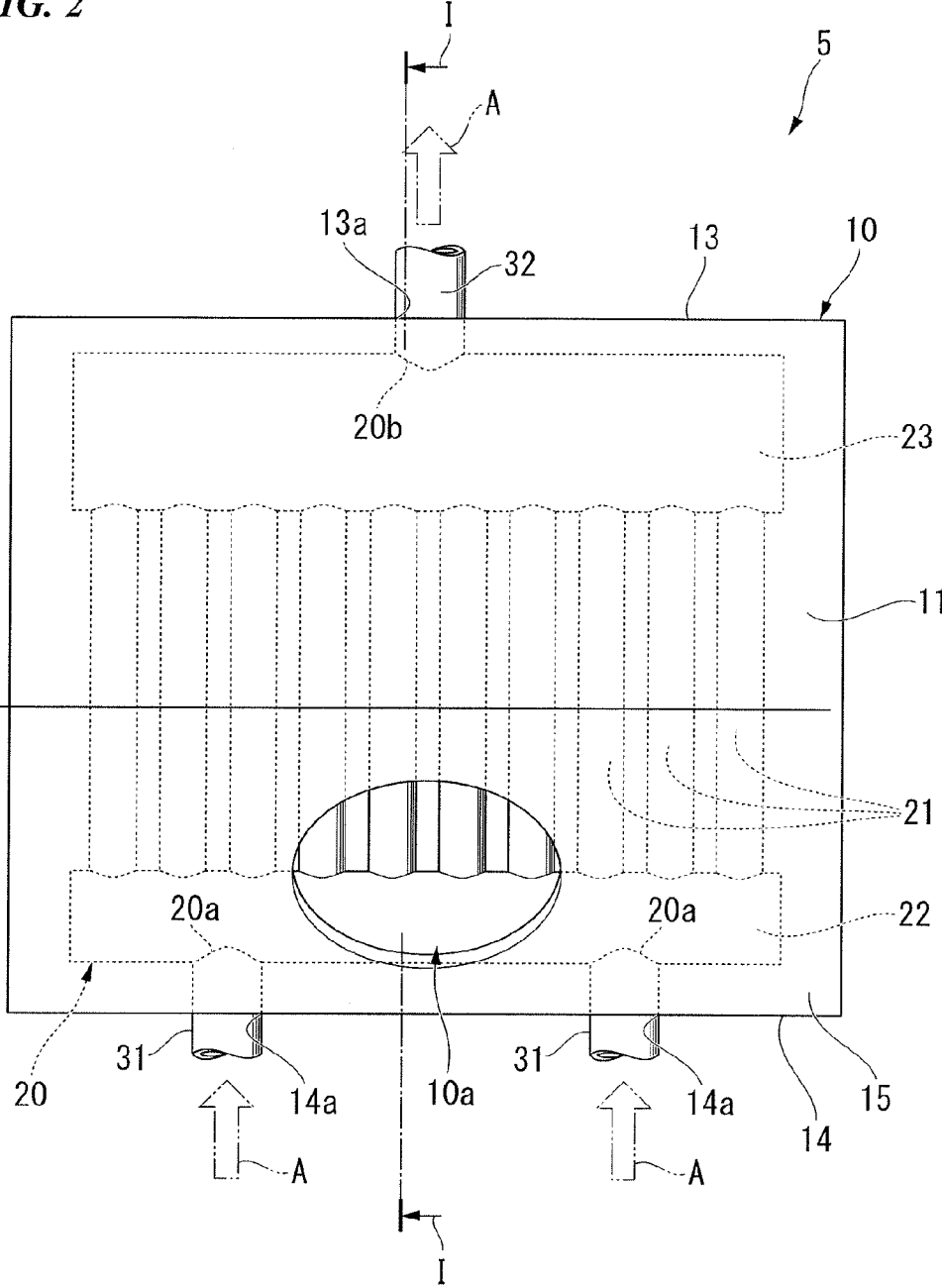


FIG. 3

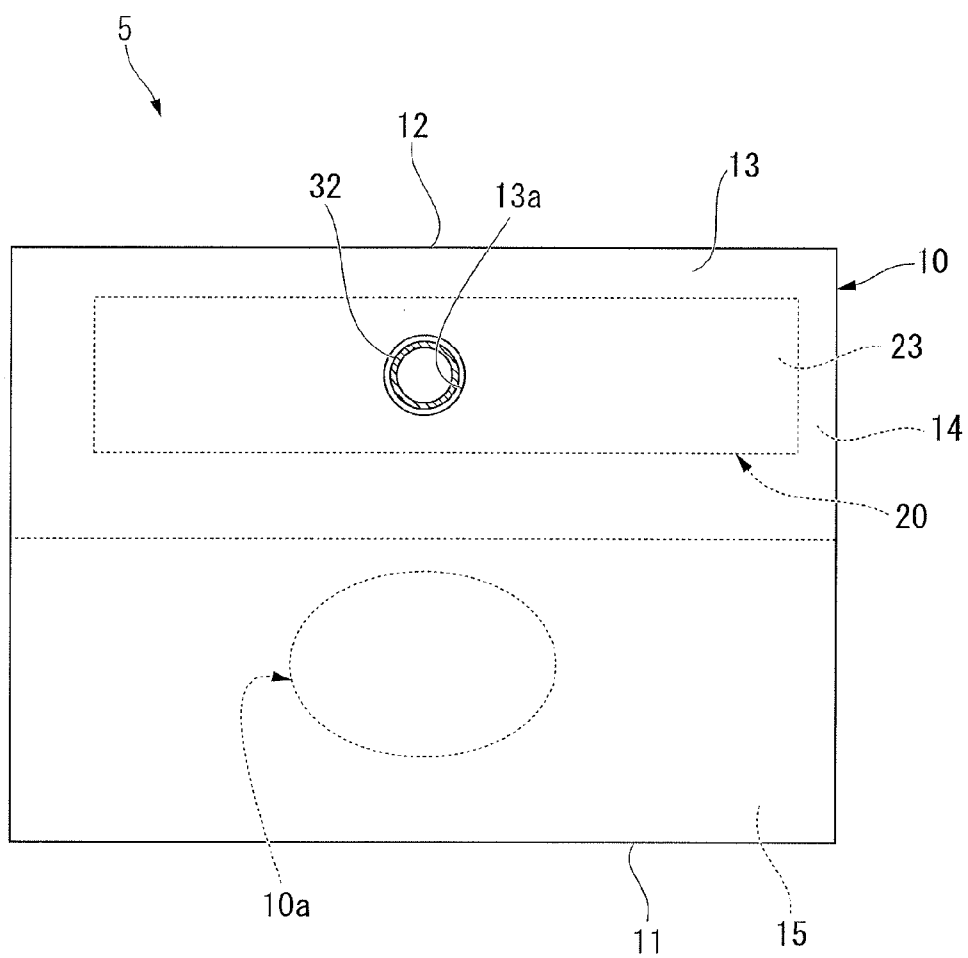


FIG. 4

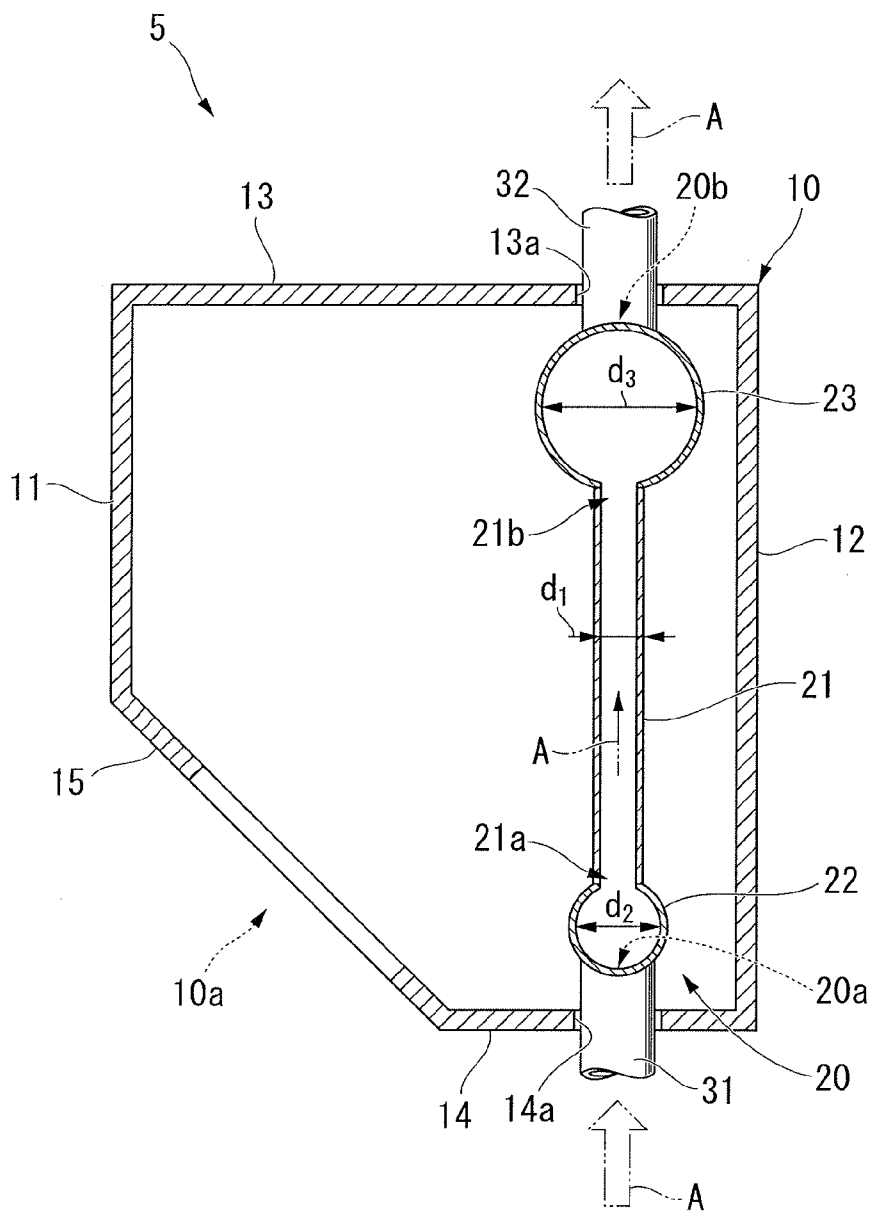
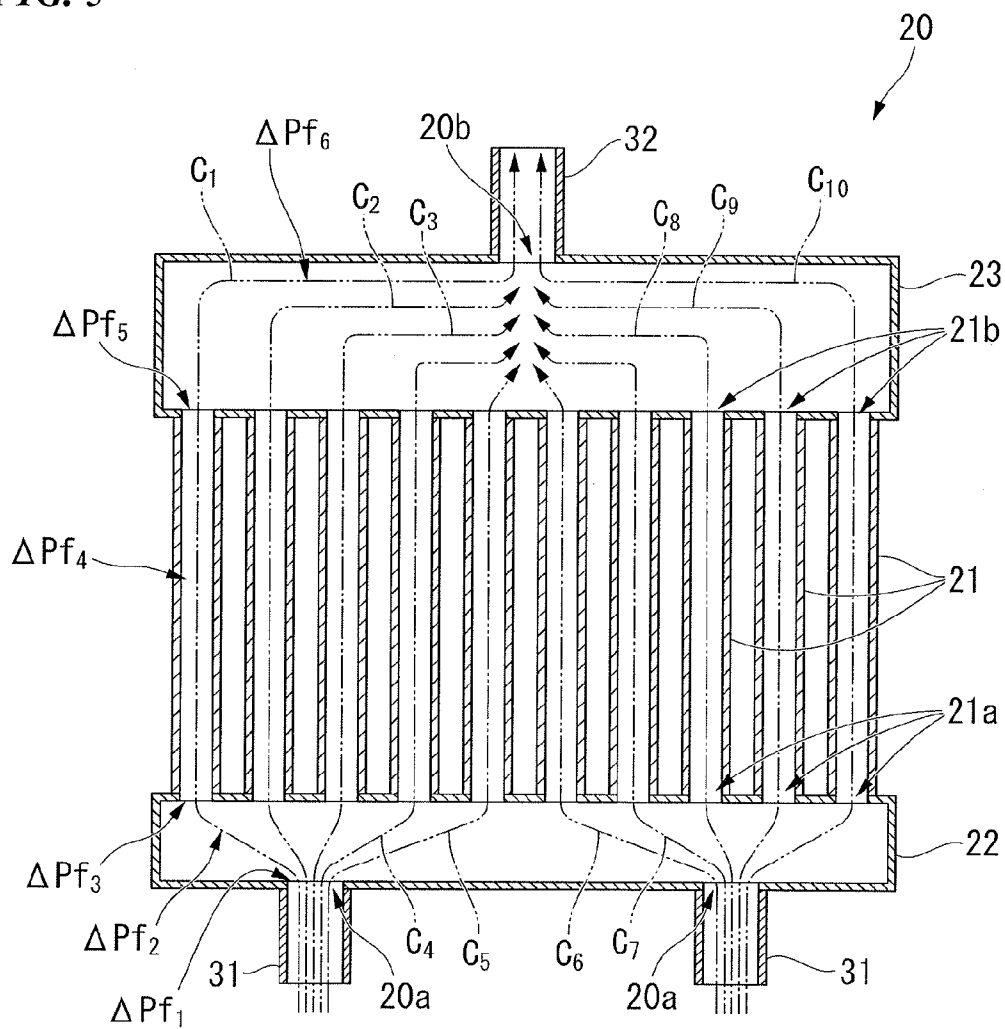


FIG. 5



SOLAR HEAT RECEIVER AND SOLAR HEAT POWER GENERATION DEVICE

TECHNICAL FIELD

[0001] The present invention relates to a solar heat receiver and a solar heat power generation device.

[0002] Priority is claimed on Japanese Patent Application No. 2011-257882, filed on Nov. 25, 2011, the content of which is incorporated herein by reference.

BACKGROUND ART

[0003] Recently devices using heat energy obtained by collecting solar light as clean energy that does not affect an environment have been introduced. As such devices, solar heat power generation devices performing power generation by converting the heat energy obtained by collecting the solar light into electric energy have been developed (e.g., see Patent Document 1).

[0004] In the solar heat power generation devices described above, light and heat are typically collected by a combination of a light collecting unit using a mirror and a solar heat receiver. Such a combination system of the light collecting unit and the heat receiver generally includes two types of systems called a trough light collecting system and a tower light collecting system.

[0005] The trough light collecting system refers to a system for causing solar light to be reflected by a semicylindrical mirror (trough), collecting the solar light and its heat on a tube passing through the center of the cylinder, and heating a heat medium flowing in the tube. However, in the trough light collecting system, since the mirror changes its direction to track the solar light under uniaxial control, it cannot expect the heat medium to be heated to a high temperature.

[0006] In contrast, the tower light collecting system refers to a system for disposing the solar heat receiver on a part of a tower erected from the ground, arranging a plurality of reflected light control mirrors, each of which is used for light collection and is called a heliostat, so as to surround the part of the tower, guiding the solar light reflected by the heliostats to the solar heat receiver, and thereby collecting the solar light and its heat. In recent years, from the viewpoint of achieving much higher efficiency of a power generation cycle, the solar heat power generation devices based on the tower light collecting system for allowing the heat medium heat-exchanged by the solar heat receiver to be heated to a higher temperature have been actively developed.

[0007] The solar heat receiver used in the tower light collecting system, as disclosed in, for instance, Patent Document 2, is equipped with a casing having an aperture through which solar light enters, and a piping system that is provided in the casing and discharges a heat medium, which is sent from an external fluid supply source, to an external fluid supply destination after the heat medium is heated by the solar light. The piping system includes: a plurality of heat receiver tubes that are housed in the casing and receive the solar light, which enters through the aperture of the casing, to heat the heat medium flowing inside the heat receiver tubes; an inlet header tube that is connected to one end side of each of the heat receiver tubes and distributes the heat medium, which is introduced from the fluid supply source, to each of the heat receiver tubes; and an outlet header tube that is connected to the other end side of each of the heat receiver tubes, collects

the heat medium passing through each of the heat receiver tubes, and leads the heat medium to the fluid supply destination.

PRIOR ART DOCUMENT

Patent Document

[0008] Patent Document 1: Japanese Unexamined Patent Application, First Publication No. H11-280638

[0009] Patent Document 2: United States Patent Application, Publication No. 2009/0241939

SUMMARY OF INVENTION

Problem to be Solved by the Invention

[0010] Incidentally, in the piping system, paths along which the heat medium flows from an inlet of the inlet header tube to an outlet of the outlet header tube are present in a number corresponding to the heat receiver tubes.

[0011] However, in the related art, since loss of energy of the heat medium differs in every path, a flow rate of the heat medium flowing through each path is not uniformly distributed. As a result, local variation in temperature may occur at some of the plurality of paths, or a difference in heating performance for the heat medium of each path may occur.

[0012] The present invention has been made in consideration of such circumstances, and an object of the present invention is to uniformize temperature distribution of a plurality of paths and heating performance for a heat medium of each path.

Means for Solving the Problem

[0013] To accomplish the above object, the present invention employs the following means.

[0014] In detail, a solar heat receiver according to the present invention includes a casing having an aperture configured to let solar light to enter, and a piping system installed in the casing and configured to discharge a heat medium, which is sent from a fluid supply source of an outside, to a fluid supply destination of the outside after the heat medium is heated by the solar light. The piping system includes: a plurality of heat receiver tubes housed in the casing and configured to receive the solar light entering through the aperture of the casing and to heat the heat medium flowing therein; an inlet header tube connected to one end side of each of the heat receiver tubes and configured to distribute the heat medium, which is introduced from the fluid supply source, to each of the heat receiver tubes; and an outlet header tube connected to the other end side of each of the heat receiver tubes and configured to collect the heat medium passing through each of the heat receiver tubes and to lead the collected heat medium to the fluid supply destination. The inlet header tube and the outlet header tube have a larger inner diameter than the heat receiver tubes.

[0015] With this constitution, energy loss of the heat medium in the inlet and outlet header tubes (hereinafter referred to as "header tubes") whose inner diameters are smaller than that in the heat receiver tubes. For this reason, a ratio of the energy loss in the header tubes to the sum of the energy loss on each path is relatively reduced, whereas a ratio of the energy loss in the heat receiver tubes to the sum of the energy loss on the paths is relatively increased.

[0016] In other words, since the energy loss is suppressed in the header tubes whose paths have different lengths, a difference in the sum of the energy loss on each path is also reduced. Thus, it is possible to reduce a difference in a flow rate of the heat medium flowing along each path, and uniformize flow rate distribution of each path. Accordingly, it is possible to uniformize temperature distribution of a plurality of paths and heating performance for the heat medium of each path.

[0017] Further, the outlet header tube may be set to have a larger inner diameter than the inlet header tube.

[0018] With this constitution, since the outlet header tube is set to have a larger inner diameter than the inlet header tube, a flow speed of the heat medium is inhibited from being increased in the outlet header tube through which the heat medium heated by the heat receiver tubes and whose volume flow rate is increased flows. Thereby, the energy loss proportional to the flow speed of the heat medium can also be suppressed. Accordingly, it is possible to further reduce the difference in the flow rate of the heat medium flowing along each path, and further uniformize the flow rate distribution.

[0019] Further, at least one of the inlet and outlet header tubes may include a plurality of flow ports, through which the heat medium is caused to flow and which are installed between the outside and the at least one of the inlet and outlet header tubes.

[0020] With this constitution, since at least one of the inlet and outlet header tubes is provided with a plurality of flow ports, an average distance from an aperture of each heat receiver tube to the flow port closest to the corresponding aperture of the heat receiver tube can be reduced. Thereby, it is possible to suppress the energy loss generated between the flow port and the aperture of the heat receiver tube, and reduce the difference in the flow rate of the heat medium flowing along each path. Thus, the flow rate distribution to each path can be uniformized.

[0021] The flow ports are preferably provided away from each other in a direction in which the heat receiver tubes are arranged.

[0022] Further, the heat medium may be air.

[0023] With this constitution, since the heat medium is air, it is possible to uniformly heat the air.

[0024] Further, a solar heat power generation device according to the present invention includes: the solar heat receiver set forth in any one of the above constitutions; a tower erected on a ground and configured to fixedly install the solar heat receiver at a high position; a plurality of heliostats disposed around the tower within a predetermined angular range and each configured to cause the solar light to enter through the aperture of the solar heat receiver; and a gas turbine unit including a compressor acting as the fluid supply source, a turbine acting as the fluid supply destination, and an electric generator configured to be driven rotatably by the turbine.

[0025] With this constitution, the solar heat power generation device includes the aforementioned solar heat receiver of the present invention. For this reason, temperature distribution of a plurality of paths and heating performance for the heat medium of each path are uniformized. As such, the solar heat power generation device can be configured as a system having high durability.

Advantageous Effects of Invention

[0026] In the solar heat receiver according to the present invention, temperature distribution of a plurality of paths and heating performance for the heat medium of each path can be uniformized.

[0027] Further, in the solar heat power generation device according to the present invention, temperature distribution of a plurality of paths and heating performance for the heat medium of each path are uniformized. As such, the solar heat power generation device can be configured as a system having excellent durability.

BRIEF DESCRIPTION OF DRAWINGS

[0028] FIG. 1 is a side view of a solar heat power generation device 100 according to an embodiment of the present invention.

[0029] FIG. 2 is a schematic front view of a solar heat receiver 5 according to an embodiment of the present invention.

[0030] FIG. 3 is a schematic top view of the solar heat receiver 5 according to the embodiment of the present invention.

[0031] FIG. 4 is a schematic side cross-sectional view of the solar heat receiver 5 according to the embodiment of the present invention, i.e. a cross-sectional view taken along line I-I of FIG. 2.

[0032] FIG. 5 is a cross-sectional view of a piping system 20 according to an embodiment of the present invention, and shows each of paths C (C₁, C₂, C₃ . . . C_n).

DESCRIPTION OF EMBODIMENTS

[0033] Hereinafter, an embodiment of the present invention will be described with reference to the accompanying drawings.

[0034] In the following description, a solar heat power generation device in which solar heat receiver of the present invention and a gas turbine unit generating electricity using a heat medium to which heat is applied by the solar heat receiver are integrally configured will be given as an example.

[0035] [Solar Heat Power Generation Device]

[0036] FIG. 1 is a side view of a solar heat power generation device 100 according to an embodiment of the present invention.

[0037] Here, a place suitable for the location of the solar heat power generation device on the Earth is an arid area of a subtropical high-pressure belt that is strong in insolation directly received from the sun and is quite close to the tropics. For example, the solar heat power generation device of the present embodiment employs a unilateral arrangement system in which it is disposed, particularly, on a high-latitude area within the subtropical high-pressure belt. Note that the present embodiment is not limited to the unilateral arrangement system.

[0038] In FIG. 1, a reference number 1 indicates a heliostat field that is installed on the ground G and is herein described as an area of the northern hemisphere. The solar heat power generation device 100 includes a light-collecting heat-receiving system 101 that collects solar light H (e.g., H1 and H2 of FIG. 1) radiated onto the heliostat field 1 and receives heat from the solar light H, and a gas turbine unit 102 that generates electricity using air A (a heat medium) to which the heat received by the light-collecting heat-receiving system 101 is applied.

[0039] Here, although not described in detail, the gas turbine unit **102** is mainly equipped with a compressor compressing the air A (working fluid) to which heat is applied by the light-collecting heat-receiving system **101**, a turbine supplied with the air A compressed by the compressor, a rotor connecting the compressor and the turbine on the same shaft, and an electric generator connected to the rotor. Thus, as the rotor is rotated by the air A supplied to the turbine, the air A is compressed by the compressor, and electricity can be generated by the electric generator.

[0040] The light-collecting heat-receiving system **101** is equipped with a plurality of heliostats **2** disposed on the heliostat field **1** in order to reflect the solar light H (H1 and H2), a tower **3** erected on the ground G, and a solar heat receiver **5** that is installed on an upper portion of the tower **3** and receives the solar light H. In the present embodiment, for example, the tower **3** is disposed on one end side (southern end in a north-south direction) of the heliostat field **1**. Further, the heliostats **2** are located on the other end side (north side) in the heliostat field **1**, and are arranged on a region of a predetermined angular range centering on the tower **3** within an approximate horizontal plane. In other words, the heliostat field **1** is set in a sector shape centering on the tower **3**. When the heliostat field **1** is located in an area of the southern hemisphere, an arrangement relation between the tower **3** and the heliostats **2** is opposite to that in the case of the aforementioned northern hemisphere.

[0041] The tower **3** includes a plurality of (e.g., four) supporting columns **3a** erected upward from the ground G, and beam sections **3b** connected to the supporting columns **3a** so as to be bridged between the supporting columns **3a**. Further, the upper portion of the tower **3** is provided with a frame **3d** supporting the solar heat receiver **5** described above.

[0042] [Solar Heat Receiver]

[0043] FIG. 2 is a schematic front view of the solar heat receiver **5**. FIG. 3 is a schematic top view of the solar heat receiver **5**. FIG. 4 is a schematic side cross-sectional view of the solar heat receiver **5** (i.e., a cross-sectional view taken along line I-I of FIG. 2). In the following description, an upstream side (north side in the present embodiment) in a radiating direction of the solar light H will be defined as a front side, and a downstream side (south side in the present embodiment) will be defined as a rear side.

[0044] As shown in FIGS. 2 to 4, the solar heat receiver **5** includes a casing **10** having an aperture **10a** through which the solar light H enters, and a piping system **20** that is set up in the casing **10** and discharges air A, which is sent from the compressor (fluid supply source) of the gas turbine unit **102**, to the turbine (fluid supply destination) of the gas turbine unit **102** after the air A is heated by the solar light H.

[0045] As shown in FIGS. 2 to 4, the casing **10** is formed in a box shape, and has a shape in which the lower half of a front portion thereof is inclinedly cut out. To be more specific, a front wall **11** is suspended from a top wall **13** by nearly half a length of a rear wall **12**, and a bottom wall **14** extends forward from the rear wall **12** by nearly half a length of the top wall **13**. A lower end edge of the front wall **11** and a front end edge of the bottom wall **14** are connected by an inclined wall **15**.

[0046] The inclined wall **15** is provided with an aperture **10a** that is open to the ground G. To be specific, the aperture **10a** is open so that an aperture direction thereof is obliquely directed toward a front lower side, and is configured so that the solar light H reflected by the heliostats **2** is introduced into the casing **10** through the aperture **10a**. A heat insulator (not

shown) is provided throughout an inner surface of the casing **10**. Thereby, heat energy inside the casing **10** is inhibited from being radiated outward from a wall of the casing **10**.

[0047] A middle portion of the rear wall **12** is connected to the frame **3d** of the aforementioned tower **3**. Thereby, the casing **10** is supported on the tower **3**.

[0048] As shown in FIG. 2, the piping system **20** has a plurality of heat receiver tubes **21**, an inlet header tube **22**, and an outlet header tube **23**.

[0049] The plurality of heat receiver tubes **21** are housed in the casing **10**, and are arranged in a row along an inner surface of the rear wall **12** away from one another at predetermined pitches with an extending direction thereof directed in a vertical direction. Each heat receiver tube **21** has a lower end (one end) connected to the inlet header tube **22** and an upper end (the other end) connected to the outlet header tube **23**.

[0050] The heat receiver tubes **21** heat the air A flowing therein by tube walls to which heat is applied by receiving the solar light H entering through the aperture **10a**.

[0051] The upstream ends (lower ends) of the plurality of heat receiver tubes **21** in a flowing direction of the air A are all connected to the inlet header tube **22**, and the inlet header tube **22** distributes the air A introduced from the compressor of the gas turbine unit **102** to each heat receiver tube **21**.

[0052] The inlet header tube **22** is a tube which extends along the inner surface of the rear wall **12** in a direction in which the heat receiver tubes **21** are arranged at an inner lower portion of the casing **10** and in the extending direction of which both ends thereof are closed. Both end sides of the inlet header tube **22** are provided with respective inlets (flow parts) **20a** of fluid supply passages **31** one by one.

[0053] Each fluid supply passage **31** extends downward from the inlet header tube **22**, is loosely inserted into a through-hole **14a** (see FIG. 4) formed in the bottom wall **14** of the casing **10**, and is pulled out of the casing **10**. Then, upstream ends of the fluid supply passages **31** are connected to the compressor of the gas turbine unit **102** described above, and are supplied with the air A from the compressor. A seal member, which seals each fluid supply passage **31** and the casing **10** to enable relative displacement, may be provided between each fluid supply passage **31** and each through-hole **14a**.

[0054] The downstream ends (upper ends) of the plurality of heat receiver tubes **21** in the flowing direction of the air A are all connected to the outlet header tube **23**, and the outlet header tube **23** collects the air A flowing through each heat receiver tube **21** and leads the collected air A to the gas turbine unit **102**.

[0055] The outlet header tube **23** is a tube which extends along the inner surface of the rear wall **12** in the direction in which the heat receiver tubes **21** are arranged at an inner upper portion of the casing **10** and in the extending direction of which both ends thereof are closed. The middle of the inlet header tube **22** in the extending direction is provided with an outlet (flow part) **20b** of a fluid discharge passage **32**.

[0056] The fluid discharge passage **32** extends upward from the outlet header tube **23**, is loosely inserted into a through-hole **13a** (see FIG. 4) formed in the top wall **13** of the casing **10**, and is pulled out of the casing **10**. Then, a downstream side of the fluid discharge passage **32** is connected to the turbine described above. The air A to which heat is applied by the heat receiver tubes **21** is supplied to the turbine through the fluid discharge passage **32**. A seal member, which seals the fluid discharge passage **32** and the casing **10** to enable relative

displacement, may be provided between the fluid discharge passage 32 and the through-hole 13a.

[0057] As shown in FIG. 4, the piping system 20 is configured so that, in comparison with an inner diameter d_1 of each heat receiver tube 21, an inner diameter d_2 of the inlet header tube 22 and an inner diameter d_3 of the outlet header tube 23 are set to be larger. Further, in comparison with the inner diameter d_2 of the inlet header tube 22, the inner diameter d_3 of the outlet header tube 23 is set to be larger.

[0058] In the piping system 20, paths C along which the air A flows from the two inlets 20a of the inlet header tube 22 to the outlet 20b of the outlet header tube 23 are formed in the respective heat receiver tubes 21 (see FIG. 5).

[0059] Here, pressure loss ΔP_f of a conduit is generally obtained by Expression (1) below.

$$\Delta P_f = 4f(\rho u^2/2) \cdot (L/D) \quad \text{Expression (1)}$$

where f is a tube friction coefficient, ρ is a density of a fluid, u is an average speed of the fluid, L is an overall length of the conduit, and D is an inner diameter. Further, with regard to the tube friction coefficient f , for example, the Swamee-Jain equation may be used.

[0060] Next, an operation of the aforementioned solar heat receiver 5 will be described.

[0061] First, when the air A is sent from the compressor of the gas turbine unit 102 to the piping system 20 via the fluid supply passages 31, the air A from the two inlets 20a is introduced into the inlet header tube 22. The air A introduced into the inlet header tube 22 is distributed to each heat receiver tube 21, and flows to any of the heat receiver tubes 21. The air A is heated by the tube walls to which heat is applied by the solar light H while the air A flows inside the heat receiver tubes 21. Then, the air A heated by passing through the heat receiver tubes 21 is collected by the outlet header tube 23, and is led to the turbine of the gas turbine unit 102.

[0062] In this case, in comparison with the inner diameter d_1 of the heat receiver tube 21, the inner diameter d_2 of the inlet header tube 22 and the inner diameter d_3 of the outlet header tube 23 are set to be larger. As such, in each path C, the air A per unit length passes relatively smoothly through the inlet header tube 22 and the outlet header tube 23, compared to the heat receiver tubes 21.

[0063] Further, when passing through the heat receiver tubes 21, the air A is subjected to thermal expansion due to the heating, and thereby a volume flow rate thereof increases. For this reason, the volume flow rate of the air A passing through the outlet header tube 23 increases, compared to the heat receiver tubes 21 and the inlet header tube 22. However, since the inner diameter d_3 of the outlet header tube 23 is set to be larger than the inner diameter d_1 of the heat receiver tube 21 and the inner diameter d_2 of the inlet header tube 22, the air A passes smoothly through the outlet header tube 23.

[0064] As described above, according to the solar heat receiver 5, the air A passes smoothly through the inlet header tube 22 and the outlet header tube 23.

[0065] To be more specific, lengths of the paths C are different in each of the inlet header tube 22 and the outlet header tube 23 (see FIG. 5). In other words, depending on an arrangement position of the heat receiver tube 21 of each path C, a distance from an inlet 21a of each heat receiver tube 21 to the inlet 20a adjacent to the corresponding inlet 21a and a distance from an outlet 21b of each heat receiver tube 21 to the outlet 20b adjacent to the corresponding outlet 21b are different from each other. For this reason, in comparison with the

heat receiver tubes 21 whose lengths are the same in the paths C, the inlet header tube 22 and the outlet header tube 23 easily influence a variation in energy loss between the paths C (see Expression (1)). In other words, when the inner diameters d_2 and d_3 are reduced in the inlet header tube 22 and the outlet header tube 23, a flow speed of the air A is increased. As such, as the heat receiver tubes 21 become distant from the inlet 20a and the outlet 20b, the energy loss shows a tendency to increase.

[0066] However, in the solar heat receiver 5, the inner diameters d_2 and d_3 are set to be larger than the inner diameter d_1 . For this reason, a ratio of the energy loss (ΔP_f_2 and ΔP_f_6 to be described below) in the inlet header tube 22 and the outlet header tube 23 to the sum of the energy loss on each path C is smaller than that in the heat receiver tubes 21, whereas a ratio of the energy loss (ΔP_f_4 to be described below) in the heat receiver tubes 21 to the sum of the energy loss is larger than those in the inlet header tube 22 and the outlet header tube 23. In other words, since the energy loss is suppressed in the inlet header tube 22 and the outlet header tube 23 having different lengths on each path C, a difference in the sum of the energy loss on each path C is also reduced. Accordingly, it is possible to reduce a difference in the flow rate of the air A flowing along each path C, and uniformize distribution of the flow rate between the paths C. Thus, it is possible to uniformize temperature distribution of the plurality of paths C and heating performance for the air A of each path C.

[0067] Further, the inner diameter d_3 of the outlet header tube 23 is set to be larger than the inner diameter d_1 of the heat receiver tube 21 and the inner diameter d_2 of the inlet header tube 22. As such, even when the air A whose volume flow rate is increased flows to the outlet header tube 23, the flow speed of the air A is inhibited from being increased. Thereby, the energy loss proportional to the flow speed of the air A can also be suppressed. Accordingly, it is possible to further reduce the difference in the flow rate of the air A flowing along each path C, and further uniformize the flow rate distribution to each path C.

[0068] Further, since the two inlets 20a are provided for the inlet header tube 22, an average distance from the inlet 21a of each heat receiver tube 21 to the inlet 20a closest to the corresponding inlet 21a can be reduced. Thereby, it is possible to suppress the energy loss (ΔP_f_2 to be described below) generated between the inlet 20a and the inlet 21a of the heat receiver tube 21, and reduce the difference in the flow rate of the air A flowing along each path C. Thus, the flow rate distribution can be uniformized.

[0069] Further, according to the aforementioned solar heat power generation device 100, since the solar heat receiver 5 is provided, the temperature distribution of the plurality of paths C and the heating performance for the air A of each path C are uniformized. As such, the solar heat power generation device 100 can be configured as a system having high durability.

[0070] In the aforementioned embodiment, the inner diameters are set as the inner diameter $d_3 >$ the inner diameter $d_2 >$ the inner diameter d_1 . However, the inner diameters d (d_1, d_2, d_3) are set in the following method, and thereby the energy loss between the paths C can be further uniformized.

[0071] That is to say, as shown in FIG. 5, the energy loss Δf_i of the path C is mainly the sum $\Sigma \Delta P_f_i$ of discharge loss ($=\Delta P_f_1$) of the inlet 20a, friction loss ($=\Delta P_f_2$) from the inlet 20a to the inlet 21a of the heat receiver tube 21, suction loss ($=\Delta P_f_3$) of the inlet 21a of the heat receiver tube 21, friction loss ($=\Delta P_f_4$) in the heat receiver tube 21, discharge loss

($=\Delta P_{f_5}$) from the outlet **21b** of the heat receiver tube **21**, and friction loss ($=\Delta P_{f_6}$) from the outlet **21b** of the heat receiver tube **21** to the outlet **20b**.

[0072] For this reason, ΔP_{f_i} is integrated with respect to each of the paths $C_1, C_2, C_3 \dots C_n$. That is, $\Sigma \Delta P_{f_i} (=P_{C1})$ of the path C_1 , $\Sigma \Delta P_{f_i} (=P_{C2})$ of the path C_2 , $\Sigma \Delta P_{f_i} (=P_{C3})$ of the path $C_3 \dots \Sigma \Delta P_{f_i} (=P_{Cn})$ of the path C_n are obtained.

[0073] As described above, when the inner diameter d_2 of the inlet header tube **22** and the inner diameter d_3 of the outlet header tube **23** are the same level as the inner diameter d_1 of the heat receiver tube **21**, the friction loss ($=\Delta P_{f_2}$) from the inlet **20a** to the heat receiver tube **21**, the suction loss ($=\Delta P_{f_3}$) to the inlet **21a** of the heat receiver tube **21**, and the discharge loss ($=\Delta P_{f_5}$) to the outlet **21b** of the heat receiver tube **21** are increased, and differences of $P_{C1}, P_{C2}, P_{C3} \dots P_{Cn}$ are increased (variation between the paths C is increased to be uniform).

[0074] For this reason, in comparison with the inner diameter d_1 of the heat receiver tube **21**, the inner diameter d_2 of the inlet header tube **22** and the inner diameter d_3 of the outlet header tube **23** are increased to reduce each of the differences of $P_{C1}, P_{C2}, P_{C3} \dots P_{Cn}$. When the inner diameter $d_1, d_2,$ and d_3 are determined, design is made by finding an optimal resolution meeting conditions that $|P_{C1}-P_{C2}| \cong |P_{C1}-P_{C3}| \cong \dots \cong |P_{C1}-P_{Cn}| \cong |P_{C2}-P_{C3}| \cong |P_{C2}-P_{C4}| \cong \dots \cong |P_{C2}-P_{Cn}| \cong \dots \cong |P_{C(n-1)}-P_{Cn}|$, and this value becomes a minimum value. By doing this, each of the differences of $P_{C1}, P_{C2}, P_{C3} \dots P_{Cn}$ with respect to each of the paths $C_1, C_2, C_3 \dots C_n$ is reduced, and the respective energy loss is approximately identical. As such, the flow rate distribution is further uniformized.

[0075] The operation processes, or various shapes and combinations of each component shown in the aforementioned embodiment are given as one example, and the present invention may be variously modified on the basis of design requirements without departing from the scope of the present invention.

[0076] For example, the heat receiver tubes **21** are arranged in a linear shape, and the inlet header tube **22** and the outlet header tube **23** are formed in a rectangular shape. However, the heat receiver tubes **21** may be arranged in a round shape, and the inlet header tube and the outlet header tube extending in the direction in which the heat receiver tubes **21** are arranged may be used. In this case, the heat receiver tubes **21** may be arranged in an arcuate shape or in a completely round shape, and the inlet header tube and the outlet header tube may be formed to extend in an arcuate shape or in a completely round shape. Further, when the inlet header tube and the outlet header tube are formed in the completely round shape, interiors of the inlet header tube and the outlet header tube may be partitioned into a plurality of spaces.

[0077] Further, the aforementioned embodiment is configured so that the inner diameters d_2 and d_3 of both of the inlet header tube **22** and the outlet header tube **23** are larger than the inner diameter d_1 of the heat receiver tube **21**. However, even when only one of the inner diameters d_2 and d_3 is larger than the inner diameter d_1 , the energy loss between the paths C can be uniformized.

[0078] Further, the aforementioned embodiment is configured so that the two inlets **20a** are formed in the inlet header tube **22**. However, three or more inlets may be formed, or only one inlet may be formed. The inlet **20a** may be provided at an arbitrary position.

[0079] Further, the aforementioned embodiment is configured so that one outlet **20b** is formed in the outlet header tube

23. However, two or more outlets may be formed. Even in this case, in comparison with when only one outlet **20b** is formed, the average distance between the outlet **20b** and the inlet **21a** of each heat receiver tube **21** can be reduced. As such, it is possible to suppress the energy loss in the outlet header tube **23** of each path C .

[0080] In addition, the aforementioned embodiment is configured so that the air A is sent from the compressor of the gas turbine unit **102** to the solar heat receiver **5**, and the air A is sent from the solar heat receiver **5** to the turbine of the gas turbine unit **102**. However, the air A may be sent from another fluid supply source to the solar heat receiver **5**, and the air A may be sent from the solar heat receiver **5** to another fluid supply destination. Further, a heat medium other than the air A may be heated by the heat receiver tubes **21**.

INDUSTRIAL APPLICABILITY

[0081] According to the aforementioned solar heat receiver, it is possible to uniformize the temperature distribution of the plurality of paths and the heating performance for the heat medium of each path. Further, according to the aforementioned solar heat power generation device, it is possible to uniformize the temperature distribution of the plurality of paths and the heating performance for the heat medium of each path. As such, the solar heat power generation device can be configured as a system having excellent durability.

REFERENCE SIGNS LIST

- [0082] 2: heliostat
- [0083] 3: tower
- [0084] 5: solar heat receiver
- [0085] 10: casing
- [0086] 10a: aperture
- [0087] 20: piping system
- [0088] 20a: inlet (flow port)
- [0089] 20b: outlet (flow port)
- [0090] 21: heat receiver tube
- [0091] 22: inlet header tube
- [0092] 23: outlet header tube
- [0093] A: air (working fluid)
- [0094] C ($C_1, C_2, C_3 \dots C_n$): path
- [0095] H (H1, H2): solar light
- [0096] d (d_1, d_2, d_3): inner diameter
- [0097] 100: solar heat power generation device
- [0098] 102: gas turbine unit (fluid supply source, fluid supply destination)

1. A solar heat receiver comprising:
 - a casing having an aperture configured to let solar light to enter; and
 - a piping system installed in the casing and configured to discharge a heat medium, which is sent from a fluid supply source of an outside, to a fluid supply destination of the outside after the heat medium is heated by the solar light,
 wherein the piping system includes:
 - a plurality of heat receiver tubes housed in the casing and configured to receive the solar light entering through the aperture of the casing and to heat the heat medium flowing therein;
 - an inlet header tube connected to one end side of each of the heat receiver tubes and configured to distribute the heat medium, which is introduced from the fluid supply source, to each of the heat receiver tubes; and

an outlet header tube connected to the other end side of each of the heat receiver tubes and configured to collect the heat medium passing through each of the heat receiver tubes and to lead the collected heat medium to the fluid supply destination, and

the inlet header tube and the outlet header tube have a larger inner diameter than each of the heat receiver tubes.

2. The solar heat receiver according to claim 1, wherein the outlet header tube is set to have a larger inner diameter than the inlet header tube.

3. The solar heat receiver according to claim 1, wherein at least one of the inlet header tube and the outlet header tube includes a plurality of flow ports, through which the heat medium is caused to flow and which are installed between the outside and the at least one of the inlet header tube and the outlet header tube.

4. The solar heat receiver according to claim 1, wherein the heat medium is air.

5. A solar heat power generation device comprising:

the solar heat receiver according to claim 1;

a tower erected on a ground and configured to fixedly install the solar heat receiver at a high position;

a plurality of heliostats disposed around the tower within a predetermined angular range and each configured to cause the solar light to enter through the aperture of the solar heat receiver; and

a gas turbine unit comprising a compressor acting as the fluid supply source, a turbine acting as the fluid supply destination, and an electric generator configured to be driven rotatably by the turbine.

* * * * *