

# **United States Patent 1991**

# Dey et al.

#### 54) METHOD OF ASSESSING A SURFACE FIGURE OF AN OPTICAL ELEMENT

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## Related U.S. Application Data

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- 51 Int. Cl... G01B 9/00
- 52) U.S. C. .................................... 356/124; 359/727;
- 58) Field of Search ..................... 356/124, 124.5, 125, 356/359 356/126, 127, 153,359-360; 359/727, 869, 641,

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## U.S. PATENT DOCUMENTS



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# [57] **ABSTRACT**

A novel method for assessing a surface figure of an optical element. The method preferably comprises sub jecting the optical element to a classical autocollimation relative to a predetermined ideal. The testing procedure is characterized by a step of modifying the classical optical testing procedure, so that the optical element under test simulates a paraboloid.

# 5 Claims, 6 Drawing Sheets



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FIG./ PRIOR ART







PRIOR ART

# TABLE

RITCHEY - CHRETIEN PRIMARY MIRRORS (EXAMPLES)



\* BEST FIT PEAK-TO-VALLEY SURFACE DEPARTURE MEASURED IN WAVELENGTHS OF HELIUM-NEOW LASER LIGHT AT O6328 MICROMETER WAVELENGTH.

# $F/G.4$







# METHOD OF ASSESSING A SURFACE FIGURE OF AN OPTICAL ELEMENT

I his is a continuation of application Ser. No.  $5$ 07/853,478, filed on Mar. 18, 1992 now abandoned.

# FIELD OF THE INVENTION

This invention relates to a method for assessing a surface figure of an optical element.

# INTRODUCTION TO THE INVENTION

Methods for assessing a surface figure, as character ized, for example,by a vertex radius of curvature R, a conic constant k, or, an algebraically related conic ec 15 centricity  $\epsilon$ , of an optical element, for example, a primary mirror of a conventional telescope, are known.

One objective of such a method is to expedite a fabri cation process of the optical element, so that, by way of, for example, standard polishing techniques, a method 20 discerned actual surface parameter,  $k_a$ , can be compared to a desired or idealized surface figure,  $k_i$ , to an end of converging on an optimal null,  $|k_a - k_i| = 0$ .<br>Further particulars and illustrations of such assessing

Further particulars and illustrations of such assessing methods are disclosed, for example, in Shannon, R. R. 25 et al: Applied Optics and Optical Engineering, Vol. VIII, pages 80–85, Academic Press, New York, 1980; and, Malacara, D., Optical Shop Testing, Chapter 14 and Appendix 4, John Wiley and Sons, New York, 1978. 30

## SUMMARY OF THE INVENTION

As alluded to above, methods for assessing a surface figure may include such assessments of a primary mirror of a conventional telescope. The choice of a particular 35 assessment methodology includes considerations of a particularly chosen telescope.

For example, it is known to employ an autocollimation assessing methodology to a Newtonian telescope (FIG. 1, numeral 10) comprising a paraboloidal primary 40 mirror 12. As shown in FIG. 2, the autocollimation assessing method can be used to compare the FIG. 1 paraboloidal primary mirror 12 conic constant  $k=-1.0$ , to an idealized "aspheric departure",  $k=0$ .

As a second example, it is also known to employ a  $45$  and: surface figure assessing methodology to a Ritchey Chrétien two mirror telescope 14 (FIG. 3) comprising a hyperboloidal primary mirror 16. Important such asses sing methodologies for the telescope 14 include inter alia: (1) a conventional Foucault knife-edge test; (2) a 50 Hartmann test; (3) a wire test; or (4), an interferometric test. For each such methodology, (and again, with ref erence to FIG. 2), one can compare a hyperboloidal primary mirror 16 conic constant  $k_a$ , to the idealized 55

'aspheric departure'',  $k=0$ .<br>We now make the following critique of the preceding conventional methodology comprising aspheric departure, as it may be applied to an optical element compris ing an hyperboloid, or, additionally, a prolate ellipsoid.

With reference to FIG. 2, we preliminarily note that 60 the extant methodologies are based on a conceit of making an hyperboloid  $(k < -1.0)$  "like" a sphere  $(k=0)$  (i.e., traditional "aspheric departure"). However, by now referencing a FIG. 2 paraboloid  $(k=-1.0)$ , we note, for the first time, that an aparaboloidal departure 65 may be a more meaningful and suitable metric of test ability for the hyperboloid or prolate ellipsoid, com pared to an aspheric departure, since the paraboloidal

 $2$  surface topology may be observed to be geometrically closer to the hyperboloidal surface topology, than the spherical surface topology.<br>A critique of the conventional methodology compris-

10 severely shaped testing lenses, than a methodology ing aspheric departure, for the case of an hyperboloid or prolate ellipsoid, follows accordingly: that it may be compared to a paraboloid, thus disadvantageously requiring, for example, more testing lenses, and more which assesses an hyperboloid for its aparaboloidal departure.

These last points may be confirmed by reference to a Table set out in FIG. 4. The Table comprises computed and tabulated departures for two Ritchey-Chrétien hyperboloidal primary mirrors A,B, of first and second diameters, respectively; their departures relative to a best-fit sphere, and relative to a best-fit paraboloid.

The Table computations show that an aparaboloidal departure is a small percentage of the aspheric departure. That is, for the vast majority of Ritchey-Chrétien hyperboloidal primary mirrors comprising a conic constant k close to  $k = -1.0$ , the primary mirror is much closer to the paraboloid  $(k = -1.0)$ , than to the sphere  $(k=0)$ . This suggests to us, that because the paraboloid has an ideal null test (the autocollimation configuration), an aparaboloidal departure may be a more meaningful assessing methodology for assessing a surface figure of an optical element, than heretofore compre hended.

Accordingly, based on these insights, we now dis close a novel method for assessing a surface figure of an optical element. The novel method of the present inven tion comprises the steps of:

- (a) subjecting the optical element to a classical colli mation testing procedure for ascertaining its sur face figure relative to a predetermined ideal;
- the testing procedure characterized by a step of: (b) modifying the classical optical testing procedure so that the optical element under test simulates a paraboloid.

The novel method, compared to prior art methodolo gies, can realize important advantages, including inter

- 1) providing simplification in the number of lenses required to employ an autocollimation method;
- 2) eliminating heretofore typically required severely shaped lenses;
- 3) providing an efficient capability for assessing a i.e. more aspheric optical elements; and
- 4) providing correction capabilities for better than 0.001 waves of visible light surface departure from ideal, for example, compared to prior art correc tions frequently measured as 0.01 waves.

## BRIEF DESCRIPTION OF THE DRAWING

The invention is illustrated in the accompanying

FIG. 1 shows a schematic of a Newtonian telescope primary mirror test configuration;

FIG. 2 shows a family of concave conicoids;

FIG. 3 shows a schematic of a Ritchey-Chrétien

FIG. 4 shows a Table comparing aparaboloidal de partures versus aspheric departures for two Ritchey Chrétien primary mirrors;

FIG. 5 shows an optical assembly that may be used to realize preferred steps of the method of the present invention; and

FIGS. 6A,B show correcting lenses used in the pres ent method.

#### DETAILED DESCRIPTION OF THE INVENTION

We first turn our attention to preferred aspects of the method of the present invention.

Preamble: A method for assessing a surface figure of an optical element.

The optical element may comprise a conventional lens, a conventional diffraction grating, or a conven tional mirror, for example, a primary mirror of a Ritch- 15.<br>ey-Chrétien telescope

The optical element may define a concave conicoid geometry, for example, an hyperboloid or a prolate ellipsoid. In a degenerate case, the optical element may define a paraboloidal geometry.<br>The surface figure (or topology) of the optical element may comprise, for example, a conic constant, k,

typically specified, for example, as some such parameter as " $k = -1.021$ ", or, an algebraically related eccentricity, e.

## Step A

Subjecting the optical element to a classical collimation testing procedure for ascertaining its surface figure relative to a predetermined ideal. 30

The classical collimation testing procedure may com prise inter alia:

1) a conventional Foucault knife-edge test;

- 2) a conventional Hartmann test;
- 3) a conventional wire test; or

4) a conventional interferometric test.

#### Step B

Modifying the classical optical testing procedure so that the optical element under test simulates a parabo- 40 loid.

Step B functions to qualify step A, thereby creating a pseudo-autocollimation test. The point of this qualifica tion is to effect a suitable metric of testability of the optical element, so that its geometry may be referenced 45 for its aparaboloidal departure (recall FIG. 2, supra), within the context, otherwise, of a classical optical testing procedure.

A preferred means for effecting such a pseudo autocollimation test is set forth immediately below, 50 (FIG. 5), in the context of an illustrative optical assem bly 18 that may be employed to realize preferred steps of the method of the present invention.

The FIG. 5 optical assembly 18 comprises a portion of a conventional Ritchey-Chrétien telescope, and in-55 cludes a flat mirror 20, and an optical element 22 com prising a large primary mirror defining an hyperboloi dal geometry. The optical assembly 18 also includes a low profile conventional interferometer 24, and a small single element refractive correcting lens  $26$ . The cor-  $60$ recting lens 26 is preferably optically designed to cor rect a relatively small amount of spherical aberration dal departure of the hyperboloidal primary mirror 22, relative to a best-fit paraboloid. Two examples of pre- 65 ferred such correcting lenses 26 are illustrated in FIGS. Chrétien primary mirrors of FIG. 4, supra. An algo-

rithm for designing a lens is disclosed in an Appendix, infra.

5 focal point associated with the traditional classical test, 10 tional aspheric departure method, may be replaced by a In operation, a FIG. 6 lens (28 or 30) is preferably located in the FIG. 5 optical assembly 18 between a (here, the interferometric autocollimation test), of a best-fit paraboloid in the autocollimation configuration. (Note, in this regard, that a customarily large and obtrusive aspheric reflective nulling mirror used in a conven simple lens e.g., a lens 28 or 30). The pseudo-autocolli-<br>mation test now proceeds, consistent, otherwise, with classical steps, for assessing the surface figure of the optical element 22 as it simulates a paraboloid.

#### APPENDIX

#### Algorithm for Designing a Refractive Lens Element

 $_{25}$  mirror of FIG. 5. A lens designer with accesss to a modern computer-<br> $_{20}$  assisted lens design program, can find a determination of an appropriate lens for use in the pseudo-autocollina tion test. Outlined below is a method used by the inven tors, to generate lenses providing excellent correction (to better than 0.001 wavelength) of the hyperboloid

#### Step 1

Select a material for a lens element. A common optical glass is appropriate, for example BK7 crown. An especially good choice is FSV fused silica which is thermally stable.

#### Step 2

 $35$  between  $\frac{1}{4}$  to 1 percent of the vertex radius of curvature Select a lens thickness. A good choice is likely to be of a mirror to be tested.

#### Step 3

Select a radii of curvature of the lens surfaces. A good choice is likely to be between 10 and 20 times the lens thickness. The surface toward the mirror is convex. The other surface is concave.

#### Step 4

Select a separation between the lens and the vertex of the mirror to be tested. A good choice is between 46 and 48 percent of the vertex radius of curvature of the mirror to be tested.

## Step 5

Enter the mirror-lens configuration into a commer cial computerized lens-design program such as Genii II or Code V.

#### Step 6

Simulate an axial point offset at infinite distance, pro jecting light parallel to the axis of symmetry of the mirror.

#### Step 7

Utilize the computer optimization software to vary the radii of the lens surfaces independently to minimize spherical aberration.

#### Step 8

Examine the lens size and shape. If it is undesirably large, the separation between mirror and lens can be increased. Returning to Step 5 should then result in a

smaller lens. If the radii of the lens surfaces are too short, the thickness of the lens can be increased. Return ing to Step 5 should then result in longer radii for the lens surfaces. A viable alternative to the detailed lens described, is especially appropriate if a Fizeau interfer 5 ometer is to be used as part of the test set (e.g., a Zygo interferometer). In this case, the correcting lens may be placed farther from the mirror than half its radius of curvature. Note that in this case, the concave surface is toward the mirror under test. 10

What is claimed:

1. A method for assessing a surface configuration of a concave conacoid optical element having a conic con stant closer to the conic constant of a paraboloid than to the conic constant of a sphere, comprising the steps of: 15

- a generating a correcting lens designed to correct departure of said optical element relative to a parabaloid mathematically best fit to the surface of said element; 20
- b. interposing said correcting lens between the sur face of said concave conacoid optical element and a focal point of said element; and
- c. subjecting the optical element with correcting lens to a classical collimation testing procedure for 25 ascertaining its surface configuration relative to said paraboloid.

2. The method of claim 1 wherein the conacoid optical element defines a hyperboloid.

 $5,361,129$ <br>5<br>of the lens surfaces are too 3. The method of claim 1 wherein the conacoid optical element defines a prolate ellipsoid.

> 4. The method of claim 1 wherein said correcting lens provides a correction of the optical element to less than

> 0.001 wave length of visible light.<br>5. The method claimed in claim 1, wherein said step of generating a correcting lens comprises the steps of:

- a selecting a material for a lens element;
- b. selecting a lens thickness;
- c. selecting radii of curvature of the lens surfaces;
- d. selecting a separation of the lens and the vertex of the optical element;
- e. entering the optical element-correcting lens config uration into a commercial computerized lens-<br>design program;<br>f. simulating an axial point offset at infinite distance,
- projecting light parallel to the axis of symmetry of the optical element;
- g. utilizing the lens-design program to vary the radii of the correcting lens surfaces independently to minimize spherical aberration; and
- h. examining the correcting lens size and shape and<br>i. if it is undesirably large, increase the separation between the optical element and the correcting lens and repeat steps e through h,
	- ii. if the radii of the correcting lens surfaces are too lens and repeat steps e through h.  $* * * * * * *$

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