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(54) **SURFACE-COATED CUTTING TOOL AND METHOD FOR MANUFACTURING SAME**

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(57) **ABSTRACT**

(21) Appl. No.: **16/482,156**

A surface-coated cutting tool includes a substrate and a coating film that coats the substrate, wherein the coating film includes a hard coating layer constituted of a domain region and a matrix region, the domain region is a region having a plurality of portions divided and distributed in the matrix region, the domain region has a structure in which a first layer composed of a first  $Al_{x1}Ti_{(1-x1)}$  compound and a second layer composed of a second  $Al_{x2}Ti_{(1-x2)}$  compound are layered on each other, the matrix region has a structure in which a third layer composed of a third  $Al_{x3}Ti_{(1-x3)}$  compound and a fourth layer composed of a fourth  $Al_{x4}Ti_{(1-x4)}$  compound are layered on each other.

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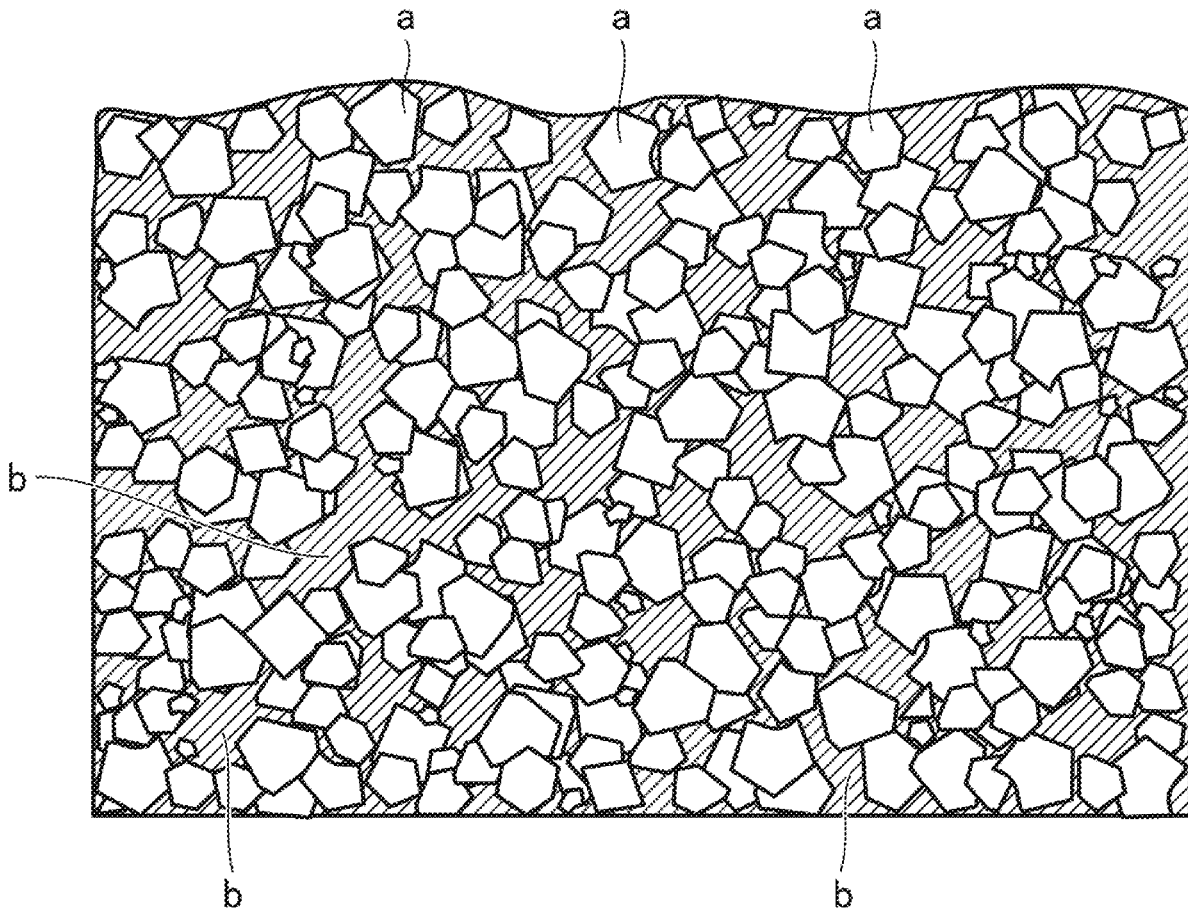


FIG.1

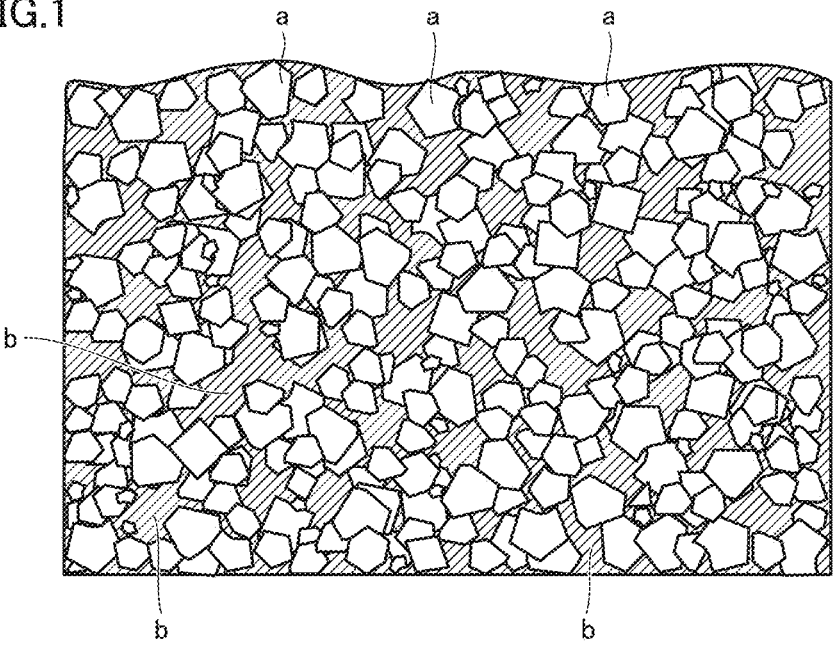


FIG.2

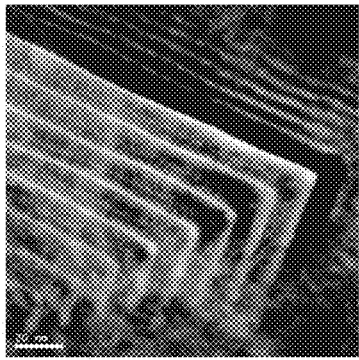


FIG.3

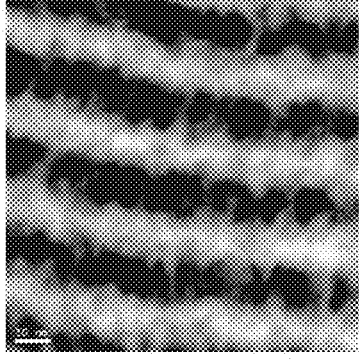


FIG.4

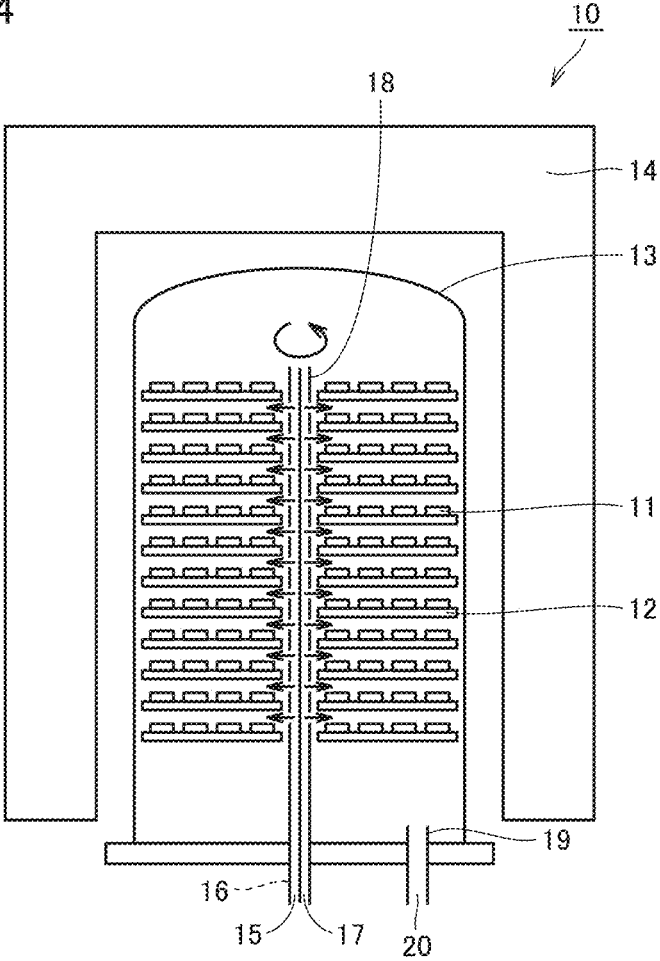
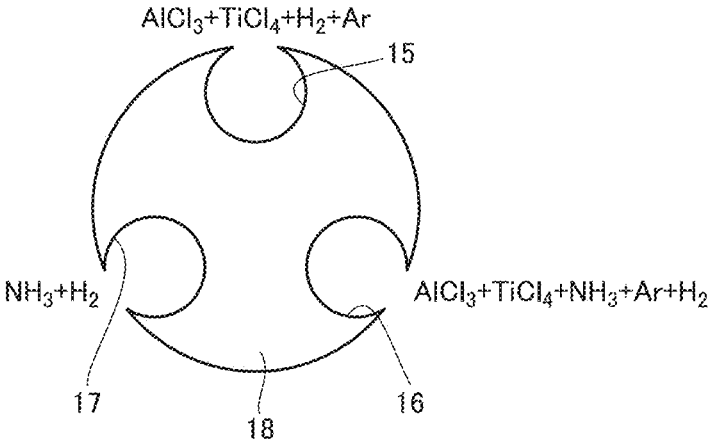


FIG.5



## SURFACE-COATED CUTTING TOOL AND METHOD FOR MANUFACTURING SAME

### TECHNICAL FIELD

**[0001]** The present disclosure relates to a surface-coated cutting tool and a method for manufacturing the surface-coated cutting tool. The present application claims a priority based on Japanese Patent Application No. 2018-054716 filed on Mar. 22, 2018, the entire content of which is incorporated herein by reference.

### BACKGROUND ART

**[0002]** Conventionally, a cutting tool composed of cemented carbide has been used to cut steel, casting, or the like. During the cutting, the cutting edge of such a cutting tool is exposed to a severe environment such as high temperature and high stress, thus resulting in wear and breakage of the cutting edge.

**[0003]** Therefore, in order to improve the life of the cutting tool, it is important to suppress the wear and breakage of the cutting edge.

**[0004]** In order to improve cutting performance of the cutting tool, coating films, each of which coats a surface of a substrate composed of cemented carbide or the like, have been developed. Among them, a coating film composed of a compound (hereinafter, also referred to as "AlTiN") of aluminum (Al), titanium (Ti), and nitrogen (N) can have high hardness, and can have improved oxidation resistance by increasing a content ratio of Al (for example, Japanese National Patent Publication No. 2015-509858 (Patent Literature 1), Japanese National Patent Publication No. 2017-508632 (Patent Literature 2), and Japanese Patent Laying-Open No. 2016-130343 (Patent Literature 3)).

### CITATION LIST

#### Patent Literature

- [0005]** PTL 1: Japanese National Patent Publication No. 2015-509858  
**[0006]** PTL 2: Japanese National Patent Publication No. 2017-508632  
**[0007]** PTL 3: Japanese Patent Laying-Open No. 2016-130343

### SUMMARY OF INVENTION

**[0008]** (1) A surface-coated cutting tool according to the present disclosure includes a substrate and a coating film that coats the substrate, wherein

**[0009]** the coating film includes a hard coating layer constituted of a domain region and a matrix region,

**[0010]** the domain region is a region having a plurality of portions divided and distributed in the matrix region,

**[0011]** the domain region has a structure in which a first layer and a second layer are layered on each other, the first layer being composed of at least one first AlTi compound selected from a group consisting of  $Al_{x1}Ti_{(1-x1)}N$ ,  $Al_{x1}Ti_{(1-x1)}BN$ , and  $Al_{x1}Ti_{(1-x1)}CN$ , the second layer being composed of at least one second AlTi compound selected from a group consisting of  $Al_{x2}Ti_{(1-x2)}N$ ,  $Al_{x2}Ti_{(1-x2)}BN$ , and  $Al_{x2}Ti_{(1-x2)}CN$ ,

**[0012]** the matrix region has a structure in which a third layer and a fourth layer are layered on each other, the third layer being composed of at least one third AlTi compound

selected from a group consisting of  $Al_{x3}Ti_{(1-x3)}N$ ,  $Al_{x3}Ti_{(1-x3)}BN$ , and  $Al_{x3}Ti_{(1-x3)}CN$ , the fourth layer being composed of at least one fourth AlTi compound selected from a group consisting of  $Al_{x4}Ti_{(1-x4)}N$ ,  $Al_{x4}Ti_{(1-x4)}BN$ , and  $Al_{x4}Ti_{(1-x4)}CN$ ,

**[0013]** the first AlTi compound has a hexagonal crystal structure, and the second AlTi compound has a cubic crystal structure,

**[0014]** the third AlTi compound has a cubic crystal structure, and the fourth AlTi compound has a cubic crystal structure,

**[0015]**  $x1$  is more than or equal to 0.9 and less than or equal to 0.95,

**[0016]**  $x2$  is more than or equal to 0.5 and less than or equal to 0.6,

**[0017]**  $x3$  is more than or equal to 0.75 and less than or equal to 0.85, and

**[0018]**  $x4$  is more than or equal to 0.5 and less than or equal to 0.6.

**[0019]** (2) A method for manufacturing a surface-coated cutting tool according to the present disclosure is a method for manufacturing the surface-coated cutting tool recited in (1), and includes:

**[0020]** preparing the substrate, and

**[0021]** emitting first gas, second gas, and third gas to the substrate in an atmosphere at more than or equal to 650° C. and less than or equal to 900° C. and under more than or equal to 0.5 kPa and less than or equal to 5 kPa, the first gas including aluminum halide gas and titanium halide gas, the second gas including aluminum halide gas, titanium halide gas, and ammonia gas, the third gas including ammonia gas.

### BRIEF DESCRIPTION OF DRAWINGS

**[0022]** FIG. 1 is a schematic view of a hard coating layer included in a coating film of a surface-coated cutting tool according to the present embodiment.

**[0023]** FIG. 2 shows an exemplary enlarged photograph of a region a.

**[0024]** FIG. 3 shows an exemplary enlarged photograph of a region b.

**[0025]** FIG. 4 is a schematic cross sectional view of a CVD apparatus used to manufacture the surface-coated cutting tool according to the present embodiment.

**[0026]** FIG. 5 is a schematic cross sectional view of a gas inlet pipe of the CVD apparatus used to manufacture the surface-coated cutting tool according to the present embodiment.

### DETAILED DESCRIPTION

#### Problem to be Solved by the Present Disclosure

**[0027]** In recent years, more efficient cutting (with an increased feed rate) has been required. It has been expected to further improve breakage resistance and wear resistance (suppress breakage and wear of a cutting edge).

**[0028]** The present disclosure has been made in view of the above-described circumstance, and has an object to provide a surface-coated cutting tool having excellent breakage resistance and wear resistance.

### Advantageous Effect of the Present Disclosure

**[0029]** According to the description above, there can be provided a surface-coated cutting tool having excellent breakage resistance and wear resistance.

### Description of Embodiments

**[0030]** First, contents of one embodiment of the present disclosure are listed and described.

**[0031]** [1] A surface-coated cutting tool according to the present disclosure includes a substrate and a coating film that coats the substrate, wherein

**[0032]** the coating film includes a hard coating layer constituted of a domain region and a matrix region,

**[0033]** the domain region is a region having a plurality of portions divided and distributed in the matrix region,

**[0034]** the domain region has a structure in which a first layer and a second layer are layered on each other, the first layer being composed of at least one first AlTi compound selected from a group consisting of  $Al_{x1}Ti_{(1-x1)}N$ ,  $Al_{x1}Ti_{(1-x1)}BN$ , and  $Al_{x1}Ti_{(1-x1)}CN$ , the second layer being composed of at least one second AlTi compound selected from a group consisting of  $Al_{x2}Ti_{(1-x2)}N$ ,  $Al_{x2}Ti_{(1-x2)}BN$ , and  $Al_{x2}Ti_{(1-x2)}CN$ ,

**[0035]** the matrix region has a structure in which a third layer and a fourth layer are layered on each other, the third layer being composed of at least one third AlTi compound selected from a group consisting of  $Al_{x3}Ti_{(1-x3)}N$ ,  $Al_{x3}Ti_{(1-x3)}BN$ , and  $Al_{x3}Ti_{(1-x3)}CN$ , the fourth layer being composed of at least one fourth AlTi compound selected from a group consisting of  $Al_{x4}Ti_{(1-x4)}N$ ,  $Al_{x4}Ti_{(1-x4)}BN$ , and  $Al_{x4}Ti_{(1-x4)}CN$ ,

**[0036]** the first AlTi compound has a hexagonal crystal structure, and the second AlTi compound has a cubic crystal structure,

**[0037]** the third AlTi compound has a cubic crystal structure, and the fourth AlTi compound has a cubic crystal structure,

**[0038]**  $x_1$  is more than or equal to 0.9 and less than or equal to 0.95,

**[0039]**  $x_2$  is more than or equal to 0.5 and less than or equal to 0.6,

**[0040]**  $x_3$  is more than or equal to 0.75 and less than or equal to 0.85, and

**[0041]**  $x_4$  is more than or equal to 0.5 and less than or equal to 0.6.

**[0042]** Since the surface-coated cutting tool is configured as described above, the surface-coated cutting tool can have excellent breakage resistance and wear resistance.

**[0043]** [2] The domain region includes a twin crystal portion. By defining in this way, the surface-coated cutting tool has excellent chipping resistance.

**[0044]** [3] A total thickness of a thickness of the first layer and a thickness of the second layer is more than or equal to 2 nm and less than or equal to 20 nm. By defining in this way, the surface-coated cutting tool has excellent wear resistance.

**[0045]** [4] A total thickness of a thickness of the third layer and a thickness of the fourth layer is more than or equal to 1.5 nm and less than or equal to 30 nm. By defining in this way, the surface-coated cutting tool has excellent breakage resistance.

**[0046]** [5] A method for manufacturing a surface-coated cutting tool according to the present disclosure is a method for manufacturing the above-described surface-coated cutting tool, and includes:

**[0047]** preparing the substrate; and

**[0048]** emitting first gas, second gas, and third gas to the substrate in an atmosphere at more than or equal to 650° C. and less than or equal to 900° C. and under more than or equal to 0.5 kPa and less than or equal to 5 kPa, the first gas including aluminum halide gas and titanium halide gas, the second gas including aluminum halide gas, titanium halide gas, and ammonia gas, the third gas including ammonia gas.

**[0049]** Since the method for manufacturing the surface-coated cutting tool is configured as described above, a surface-coated cutting tool having excellent breakage resistance and wear resistance can be manufactured.

### Details of Embodiments of the Present Disclosure

**[0050]** The following describes one embodiment (hereinafter, referred to as “the present embodiment”) of the present disclosure. However, the present embodiment is not limited thereto. It should be noted that the same reference characters indicate the same or equivalent portions in the figures used for the below description of the embodiment. In the present specification, the expression “A to B” represents a range of lower to upper limits (i.e., more than or equal to A and less than or equal to B). When no unit is indicated for A and a unit is indicated only for B, the unit of A is the same as the unit of B. Further, in the present specification, when a compound is expressed by a chemical formula in which a composition ratio of composition elements is not limited such as “TiC”, it is assumed that the chemical formula includes all the conventionally known composition ratios (element ratios). In this case, it is assumed that the above-described chemical formula includes not only a stoichiometric composition but also a non-stoichiometric composition. For example, the chemical formula “TiC” includes not only a stoichiometric composition “ $Ti_1C_1$ ” but also a non-stoichiometric composition such as “ $Ti_1C_{0.8}$ ”. The same also applies to compounds other than the “TiC”.

**[0051]** <<Surface-Coated Cutting Tool>>

**[0052]** A surface-coated cutting tool according to the present embodiment includes a substrate and a coating film that coats the substrate, wherein

**[0053]** the coating film includes a hard coating layer constituted of a domain region and a matrix region,

**[0054]** the domain region is a region having a plurality of portions divided and distributed in the matrix region,

**[0055]** the domain region has a structure in which a first layer and a second layer are layered on each other, the first layer being composed of at least one first AlTi compound selected from a group consisting of  $Al_{x1}Ti_{(1-x1)}N$ ,  $Al_{x1}Ti_{(1-x1)}BN$ , and  $Al_{x1}Ti_{(1-x1)}CN$ , the second layer being composed of at least one second AlTi compound selected from a group consisting of  $Al_{x2}Ti_{(1-x2)}N$ ,  $Al_{x2}Ti_{(1-x2)}BN$ , and  $Al_{x2}Ti_{(1-x2)}CN$ ,

**[0056]** the matrix region has a structure in which a third layer and a fourth layer are layered on each other, the third layer being composed of at least one third AlTi compound selected from a group consisting of  $Al_{x3}Ti_{(1-x3)}N$ ,  $Al_{x3}Ti_{(1-x3)}BN$ , and  $Al_{x3}Ti_{(1-x3)}CN$ , the fourth layer being composed of at least one fourth AlTi compound selected from a group consisting of  $Al_{x4}Ti_{(1-x4)}N$ ,  $Al_{x4}Ti_{(1-x4)}BN$ , and  $Al_{x4}Ti_{(1-x4)}CN$ ,

[0057] the first AlTi compound has a hexagonal crystal structure, and the second AlTi compound has a cubic crystal structure,

[0058] the third AlTi compound has a cubic crystal structure, and the fourth AlTi compound has a cubic crystal structure,

[0059] x1 is more than or equal to 0.9 and less than or equal to 0.95,

[0060] x2 is more than or equal to 0.5 and less than or equal to 0.6,

[0061] x3 is more than or equal to 0.75 and less than or equal to 0.85, and

[0062] x4 is more than or equal to 0.5 and less than or equal to 0.6.

[0063] The surface-coated cutting tool (hereinafter, also simply referred to as "cutting tool") of the present embodiment includes the substrate and the coating film that coats the substrate. Examples of the cutting tool can include a drill, an end mill, an indexable cutting insert for drill, an indexable cutting insert for end mill, an indexable cutting insert for milling, an indexable cutting insert for turning, a metal saw, a gear cutting tool, a reamer, a tap, and the like.

[0064] <Substrate>

[0065] For the substrate of the present embodiment, any conventionally known substrate can be used. For example, the substrate preferably includes at least one selected from a group consisting of: a cemented carbide (for example, a tungsten carbide (WC) based cemented carbide, a cemented carbide including Co in addition to WC, or a cemented carbide having a carbonitride of Cr, Ti, Ta, and Nb, or the like added therein in addition to WC); a cermet (including TiC, TiN, TiCN, or the like as a main component); a high-speed steel; a ceramic (titanium carbide, silicon carbide, silicon nitride, aluminum nitride, aluminum oxide, or the like); a cubic boron nitride sintered material (cBN sintered material); and a diamond sintered material. The substrate more preferably includes at least one selected from a group consisting of the cemented carbide, the cermet, and the cBN sintered material.

[0066] Among these various substrates, it is particularly preferable to select the WC based cemented carbide or the cBN sintered material. This is due to the following reason: each of these substrates is excellent in balance between hardness and strength particularly at a high temperature, and has an excellent characteristic as a substrate of a surface-coated cutting tool for the above-described purpose of use.

[0067] When the cemented carbide is used as the substrate, the effects of the present embodiment are achieved even if the cemented carbide includes free carbon or an abnormal phase called  $\eta$  phase in the structure thereof. It should be noted that the substrate used in the present embodiment may have a modified surface. For example, in the case of the cemented carbide, a  $\beta$ -free layer may be formed on the surface. In the case of the cBN sintered material, a surface hardening layer may be formed. Even when the surface is thus modified, the effects of the present embodiment are exhibited.

[0068] When the surface-coated cutting tool is an indexable cutting insert, a substrate having a chip breaker or a substrate having no chip breaker may be included. For the shape of a ridgeline portion of the cutting edge, any of the following shapes is included: a sharp edge (ridge at which a rake face and a flank face cross each other); a honing (shape obtained by providing a curvature to the sharp edge); a

negative land (chamfered shape), and a shape obtained by combining the honing and the negative land.

[0069] <Coating Film>

[0070] The coating film according to the present embodiment includes a hard coating layer constituted of a domain region and a matrix region. The "coating film" has a function of improving various characteristics in the cutting tool such as breakage resistance, wear resistance, and the like by coating at least a portion (for example, a portion to be brought into contact with a workpiece during cutting) of the substrate. The coating film preferably coats the entire surface of the substrate. However, a coating film that does not coat a portion of the substrate and a coating film having a partially different configuration are not deviated from the scope of the present embodiment.

[0071] The thickness of the coating film is preferably more than or equal to 2  $\mu\text{m}$  and less than or equal to 20  $\mu\text{m}$ , and is more preferably more than or equal to 5  $\mu\text{m}$  and less than or equal to 15  $\mu\text{m}$ . Here, the thickness of the coating film refers to a total of respective thicknesses of layers included in the coating film. Examples of the "layers included in the coating film" include a hard coating layer, a foundation layer, an outermost layer, and the like, which are described below. The thickness of the coating film can be determined, for example, as follows a transmission electron microscope (TEM) is used to measure thicknesses at ten arbitrary points in a cross sectional sample parallel to the normal direction of the surface of the substrate, and the average value of the measured thicknesses at the ten points is determined. The same applies to respective measurements of thicknesses of the hard coating layer, the foundation layer, and the outermost layer, which are described below. Examples of the transmission electron microscope include JEM-2100F (trademark) provided by JEOL Ltd.

[0072] (Hard Coating Layer)

[0073] FIG. 1 is a schematic view of the hard coating layer included in the coating film of the surface-coated cutting tool according to the present embodiment. The hard coating layer is constituted of the above-described domain region (region a in FIG. 1) and the above-described matrix region (region b in FIG. 1 (region other than region a)). In FIG. 1, portions of domain region a appear to overlap with each other, however, domain region a includes portions between which matrix region b is interposed in the depth direction of the figure. Although the hard coating layer has a blow-described composition, an inevitable impurity may be included as long as the effects exhibited by the surface-coated cutting tool according to the present embodiment are not compromised. The content ratio of the inevitable impurity is preferably more than or equal to 0 mass % and less than or equal to 10 mass % relative to the total mass of the hard coating layer.

[0074] The hard coating layer may be provided directly on the substrate or may be provided on the substrate with another layer such as the foundation layer being interposed therebetween as long as the effects exhibited by the surface-coated cutting tool according to the present embodiment are not compromised. On the hard coating layer, another layer such as an outermost layer may be provided. Moreover, the hard coating layer may be the outermost layer (outermost surface layer) of the coating film.

[0075] The thickness of the hard coating layer is preferably more than or equal to 0.5  $\mu\text{m}$  and less than or equal to

15  $\mu\text{m}$ , and is more preferably more than or equal to 3  $\mu\text{m}$  and less than or equal to 13  $\mu\text{m}$ .

**[0076]** (Domain Region)

**[0077]** The term “domain region” in the present embodiment refers to a region (for example, region a in FIG. 1) having a plurality of portions divided and distributed in the below-described matrix region. Moreover, it can be also understood that the domain region is a region divided into a plurality of regions in the hard coating layer. It should be noted that the “distributed” state above does not exclude a state in which regions of the domain region are in contact with each other. The domain region has a structure in which a first layer and a second layer are alternately layered on each other, the first layer being composed of at least one first AlTi compound selected from a group consisting of  $\text{Al}_{x_1}\text{Ti}_{(1-x_1)}\text{N}$ ,  $\text{Al}_{x_1}\text{Ti}_{(1-x_1)}\text{BN}$ , and  $\text{Al}_{x_1}\text{Ti}_{(1-x_1)}\text{CN}$ , the second layer being composed of at least one second AlTi compound selected from a group consisting of  $\text{Al}_{x_2}\text{Ti}_{(1-x_2)}\text{N}$ ,  $\text{Al}_{x_2}\text{Ti}_{(1-x_2)}\text{BN}$ , and  $\text{Al}_{x_2}\text{Ti}_{(1-x_2)}\text{CN}$ . Here,  $x_1$  represents an atomic ratio of Al in the first layer and  $x_2$  represents an atomic ratio of Al in the second layer. The first AlTi compound is preferably  $\text{Al}_{x_1}\text{Ti}_{(1-x_1)}\text{N}$ . Moreover, the second AlTi compound is preferably  $\text{Al}_{x_2}\text{Ti}_{(1-x_2)}\text{N}$ .

**[0078]** FIG. 2 shows an exemplary enlarged photograph of region a. A multilayer structure may be formed in which one or more first layers (dark layers in FIG. 2) and one or more second layers (bright layers in FIG. 2) are layered alternately on each other. In the present embodiment, the domain region may have a portion including such a multilayer structure. Alternatively, the domain region may be constituted of such a multilayer structure.

**[0079]** The domain region can be clearly distinguished from the below-described matrix region by way of observation with a TEM and a selected area electron diffraction image analysis.

**[0080]** Although the volume ratio of the domain region is not particularly limited, the volume ratio of the domain region may be more than or equal to 10 volume % and less than or equal to 90 volume %, may be more than or equal to 20 volume % and less than or equal to 80 volume %, or may be more than or equal to 50 volume % and less than or equal to 80 volume % with respect to the total volume of the domain region and the matrix region. The volume ratio of the domain region is determined by performing X-ray diffraction measurement (XRD measurement) and Rietveld analysis. For example, when the surface-coated cutting tool is an indexable cutting insert, the XRD measurement is performed in accordance with conditions described in Table 10 below. On this occasion, each of regions to be measured is preferably a flat region within 2 mm from a ridgeline of the indexable cutting insert. It is preferable to select two regions to be measured, and perform measurement twice or more for each region. Then, the obtained data is subjected to the Rietveld analysis, thereby determining the volume ratio of the domain region.

**[0081]** The thickness of the first layer is preferably more than or equal to 2 nm and less than or equal to 20 nm, and is more preferably more than or equal to 4 nm and less than or equal to 14 nm. The thickness of the second layer is preferably more than or equal to 0.5 nm and less than or equal to 5 nm, and is more preferably more than or equal to 1 nm and less than or equal to 4 nm. Moreover, when the domain region includes the above-described multilayer structure, the thickness of the first layer means the average

value of the respective thicknesses of the first layers at ten arbitrary locations in the multilayer structure. The same applies to the thickness of the second layer.

**[0082]** The total thickness of the thickness of the first layer and the thickness of the second layer (total of the respective thicknesses of one first layer and one second layer) is preferably more than or equal to 2 nm and less than or equal to 25 nm, is more preferably more than or equal to 2.5 nm and less than or equal to 25 nm, and is further preferably more than or equal to 5 nm and less than or equal to 20 nm.

**[0083]**  $x_1$  in the first AlTi compound is more than or equal to 0.9 and less than or equal to 0.95, and is preferably more than or equal to 0.91 and less than or equal to 0.94,  $x_1$  can be determined by using an energy dispersive X-ray spectroscopy (EDX) apparatus accompanied with a scanning electron microscope (SEM) or TEM to analyze crystal grains in the first layer appearing in the above-described cross sectional sample. Specifically, the values of  $x_1$  are measured and determined at arbitrary ten points in the first layer of the domain region of the cross sectional sample, and the average value of the determined values at the ten points is regarded as  $x_1$  in the first layer. Here, the “ten arbitrary points” are selected from different crystal grains in the first layer. Moreover, when the domain region includes the above-described multilayer structure,  $x_1$  means the average value of the respective values of  $x_1$  in the first layers at ten arbitrary locations in the multilayer structure. The same applies to below-described cases of  $x_2$ ,  $x_3$  and  $x_4$ . Examples of the above-described EDX apparatus include JED-2300 (trademark) provided by JEOL Ltd.

**[0084]**  $x_2$  in the second AlTi compound is more than or equal to 0.5 and less than or equal to 0.6, and is preferably more than or equal to 0.53 and less than or equal to 0.58,  $x_2$  can be determined by using an EDX apparatus accompanied with a SEM or TEM to analyze crystal grains in the second layer appearing in the above-described cross sectional sample. Specifically,  $x_2$  is determined by the same method as the above-described method for determining  $x_1$ .

**[0085]** The first AlTi compound included in the first layer includes a hexagonal crystal structure. The inclusion of the hexagonal crystal structure in the first AlTi compound can be confirmed by analyzing a pattern of an electron diffraction image obtained by performing selected area electron diffraction (SAED) measurement to the first layer of the cross sectional sample. Specifically, the electron diffraction measurement is performed to crystal grains of the first AlTi compound in the first layer. On this occasion, the number of crystal grains to be measured is at least more than or equal to 10 and is more preferably more than or equal to 20. Moreover, when the domain region includes the multilayer structure, for the electron diffraction measurement, the above-described method is preferably performed to the first layers at the arbitrary ten locations. The same applies to the second layer, the third layer, and the fourth layer, which are described below. Material crystal structure parameters required for the pattern analysis of the electron diffraction image are obtained from International Centre for Diffraction Data (ICDD), for example. The analysis can be performed using the crystal structure parameters and electron diffraction graphic simulation software (such as ReciPro). Examples of an apparatus used for the electron diffraction measurement includes “JEM-2100F” (trademark) provided by JEOL Ltd.

**[0086]** The second AlTi compound included in the second layer includes a cubic crystal structure. The inclusion of the cubic crystal structure in the second AlTi compound can be confirmed by performing a pattern analysis of an electron diffraction image obtained by performing electron diffraction measurement (SAED measurement) to the second layer of the cross sectional sample. Specific conditions for the electron diffraction measurement and the pattern analysis of the electron diffraction image are the same as those described above.

**[0087]** In the present embodiment, the first AlTi compound includes the hexagonal crystal structure, and the second AlTi compound includes the cubic crystal structure. With this, the surface-coated cutting tool becomes excellent in toughness and oxidation resistance. The first AlTi compound is preferably constituted of the hexagonal crystal structure, and the second AlTi compound is preferably constituted of the cubic crystal structure.

**[0088]** In one form of the present embodiment, the domain region preferably includes a twin crystal portion. Here, the “twin crystal portion” means a structure including a portion at which two single crystals of the domain region are gathered and joined in a certain direction. For example, region a shown in FIG. 2 corresponds to the twin crystal portion. Whether the twin crystal portion is included or not can be determined by observing the domain region using a transmission electron microscope.

**[0089]** (Matrix Region)

**[0090]** In the present embodiment, the “matrix region” refers to a region (for example, region b in FIG. 1) serving as a matrix of the coating film and other than the domain region. In other words, it can be also understood that most portions of the matrix region are regions disposed to surround the plurality of regions included in the domain region. Moreover, it can be also understood that most portions of the matrix region are disposed between the plurality of regions of the domain region. The matrix region has a structure in which a third layer and a fourth layer are layered on each other, the third layer being composed of at least one third AlTi compound selected from a group consisting of  $Al_{x3}Ti_{(1-x3)}N$ ,  $Al_{x3}Ti_{(1-x3)}BN$ , and  $Al_{x3}Ti_{(1-x3)}CN$ , the fourth layer being composed of at least one fourth AlTi compound selected from a group consisting of  $Al_{x4}Ti_{(1-x4)}N$ ,  $Al_{x4}Ti_{(1-x4)}BN$ , and  $Al_{x4}Ti_{(1-x4)}CN$ . Here,  $x3$  represents an atomic ratio of Al in the third layer and  $x4$  represents an atomic ratio of Al in the fourth layer. The third AlTi compound is preferably an  $Al_{x3}Ti_{(1-x3)}N$ . Moreover, the fourth AlTi compound is preferably  $Al_{x4}Ti_{(1-x4)}N$ .

**[0091]** FIG. 3 shows an exemplary enlarged photograph of region b. A multilayer structure may be formed in which one or more third layers (dark layers in region b in FIG. 3) and one or more fourth layers (bright layers in region b in FIG. 3) are layered alternately on each other. In the present embodiment, the matrix region may have a portion including such a multilayer structure. Alternatively, the matrix region may be constituted of such a multilayer structure.

**[0092]** The matrix region can be clearly distinguished from the above-described domain region by way of observation with a TEM and a selected area electron diffraction image analysis.

**[0093]** Although the volume ratio of the matrix region is not particularly limited, the volume ratio of the matrix region may be more than or equal to 10 volume % and less than or equal to 90 volume %, may be more than or equal

to 20 volume % and less than or equal to 80 volume %, or may be more than or equal to 50 volume % and less than or equal to 80 volume % with respect to the total volume of the domain region and the matrix region. The volume ratio of the matrix region is determined by performing X-ray diffraction measurement (XRD measurement) and Rietveld analysis. Specifically, the volume ratio of the matrix region can be determined by the same method as the above-described method for determining the volume ratio of the domain region.

**[0094]** The thickness of the third layer is preferably more than or equal to 1 nm and less than or equal to 20 nm, and is more preferably more than or equal to 2 nm and less than or equal to 10 nm. The thickness of the fourth layer is preferably more than or equal to 0.5 nm and less than or equal to 10 nm, and is more preferably more than or equal to 1 nm and less than or equal to 2 nm. Moreover, when the matrix region includes the above-described multilayer structure, the thickness of the third layer means the average value of the respective thicknesses of the third layers at ten arbitrary locations in the multilayer structure. The same applies to the thickness of the fourth layer.

**[0095]** The total thickness of the thickness of the third layer and the thickness of the fourth layer (total of the respective thicknesses of one third layer and one fourth layer) is preferably more than or equal to 1.5 nm and less than or equal to 30 nm, and is more preferably more than or equal to 3 nm and less than or equal to 10 nm.

**[0096]**  $x3$  in the third AlTi compound is more than or equal to 0.75 and less than or equal to 0.85, and is preferably more than or equal to 0.76 and less than or equal to 0.82,  $x3$  can be determined by using an EDX apparatus accompanied with a SEM or TEM to analyze crystal grains in the third layer appearing in the above-described cross sectional sample. Specifically,  $x3$  is determined by the same method as the method for determining  $x1$ .

**[0097]**  $x4$  in the fourth AlTi compound is more than or equal to 0.5 and less than or equal to 0.6, and is preferably more than or equal to 0.52 and less than or equal to 0.56,  $x4$  can be determined by using an EDX apparatus accompanied with a SEM or TEM to analyze crystal grains in the fourth layer appearing in the above-described cross sectional sample. Specifically,  $x4$  is determined by the same method as the method for determining  $x1$ .

**[0098]** The third AlTi compound included in the third layer includes a cubic crystal structure. The inclusion of the cubic crystal structure in the third AlTi compound can be confirmed by performing a pattern analysis of an electron diffraction image obtained by performing electron diffraction measurement (SAED measurement) to the third layer of the cross sectional sample. Specific conditions for the SAED measurement and the pattern analysis of the electron diffraction image are the same as those described above.

**[0099]** The fourth AlTi compound included in the fourth layer includes a cubic crystal structure. The inclusion of the cubic crystal structure in the fourth AlTi compound can be confirmed by performing a pattern analysis of an electron diffraction image obtained by performing electron diffraction measurement (SAED measurement) to the fourth layer of the cross sectional sample. Specific conditions for the SAED measurement and the pattern analysis of the electron diffraction are the same as those described above.

**[0100]** In the present embodiment, the third AlTi compound includes the cubic crystal structure, and the fourth



AlTi compound includes the cubic crystal structure. With this, the surface-coated cutting tool becomes excellent in deformation resistance. Preferably, the third AlTi compound is constituted of the cubic crystal structure, and the fourth AlTi compound is constituted of the cubic crystal structure.

**[0101]** (Other Layer(s))

**[0102]** As long as the effects of the present embodiment are not compromised, the coating film may further include other layer(s). The other layer(s) may each have a composition different from or the same as the composition of the hard coating layer. Examples of the other layer(s) include a TiN layer, a TiCN layer, a TiBN layer, an Al<sub>2</sub>O<sub>3</sub> layer, and the like. It should be noted that an order of layering these layers is particularly not limited. Examples of the other layer(s) includes: a foundation layer provided between the substrate and the hard coating layer; an outermost layer provided on the hard coating layer; and the like. The thickness of each of the other layer(s) is not particularly limited as long as the effects of the present embodiment are not compromised. For example, the thickness of each of the other layer(s) is more than or equal to 0.1 μm and less than or equal to 2 μm.

**[0103]** <<Method for Manufacturing Surface-Coated Cutting Tool>>

**[0104]** A method for manufacturing a surface-coated cutting tool according to the present embodiment is a method for manufacturing a surface-coated cutting tool including a substrate and a coating film that coats the substrate, and includes:

**[0105]** preparing the substrate; and

**[0106]** emitting first gas, second gas, and third gas to the substrate in an atmosphere at more than or equal to 650° C. and less than or equal to 900° C. and under more than or equal to 0.5 kPa and less than or equal to 5 kPa, the first gas including aluminum halide gas and titanium halide gas, the second gas including aluminum halide gas, titanium halide gas, and ammonia gas, the third gas including ammonia gas.

**[0107]** <Step of Preparing Substrate>

**[0108]** In this step, the substrate is prepared. As the substrate, any conventionally known substrate for such a purpose of use can be used as described above. For example, when the substrate is composed of cemented carbide, the substrate composed of cemented carbide can be obtained in the following manner: source material powders in a predetermined blending composition (mass %) are mixed uniformly using a commercially available attritor, and then the mixed powders are pressed and molded into a predetermined shape (for example, SEET13T3AGSN, CNMG120408NWX, or the like) and are then sintered in a predetermined sintering furnace at 1300° C. to 1500° C. for 1 to 2 hours. Moreover, a commercially available product may be used for the substrate without modification. Examples of the commercially available product include EH520 (trademark) provided by Sumitomo Electric Industries HardMetal.

**[0109]** <Step of Emitting First Gas, Second Gas, and Third Gas to Substrate>

**[0110]** In this step, the first gas, the second gas, and the third gas are emitted to the substrate in an atmosphere at more than or equal to 650° C. and less than or equal to 900° C. and under more than or equal to 0.5 kPa and less than or equal to 5 kPa, the first gas including aluminum halide gas and titanium halide gas, the second gas including aluminum halide gas, titanium halide gas, and ammonia gas, the third

gas including ammonia gas. This step can be performed using a CVD apparatus described below, for example.

**[0111]** (CVD Apparatus)

**[0112]** FIG. 4 is a schematic cross sectional view of an exemplary CVD apparatus used to manufacture the cutting tool according to the embodiment. As shown in FIG. 4, CVD apparatus 10 includes: a plurality of substrate setting jigs 12 for placing substrates 11; and a reaction container 13 that is composed of a heat-resistant alloy steel and that covers substrate setting jigs 12. Moreover, a temperature adjusting apparatus 14 for controlling a temperature in reaction container 13 is provided to surround reaction container 13.

**[0113]** In reaction container 13, a gas inlet pipe 18 is provided to extend in an inner space of reaction container 13 in the vertical direction and to be rotatable with respect to its axis in the vertical direction. Gas inlet pipe 18 has a first gas inlet pipe 15, a second gas inlet pipe 16, and a third gas inlet pipe 17, which are adjacent to and joined to one another. Gas inlet pipe 18 is configured to avoid the first gas introduced into first gas inlet pipe 15, the second gas introduced into second gas inlet pipe 16, and the third gas introduced into third gas inlet pipe 17 from being mixed with one another in gas inlet pipe 18. Moreover, first gas inlet pipe 15, second gas inlet pipe 16, and third gas inlet pipe 17 have respective portions provided with a plurality of through holes for emitting, to substrates 11 placed on substrate setting jigs 12, the gases flowing in first gas inlet pipe 15, second gas inlet pipe 16, and third gas inlet pipe 17.

**[0114]** Further, reaction container 13 is provided with a gas exhaust pipe 19 for exhausting the gas inside reaction container 13 to outside. The gas inside reaction container 13 passes through gas exhaust pipe 19 and is exhausted to the outside of reaction container 13 via a gas outlet 20.

**[0115]** More specifically, the first gas, the second gas, and the third gas are introduced into first gas inlet pipe 15, second gas inlet pipe 16, and third gas inlet pipe 17, respectively. On this occasion, the temperatures of the first gas, the second gas, and the third gas in the respective gas inlet pipes are not particularly limited as long as the first gas, the second gas, and the third gas are not liquefied at these temperatures. Next, the first gas, the second gas, and the third gas are repeatedly emitted in this order into reaction container 13 having an atmosphere at more than or equal to 650° C. and less than or equal to 900° C. (preferably, more than or equal to 700° C. and less than or equal to 750° C.) and under more than or equal to 0.5 kPa and less than or equal to 5 kPa (preferably, more than or equal to 2 kPa and less than or equal to 2.5 kPa). Since the plurality of through holes are provided in gas inlet pipe 18, the introduced first gas, second gas, and third gas are emitted from different through holes into reaction container 13. On this occasion, gas inlet pipe 18 is rotated at a rotating speed of, for example, 2 to 4 rpm with respect to its axis as indicated by a rotation arrow in FIG. 4. Accordingly, the first gas, the second gas, and the third gas can be repeatedly emitted to substrate 11 in this order.

**[0116]** (First Gas)

**[0117]** The first gas includes aluminum halide gas and titanium halide gas.

**[0118]** Examples of the aluminum halide gas include aluminum chloride gas (AlCl<sub>3</sub> gas or Al<sub>2</sub>Cl<sub>6</sub> gas), and the like. Preferably, AlCl<sub>3</sub> gas is used. The concentration (volume %) of the aluminum halide gas is preferably more than or equal to 0.3 volume % and less than or equal to 1.5 volume % and

is more preferably more than or equal to 0.6 volume % and less than or equal to 0.8 volume % relative to the total volume of the first gas.

**[0119]** Examples of the titanium halide gas include titanium(IV) chloride gas ( $\text{TiCl}_4$  gas), titanium(III) chloride gas ( $\text{TiCl}_3$  gas), and the like. Preferably, titanium(IV) chloride gas is used. The concentration (volume %) of the titanium halide gas is preferably more than or equal to 0.1 volume % and less than or equal to 1.0 volume % and is more preferably more than or equal to 0.2 volume % and less than or equal to 0.4 volume % relative to the total volume of the first gas.

**[0120]** A molar ratio of the aluminum halide gas in the first gas is preferably more than or equal to 0.5 and less than or equal to 0.85 and is more preferably more than or equal to 0.6 and less than or equal to 0.8 relative to the total number of moles of the aluminum halide gas and the titanium halide gas. The present inventors consider that when the molar ratio falls within the above-described range, the third layer and the fourth layer are formed through nucleation-growth decomposition.

**[0121]** The first gas may include hydrogen gas, or may include an inert gas such as argon gas. The concentration (volume %) of the inert gas is preferably more than or equal to 5 volume % and less than or equal to 50 volume % and is more preferably more than or equal to 20 volume % and less than or equal to 40 volume % relative to the total volume of the first gas. The hydrogen gas is normally a remainder of the first gas.

**[0122]** The first gas is preferably emitted to the substrate at a flow rate of 20 to 40 L/min.

**[0123]** (Second Gas)

**[0124]** The second gas includes aluminum halide gas, titanium halide gas, and ammonia gas. For the aluminum halide gas and the titanium halide gas, gases illustrated in the above section "(First Gas)" can be used. On this occasion, the aluminum halide gas and the titanium halide gas used for the first gas may be the same as or different from the aluminum halide gas and the titanium halide gas used for the second gas, respectively.

**[0125]** The concentration (volume %) of the aluminum halide gas is preferably more than or equal to 4 volume % and less than or equal to 5 volume % and is more preferably more than or equal to 4.3 volume % and less than or equal to 4.8 volume % relative to the total volume of the second gas.

**[0126]** The concentration (volume %) of the titanium halide gas is preferably more than or equal to 0.1 volume % and less than or equal to 1 volume % and is more preferably more than or equal to 0.3 volume % and less than or equal to 0.8 volume % relative to the total volume of the second gas.

**[0127]** A molar ratio of the aluminum halide gas in the second gas is preferably more than or equal to 0.82 and less than or equal to 0.98 and is more preferably more than or equal to 0.85 and less than or equal to 0.95 relative to the total number of moles of the aluminum halide gas and the titanium halide gas. The present inventors consider that when the molar ratio falls within the above-described range, the first layer and the second layer are formed through spinodal decomposition.

**[0128]** The concentration (volume %) of the ammonia gas is preferably more than or equal to 5 volume % and less than or equal to 25 volume % and is more preferably more than

or equal to 10 volume % and less than or equal to 20 volume % relative to the total volume of the second gas.

**[0129]** The second gas may include hydrogen gas, or may include an inert gas such as argon gas. The concentration (volume %) of the inert gas is preferably more than or equal to 5 volume % and less than or equal to 50 volume % and is more preferably more than or equal to 15 volume % and less than or equal to 20 volume % relative to the total volume of the second gas. The hydrogen gas is normally a remainder of the second gas.

**[0130]** The second gas is preferably emitted to the substrate at a flow rate of 20 to 40 L/min.

**[0131]** (Third Gas)

**[0132]** The third gas includes ammonia gas. Moreover, the third gas may include hydrogen gas, or may include an inert gas such as argon gas. By emitting the third gas to the substrate, the formation of the matrix region is promoted.

**[0133]** The concentration (volume %) of the ammonia gas is preferably more than or equal to 3 volume % and less than or equal to 30 volume % and is more preferably more than or equal to 10 volume % and less than or equal to 20 volume % relative to the total volume of the third gas. The hydrogen gas is normally a remainder of the third gas.

**[0134]** The third gas is preferably emitted to the substrate at a flow rate of 10 to 20 L/min.

**[0135]** <Other Step(s)>

**[0136]** In the manufacturing method according to the present embodiment, in addition to the steps described above, a step of forming the other layer(s), a step of performing surface treatment, and/or the like may be performed appropriately. When the above-described other layer(s) are formed, the other layer(s) may be formed by a conventional method.

### Examples

**[0137]** While the present disclosure will be described in more detail hereinafter with reference to Examples, the present disclosure is not limited thereto.

**[0138]** <<Production of Cutting Tool>>

**[0139]** <Preparation of Substrate>

**[0140]** First, as substrates on which coating films were to be formed, substrates K and substrates L shown in Table 1 below were prepared (the step of preparing the substrate). Specifically, first, source material powders in a blending composition (mass %) described in Table 1 were mixed uniformly. The expression "Remainder" in Table 1 indicates that WC is a remainder of the blending composition (mass %).

TABLE 1

Type	Blending Composition (Mass %)		
	Co	$\text{Cr}_3\text{C}_2$	WC
Substrate K	7.0	0.3	Remainder
Substrate L	12.0	0.5	Remainder

[0141] Next, the mixed powders were pressed and molded into a predetermined shape and were then sintered at 1300 to 1500° C. for 1 to 2 hours, thereby obtaining substrates K each composed of cemented carbide (substrate shape (JIS): CNMG120408-EX) and substrates L each composed of cemented carbide (substrate shape (JIS): SEET13T3AGSN-G).

[0142] It should be noted that CNMG120408-EX represents a shape of an indexable cutting insert for turning, and SEET13T3AGSN-G is a shape of an indexable cutting insert for milling.

[0143] <Production of Coating Film>

[0144] By forming the foundation layer, the hard coating layer, and the outermost layer shown in Table 11 on a surface of substrate K or substrate L, a coating film was produced on the surface of substrate K or substrate L. The following describes a method for producing each layer included in the coating film.

[0145] (Production of Hard Coating Layer)

[0146] Under film formation conditions described in Table 2, first gas, second gas, and third gas, which have compositions described in Tables 3 to 5, were repeatedly emitted to the surface of each substrate K or L in this order, thereby producing a hard coating layer (the step of emitting the first gas, the second gas, and the third gas to the substrate). It should be noted that when the foundation layer was provided on the surface of the substrate, the hard coating film was provided on a surface of the foundation layer.

[0147] For example, a hard coating layer indicated by an identification sign [1] of Table 6 was produced by repeatedly emitting the first gas, the second gas and the third gas to the surface of the substrate in this order under film formation conditions (identification sign A of Table 2) involving a temperature of 750° C., a pressure of 2.5 kPa, and a gas inlet pipe rotating speed of 2 rpm, the first gas being indicated by an identification sign 1-c in Table 3 (0.7 volume % of AlCl<sub>3</sub>, 0.3 volume % of TiCl<sub>4</sub>, 20 volume % of Ar, and a remainder of H<sub>2</sub>; gas flow rate of 20 L/min), the second gas being indicated by an identification sign 2-c in Table 4 (4.5 volume % of AlCl<sub>3</sub>, 0.5 volume % of TiCl<sub>4</sub>, 10 volume % of NH<sub>3</sub>, 17 volume % of Ar and a remainder of H<sub>2</sub>; gas flow rate of 40 L/min), the third gas being indicated by an identification sign 3-a in Table 5 (10 volume % of NH<sub>3</sub> and a remainder of H<sub>2</sub>; gas flow rate of 10 L/min). The composition and the like of the produced hard coating layer are shown in Table 6. The expression “None” in Table 6 indicates that since a corresponding gas was not emitted, no domain region or no matrix region was formed.

TABLE 2

Film Formation Conditions			
	Identification Sign		
	A	B	C
Temperature (° C.)	750	770	770
Pressure (kPa)	2.5	3.0	3.0
Rotating Speed (rpm)	2	2	4

TABLE 3

Composition of First Gas				
	Identification Sign			
	1-b	1-c	1-d	1-e
AlCl <sub>3</sub> (vol %)	0.6	0.7	0.8	0.6
TiCl <sub>4</sub> (vol %)	0.4	0.3	0.2	0.4
AlCl <sub>3</sub> /(AlCl <sub>3</sub> + TiCl <sub>4</sub> ) (Molar Ratio)	0.6	0.7	0.8	0.6
Ar (vol %)	30	20	40	30
H <sub>2</sub> (vol %)	Remainder	Remainder	Remainder	Remainder
Gas Flow Rate (L/min)	20	20	20	30

TABLE 4

Composition of Second Gas				
	Identification Sign			
	2-b	2-c	2-d	2-e
AlCl <sub>3</sub> (vol %)	4.3	4.5	4.8	4.3
TiCl <sub>4</sub> (vol %)	0.8	0.5	0.3	0.8
AlCl <sub>3</sub> /(AlCl <sub>3</sub> + TiCl <sub>4</sub> ) (Molar Ratio)	0.85	0.90	0.95	0.85
NH <sub>3</sub> (vol %)	10	10	10	10
Ar (vol %)	15	17	20	15
H <sub>2</sub> (vol %)	Remainder	Remainder	Remainder	Remainder
Gas Flow Rate (L/min)	40	40	40	30

TABLE 5

Composition of Third Gas		
	Identification Sign	
	3-a	3-b
NH <sub>3</sub> (vol %)	10	2
H <sub>2</sub> (vol %)	Remainder	Remainder
Gas Flow Rate (L/min)	10	10

TABLE 6

Iden- tifi- cation Sign					Martix Region				Domain Region				Total thick- ness (nm)	Film Hard- ness (GPa)	Film Young's Modulus (GPa)	
	Table	Table	Table	Table	Third Layer o-AlTiN		Fourth Layer o-AlTiN		First Layer		Second Layer					
	2	3	4	5	Com- Thick- ness (nm)	posi- tion of Al x3	Com- Thick- ness (nm)	posi- tion of Al x4	h-AlTiN Thick- ness (nm)	Composi- tion of Al x1	o-AlTiN Thick- ness (nm)	Composi- tion of Al x2				
[1]	A	1-c	2-c	3-a	2.3	0.76	1.5	0.54	3.8	9.7	0.92	1.9	0.52	11.6	33	579
[2]	B	1-c	2-c	3-a	2.0	0.81	1.2	0.56	3.2	8.2	0.91	1.5	0.53	9.7	38	667
[3]	C	1-c	2-0	3-a	2.5	0.82	1.8	0.52	4.3	10.9	0.93	2.2	0.58	13.1	35	614
[4]	A	1-0	2-c	3-b	2.7	0.78	1.9	0.56	4.6	11.4	0.94	2.7	0.51	14.1	32	561
[5]	A	1-b	2-c	3-a	2.2	0.75	1.6	0.52	3.8	9.6	0.92	2.0	0.52	11.6	34	596
[6]	A	1-d	2-c	3-a	2.5	0.80	1.3	0.57	3.8	9.8	0.92	1.8	0.52	11.6	32	563
[7]	A	1-c	2-b	3-a	9.3	0.76	1.5	0.54	3.8	0.8	0.93	2.5	0.55	12.3	34	602
[8]	A	1-c	2-d	3-a	2.3	0.76	1.5	0.54	3.8	9.6	0.90	1.1	0.50	10.7	32	566
[9]	A	1-e	2-e	3-a	3.0	0.80	1.1	0.53	4.1	6.2	0.90	1.2	0.58	7.4	33	569
[y]	A	1-c	None	3-a	2.4	0.77	1.6	0.52	4.0			None			31	525
[z]	A	None	2-c	None			None			10.5	0.91	1.8	0.51	12.3	29	509
[α]	A	1-e	2-d	3-b	3.2	0.7	2	0.65	5.2	10.5	0.94	1.5	0.5	12	28	530
[β]	A	1-d	2-d	3-b	2.4	0.89	1.7	0.51	4.1	11.9	0.96	3	0.4	14.9	29	535

**[0148]** (Production of Foundation Layer and Production of Outermost Layer)

**[0149]** Under film formation conditions described in Table 7, reactive gas having a composition described in Table 7 was emitted to the surface of the substrate in the case of the foundation layer and was emitted to the surface of the hard coating layer in the case of the outermost layer, thereby producing the foundation layer and the outermost layer.

TABLE 7

Type of Foundation		Film Formation Conditions		
Layer or Outermost Layer	Composition of Reactive Gas (vol %)	Pres- sure (kPa)	Temper- ature (° C.)	Gas Flow Rate (L/min)
TiN (Foundation Layer)	TiCl <sub>4</sub> = 2.0%, N <sub>2</sub> = 39.7%, H <sub>2</sub> = Remainder	6.7	915	63.8
TiN (Outermost Layer)	TiCl <sub>4</sub> = 0.5%, N <sub>2</sub> = 41.2%, H <sub>2</sub> = Remainder	79.8	780	45.9
TiCN	TiCl <sub>4</sub> = 2.0%, CH <sub>3</sub> CN = 0.7%, H <sub>2</sub> = Remainder	9	860	50.5
TiBN	TiCl <sub>4</sub> = 36.7%, BCl <sub>3</sub> = 0.1%, N <sub>2</sub> = 61.7%, H <sub>2</sub> = Remainder	6.7	800	80.3
Al <sub>2</sub> O <sub>3</sub>	AlCl <sub>3</sub> = 1.6%, CO <sub>2</sub> = 4.5%, H <sub>2</sub> S = 0.2%, NO <sub>2</sub> = 0.5%, H <sub>2</sub> = Remainder	6.7	850	46.2

**[0150]** <<Evaluation on Characteristics of Cutting Tool>>

**[0151]** By using cutting tools of the samples (sample 1 to sample 27) produced as described above, characteristics of each of the cutting tools were evaluated as described below.

**[0152]** <Measurement of Thicknesses of Coating Film and the Like>

**[0153]** The thickness of the coating film as well as the respective thicknesses of the foundation layer, the hard coating layer (the first layer, the second layer, the third layer, and the fourth layer), and the outermost layer included in the coating film were determined by using a transmission elec-

tron microscope (TEM) (trademark: JEM-2100F provided by JEOL Ltd.) to perform measurement at arbitrary ten points in a cross sectional sample parallel to the normal direction of the surface of the substrate and calculating the average value of the measured thicknesses at the ten points. Results are shown in Table 6 and Table 11. Here, the expression "Thickness" of the first layer in Table 6 means the average value of the respective thicknesses of the plurality of first layers included in the multilayer structure, the thicknesses of the plurality of first layers being determined by the above-described method. The same applies to the thicknesses of the second layer, the third layer, and the fourth layer. The expression "None" in the sections "Foundation Layer" and "Outermost Layer" indicates that the foundation layer and the outermost layer do not exist in the coating film. Moreover, the expression "[1](3.5)" or the like in the section "Hard Coating Layer" indicates that the hard coating layer has the configuration indicated by the identification sign [1] of Table 6 and has a total thickness of 3.5 μm. The expression "TiN(0.5)" in Table 11 indicates that the corresponding layer is a TiN layer having a thickness of 0.5 μm. Moreover, when two compounds are described in one section (for example, "TiN(0.5)-TiCN(0.5)" or the like), it is indicated that the compound (TiN(0.5)) at the left side is a layer located at a side close to the surface of the substrate and the compound (TiCN(1.5)) at the right side is a layer located at a side far from the surface of the substrate. Further, the expression "[Al<sub>2</sub>O<sub>3</sub>(0.2)-TiN(0.1)]x3" or the like means that three layers each represented by "Al<sub>2</sub>O<sub>3</sub>(0.2)-TiN(0.1)" are repeatedly layered. It should be noted that the order of layering the Al<sub>2</sub>O<sub>3</sub> layer and the TiN layer in the "Al<sub>2</sub>O<sub>3</sub>(0.2)-TiN(0.1)" is the same as that in the above description.

**[0154]** Moreover, as a result of observation of the hard coating layer using a TEM, it was found that the domain region had a multilayer structure in which the first layer and the second layer were layered alternately (for example, FIG. 2). Moreover, a twin crystal portion was observed in the domain region. Further, from a selected area electron diffraction image, it was found that the first layer of the domain

region had a hexagonal crystal structure, the second layer had a cubic crystal structure, and the Al composition in the first layer and the Al composition in the second layer were different in a <100> direction (FIG. 2; the upper right portion of the photograph). On the other hand, it was found that each of the third layer and the fourth layer of the matrix region had a cubic crystal structure and a multilayer structure was formed in which the third layer and the fourth layer were layered alternately (for example, FIG. 3).

**[0155]** <Measurement of Film Hardness and Film Young's Modulus>

**[0156]** The film hardness and film Young's modulus of the hard coating layer were measured under below-described conditions using a nano indenter (trademark: ENT1100a provided by Elionix). On this occasion, when measuring them in a sample in which the hard coating layer is not located on the outermost surface, the measurement was performed after the hard coating layer was exposed by mechanical polishing or the like. Moreover, the film hardnesses and film Young's moduli were measured and determined at arbitrary ten points in the hard coating layer, and the average value of the determined film hardnesses and film Young's moduli at the ten points were employed as the film hardness and the film Young's modulus in the hard coating layer. It should be noted that the film hardness and film Young's modulus of the hard coating layer was calculated from a curve of load and displacement based on the Oliver-Pharr theory. Results are shown in Table 6.

**[0157]** Measurement Conditions of Nano Indenter

**[0158]** Indenter material: Diamond

**[0159]** Indenter shape: Berkovich indenter

**[0160]** Test load: 30 mN

**[0161]** Step interval: 20 msec

**[0162]** Holding time: 1000 msec

**[0163]** The number of measurement points: 10 points

**[0164]** <Crystal Structures of Domain Region and Matrix Region>

**[0165]** The AlTiN crystal structures in the domain region (the first layer and the second layer) and the matrix region (the third layer and the fourth layer) were measured under conditions shown in Table 8 below by using a transmission electron microscope and an apparatus (trademark: JEM-2100F provided by JEOL Ltd.) for selected area electron diffraction measurement (TEM-SAED measurement). On this occasion, the number of crystal grains to be measured was at least 10 or more in a layer at one location. The measurement was performed for each of layers at ten arbitrary locations. As a result, it was found that each of the second layer of the domain region and the third layer and the fourth layer of the matrix region had a cubic crystal structure. Moreover, it was found that the first layer of the domain region had a hexagonal crystal structure. It should be noted that in the sections "Domain Region" and "Matrix Region" of Table 6, "h" in the expression "h-AlTiN" or the like indicates that the compound has a hexagonal crystal structure. Moreover, "c" in the expression "c-AlTiN" or the like indicates that the compound has a cubic crystal structure.

TEM Observation and Electron Diffraction Analysis Method	
Apparatus	JEM-2100F (Provided by JEOL Ltd.)
Acceleration Voltage	200 kV
Amount of Current	80 pA
Camera Length	1 m

-continued

TEM Observation and Electron Diffraction Analysis Method	
Apparatus	JEM-2100F (Provided by JEOL Ltd.)
Size of Selected Area	φ200 nm
Observation Magnification	5000x to 150000X

**[0166]** <Compositions of Domain Region and Matrix Region>

**[0167]** The respective compositions of the first layer, second layer, third layer, and fourth layer in the hard coating layer were measured under conditions of Table 9 below by using an EDX measurement apparatus (trademark: JED-2300 provided by JEOL Ltd.). For example, the values of x1 were determined by performing measurement at arbitrary ten points in the first layer of the domain region of the cross sectional sample, and the average value of the determined values at the ten points was regarded as x1 in the first layer. Here, the "ten arbitrary points" were selected from different crystal grains in the first layer. Moreover, when the domain region includes the above-described multilayer structure, x1 was represented by the average value of the respective values of x1 of the first layers at ten arbitrary locations in the multilayer structure. The same method was employed for the second layer, the third layer, and the fourth layer. Results are shown in Table 6.

**[0168]** EDX Measurement Conditions

TABLE 9	
EDX analysis method	
Apparatus	JED-2300 (provided by JEOL Ltd.)
Detector	Silicon Drift Detector
Analysis Software	Analysis station (provided by JEOL. Ltd.)
Analysis Spot Size	0.1 nm

**[0169]** <Volume Ratios of Domain Region and Matrix Region>

**[0170]** The respective volume ratios of the domain region and the matrix region were measured under conditions shown in Table 10 below with respect to the total volume of the domain region (the first layer and the second layer) and the matrix region (the third layer and the fourth layer) by using an X-ray diffraction measurement (XRD measurement) apparatus (trademark: SmartLab provided by Rigaku). On this occasion, when measuring them in a sample in which the hard coating layer is not located on the outermost surface, the measurement was performed after the hard coating layer was exposed by mechanical polishing or the like. Moreover, each of regions to be measured was a flat region within 2 mm from the cutting edge of the tool. Two regions to be measured were selected and measurement was performed twice or more for each region. As a result, it was found that each of the second layer of the domain region and the third layer and fourth layer of the matrix region had a cubic crystal structure. It was found that the first layer of the domain region had a hexagonal crystal structure. Moreover, the respective volume ratios of the domain region and the matrix region could be quantitatively estimated by way of the Rietveld analysis (analysis software name: PDXL pro-

vided by Rigaku). Specifically, in the hard coating layer corresponding to each of identification signs [1] to [8] in Table 6, the volume ratios of the domain region and the matrix region were 80 volume % and 20 volume %, respectively. Moreover, in the hard coating layer corresponding to the identification sign [9] in Table 6, the volume ratios of the domain region and the matrix region were 50 volume % and 50 volume %, respectively.

TABLE 10

XRD Measurement and Analysis Method	
Apparatus	SmartLab (provided by Rigaku)
X-ray Output	9 kW (Voltage: 40 kV, Current: 200 mA)
X-ray Target	Cu
X-ray Optical System	Concentrated Optical System
Incoming X-ray Parallel Slit	Soller_slit_5 deg
Incoming Slit Longitudinally Limited Slit	2/3 deg 2 mm

TABLE 10-continued

XRD Measurement and Analysis Method		
Apparatus	SmartLab (provided by Rigaku)	
Light Receiving Slit 1	20 mm	
Filter	Ni	
Light Receiving Parallel Slit	Soller_slit_5 deg	
Light Receiving Slit 2	20 mm	
Detector	Silicon Strip Detector (D/teX Ultra 250 provided by Rigaku)	
Measurement Conditions	Scanning Zone (2θ)	30 to 90 deg
	Scanning Rate	1 deg/min
Data Analysis	Analysis Software	PDXL Rietveld Analysis (provided by Rigaku)
	Material Crystal Structure Parameters Required for Data Analysis	Obtained from International Centre for Diffraction Data (ICDD)

TABLE 11

Configuration of Coating Film and Thickness of each Layer					
Sample Number	Substrate Type	Foundation Layer (μm)	Hard Coating		Total Thickness of Coating Film (μm)
			Layer (μm)	Outermost Layer (μm)	
Sample 1	K	TiN(0.5)	[1] (3.5)	None	4.0
Sample 2	K	TiN(0.5)	[2] (2.5)	Al <sub>2</sub> O <sub>3</sub> (1.0)	4.0
Sample 3	K	TiN(0.5)	[3] (2.6)	[Al <sub>2</sub> O <sub>3</sub> (0.2)—TiN(0.1)] × 3	4.0
Sample 4	K	None	[1] (6.0)	None	6.0
Sample 5	K	TiCN(2.0)	[4] (3.0)	Al <sub>2</sub> O <sub>3</sub> (1.0)	6.0
Sample 6	K	TiCN(2.0)	[5] (3.1)	[Al <sub>2</sub> O <sub>3</sub> (0.2)—TiN(0.1)] × 3	6.0
Sample 7	K	TiN(0.5)—TiCN(1.5)	[1] (4.0)	None	6.0
Sample 8	K	TiN(0.5)—TiCN(1.5)	[6] (3.0)	Al <sub>2</sub> O <sub>3</sub> (1.0)	6.0
Sample 9	K	TiN(0.5)—TiCN(1.5)	[7] (3.1)	[Al <sub>2</sub> O <sub>3</sub> (0.2)—TiN(0.1)] × 3	6.0
Sample 10	K	TiN(0.5)—TiCN(1.5)	[8] (9.0)	None	11.0
Sample 11	K	TiN(0.5)—TiCN(1.5)	[1] (7.0)	Al <sub>2</sub> O <sub>3</sub> (2.0)	11.0
Sample 12	K	TiN(0.5)—TiCN(1.5)	[1] (7.8)	[Al <sub>2</sub> O <sub>3</sub> (0.3)—TiN(0.1)] × 3	11.0
Sample 12'	K	TiN(0.5)	[9] (2.4)	Al <sub>2</sub> O <sub>3</sub> (1.0)	3.9
Sample 13	L	TiN(0.5)	[1] (3.5)	None	4.0
Sample 14	L	TiN(0.5)	[2] (2.5)	Al <sub>2</sub> O <sub>3</sub> (1.0)	4.0
Sample 15	L	TiN(0.5)	[3] (2.6)	[Al <sub>2</sub> O <sub>3</sub> (0.2)—TiN(0.1)] × 3	4.0
Sample 16	L	None	[1] (6.0)	None	6.0
Sample 17	L	TiCN(2.0)	[4] (3.0)	Al <sub>2</sub> O <sub>3</sub> (1.0)	6.0
Sample 18	L	TiCN(2.0)	[5] (3.1)	[Al <sub>2</sub> O <sub>3</sub> (0.2)—TiN(0.1)] × 3	6.0
Sample 19	L	TiN(0.5)—TiCN(1.5)	[1] (4.0)	None	6.0
Sample 20	L	TiN(0.5)—TiCN(1.5)	[6] (3.0)	Al <sub>2</sub> O <sub>3</sub> (1.0)	6.0
Sample 21	L	TiN(0.5)—TiCN(1.5)	[7] (3.1)	[Al <sub>2</sub> O <sub>3</sub> (0.2)—TiN(0.1)] × 3	6.0
Sample 21'	L	TiN(0.5)	[9] (2.4)	Al <sub>2</sub> O <sub>3</sub> (1.0)	3.9
Sample 22	K	None	[y] (6.0)	None	6.0
Sample 23	K	TiN(0.5)—TiCN(1.5)	[z] (4.0)	None	6.0
Sample 24	L	TiN(0.5)	[y] (3.5)	None	4.0
Sample 25	L	TiN(0.5)	[z] (2.5)	Al <sub>2</sub> O <sub>3</sub> (1.0)	4.0
Sample 26	K	TiN(0.5)	[1] (3.5)	None	4.0
Sample 27	L	TiN(0.5)	[1] (3.5)	None	4.0

[0171] <<Cutting Test>>

[0172] <Test 1: Turning Test>

[0173] Each of the cutting tools of the samples (sample 1 to sample 12', sample 22, sample 23, and sample 26) produced as described above was used to measure a cutting time until a flank face wear amount (Vb) reached 0.2 mm or breakage (chipping) occurred under below-described cutting conditions. Moreover, a type of final damage of the cutting edge thereof was observed. Results are shown in Table 12. As the cutting time is longer, the cutting tool can be evaluated to have more excellent wear resistance.

[0174] Cutting Conditions

[0175] Workpiece: Hastelloy 276

[0176] Speed: 50 m/min

[0177] Amount of cut (ap): 1.5 mm

TABLE 12

Sample Number	Cutting time (Minute)	Type of Final Damage
Sample 1	19	Normal Wear
Sample 2	21	Normal Wear
Sample 3	20	Normal Wear
Sample 4	24	Normal Wear
Sample 5	22	Normal Wear
Sample 6	25	Normal Wear
Sample 7	25	Normal Wear
Sample 8	23	Normal Wear
Sample 9	27	Normal Wear
Sample 10	28	Normal Wear
Sample 11	30	Normal Wear
Sample 12	29	Normal Wear
Sample 12'	20	Normal Wear
Sample 22	8	Breakage
Sample 23	5	Wear
Sample 26	11	Wear

[0178] <Test 2: Milling Test>

[0179] Each of the cutting tools of the samples (sample 13 to sample 21', sample 24, sample 25, and sample 27) produced as described above was used to measure a cutting distance until a flank face wear amount (Vb) reached 0.2 mm or breakage (chipping) occurred under below-described cutting conditions. Moreover, a type of final damage of the cutting edge thereof was observed. Results are shown in Table 13. As the cutting distance is longer, the cutting tool can be evaluated to have more excellent wear resistance.

[0180] Cutting Conditions

[0181] Workpiece: SUS304

[0182] Circumferential speed: 150 m/min

[0183] Amount of cut (ap): 2.0 mm

[0184] Width of cut (ae): 30 mm

TABLE 13

Sample Number	Cutting Distance (m)	Type of Final Damage
Sample 13	2.75	Normal Wear
Sample 14	3.25	Normal Wear
Sample 15	3.00	Normal Wear
Sample 16	4.25	Normal Wear
Sample 17	3.75	Normal Wear
Sample 18	4.50	Normal Wear
Sample 19	4.25	Normal Wear
Sample 20	4.00	Normal Wear
Sample 21	4.75	Normal Wear
Sample 21'	3.00	Normal Wear

TABLE 13-continued

Sample Number	Cutting Distance (m)	Type of Final Damage
Sample 24	1.75	Chipping
Sample 25	1.25	Wear
Sample 27	2.00	Wear

[0185] The cutting tools of samples 1 to 12' correspond to Examples and the cutting tools of sample 22, sample 23, and sample 26 correspond to Comparative Examples. In view of the results of Table 12, each of the cutting tools of samples 1 to 12' attained excellent results, i.e., the cutting time was more than or equal to 19 minutes. Moreover, the type of final damage of each of the cutting tools of samples 1 to 12' was normal wear. On the other hand, the cutting time of each of the cutting tools of sample 22, sample 23, and sample 26 was less than or equal to 8 minutes. The cutting tool of sample 22 was finally broken. The cutting tool of sample 23 was significantly worn and had a short tool life due to the wear. Sample 26 had a large wear amount. In view of the results of Test 1, it is considered that each of the cutting tools of samples 1 to 12' has improved strength at a high temperature and excellent thermal cracking resistance as compared with the cutting tools of sample 22, sample 23, and sample 26. That is, it was found that the cutting tools of samples 1 to 12' were excellent in breakage resistance, wear resistance and thermal cracking resistance.

[0186] The cutting tools of samples 13 to 21' correspond to Examples and the cutting tools of sample 24, sample 25, and sample 27 correspond to Comparative Examples. In view of the results of Table 13, each of the cutting tools of samples 13 to 21' attained excellent results, i.e., the cutting distance was more than or equal to 2.75 m. Moreover, the type of final damage of each of the cutting tools of samples 13 to 21' was normal wear. On the other hand, the cutting distances of the cutting tools of sample 24, sample 25, and sample 27 were 1.75 m, 1.25 m and 2.00 m. Moreover, chipping was observed in the cutting tool of sample 24. The cutting tool of sample 25 was significantly worn and had a short tool life due to the wear. Sample 27 had a large wear amount. In view of the results of Test 2, it was found that each of the cutting tools of samples 13 to 21' had more excellent breakage resistance and wear resistance as well as a longer tool life than those of the cutting tools of sample 24, sample 25, and sample 27.

[0187] Heretofore, the embodiments and examples of the present disclosure have been illustrated, but it has been initially expected to appropriately combine configurations of the embodiments and examples.

[0188] The embodiments and examples disclosed herein are illustrative and non-restrictive in any respect. The scope of the present invention is defined by the terms of the claims, rather than the embodiments and examples described above, and is intended to include any modifications within the scope and meaning equivalent to the terms of the claims.

REFERENCE SIGNS LIST

[0189] **10**: CVD apparatus; **11**, substrate; **12**: substrate setting jig; **13**: reaction container; **14**: temperature adjusting apparatus; **15**: first gas inlet pipe; **16**: second gas inlet pipe; **17**: third gas inlet pipe; **18**: gas inlet pipe; **19**: gas exhaust pipe; **20**: gas outlet; a: region a, domain region; b: region b, matrix region.

1. A surface-coated cutting tool comprising a substrate and a coating film that coats the substrate, wherein

the coating film includes a hard coating layer constituted of a domain region and a matrix region,

the domain region is a region having a plurality of portions divided and distributed in the matrix region,

the domain region has a structure in which a first layer and a second layer are layered on each other, the first layer being composed of at least one first AlTi compound selected from a group consisting of  $Al_{x1}Ti_{(1-x1)}N$ ,  $Al_{x1}Ti_{(1-x1)}BN$ , and  $Al_{x1}Ti_{(1-x1)}CN$ , the second layer being composed of at least one second AlTi compound selected from a group consisting of  $Al_{x2}Ti_{(1-x2)}N$ ,  $Al_{x2}Ti_{(1-x2)}BN$ , and  $Al_{x2}Ti_{(1-x2)}CN$ ,

the matrix region has a structure in which a third layer and a fourth layer are layered on each other, the third layer being composed of at least one third AlTi compound selected from a group consisting of  $Al_{x3}Ti_{(1-x3)}N$ ,  $Al_{x3}Ti_{(1-x3)}BN$ , and  $Al_{x3}Ti_{(1-x3)}CN$ , the fourth layer being composed of at least one fourth AlTi compound selected from a group consisting of  $Al_{x4}Ti_{(1-x4)}N$ ,  $Al_{x4}Ti_{(1-x4)}BN$ , and  $Al_{x4}Ti_{(1-x4)}CN$ ,

the first AlTi compound has a hexagonal crystal structure, and the second AlTi compound has a cubic crystal structure,

the third AlTi compound has a cubic crystal structure, and the fourth AlTi compound has a cubic crystal structure,

$x1$  is more than or equal to 0.9 and less than or equal to 0.95,

$x2$  is more than or equal to 0.5 and less than or equal to 0.6,

$x3$  is more than or equal to 0.75 and less than or equal to 0.85, and

$x4$  is more than or equal to 0.5 and less than or equal to 0.6.

2. The surface-coated cutting tool according to claim 1, wherein the domain region includes a twin crystal portion.

3. The surface-coated cutting tool according to claim 1, wherein a total thickness of a thickness of the first layer and a thickness of the second layer is more than or equal to 2 nm and less than or equal to 20 nm.

4. The surface-coated cutting tool according to claim 1, wherein a total thickness of a thickness of the third layer and a thickness of the fourth layer is more than or equal to 1.5 nm and less than or equal to 30 nm.

5. A method for manufacturing the surface-coated cutting tool recited in claim 1, the method comprising:

preparing the substrate; and

emitting each of first gas, second gas, and third gas to the substrate in an atmosphere at more than or equal to 650° C. and less than or equal to 900° C. and under more than or equal to 0.5 kPa and less than or equal to 5 kPa, the first gas including aluminum halide gas and titanium halide gas, the second gas including aluminum halide gas, titanium halide gas, and ammonia gas, the third gas including ammonia gas.

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