



(19) **United States**

(12) **Patent Application Publication**
Sharvit et al.

(10) **Pub. No.: US 2020/0381826 A1**

(43) **Pub. Date: Dec. 3, 2020**

(54) **HIGH-RESOLUTION PHASE SHIFTER**

(52) **U.S. Cl.**

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CPC **H01Q 3/36** (2013.01); **H01P 5/16** (2013.01); **H03F 3/245** (2013.01); **H03F 2200/294** (2013.01); **H03H 11/20** (2013.01)

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(57) **ABSTRACT**

(21) Appl. No.: **16/901,326**

(22) Filed: **Jun. 15, 2020**

Related U.S. Application Data

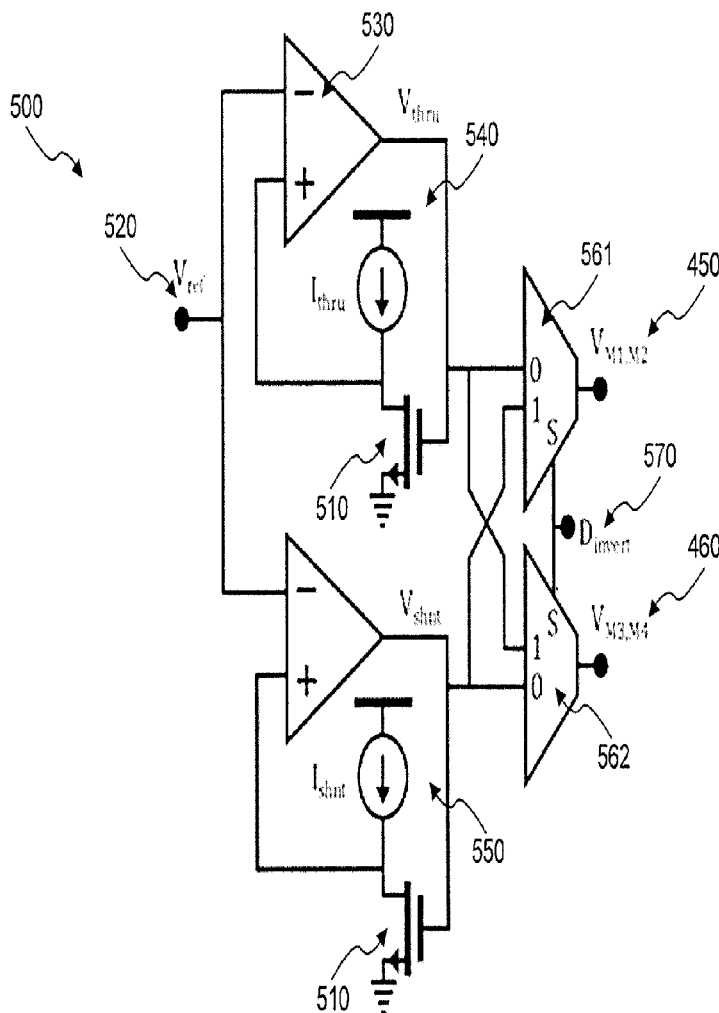
(63) Continuation of application No. 15/959,931, filed on Apr. 23, 2018, now Pat. No. 10,727,587.

(60) Provisional application No. 62/490,251, filed on Apr. 26, 2017.

Publication Classification

(51) **Int. Cl.**
H01Q 3/36 (2006.01)
H01P 5/16 (2006.01)
H03H 11/20 (2006.01)

A radiation pattern of a phased array antenna, comprising a plurality of antenna elements, may be dynamically modified using phase shifters to apply variable phase shifts between antenna elements. In a phased array antenna designed for airborne applications, the phase shifters may be required to enable a fine phase-shifting resolution and to operate over a wide temperature range. The phase shifters may also be required to perform while exhibiting small process variations, small form factor, low power consumption, and low loss. One possible solution to this is a passive vector-interpolating phase shifter configured to exhibit such characteristics.



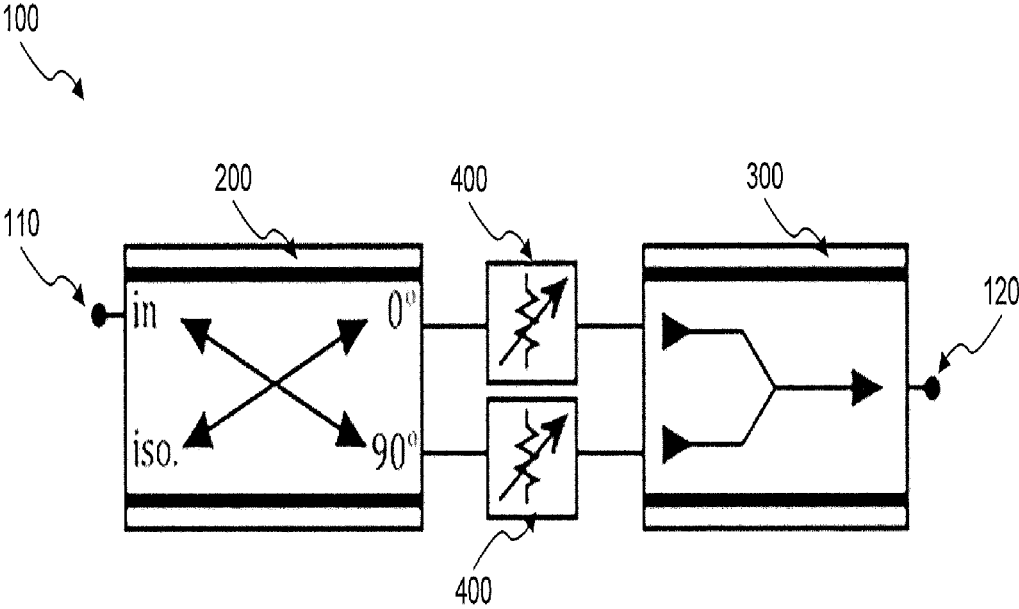


Fig. 1

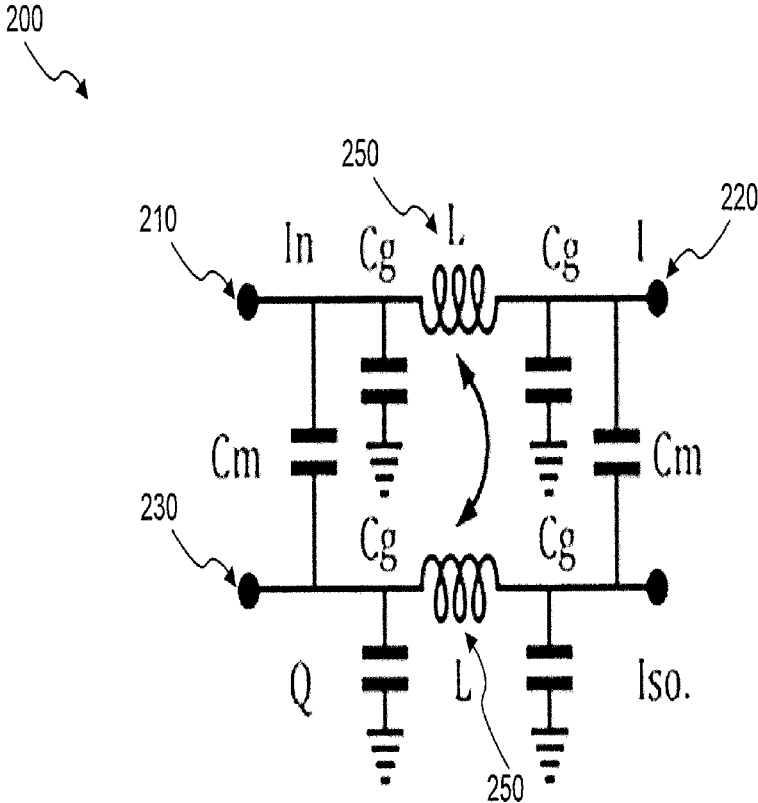


Fig. 2

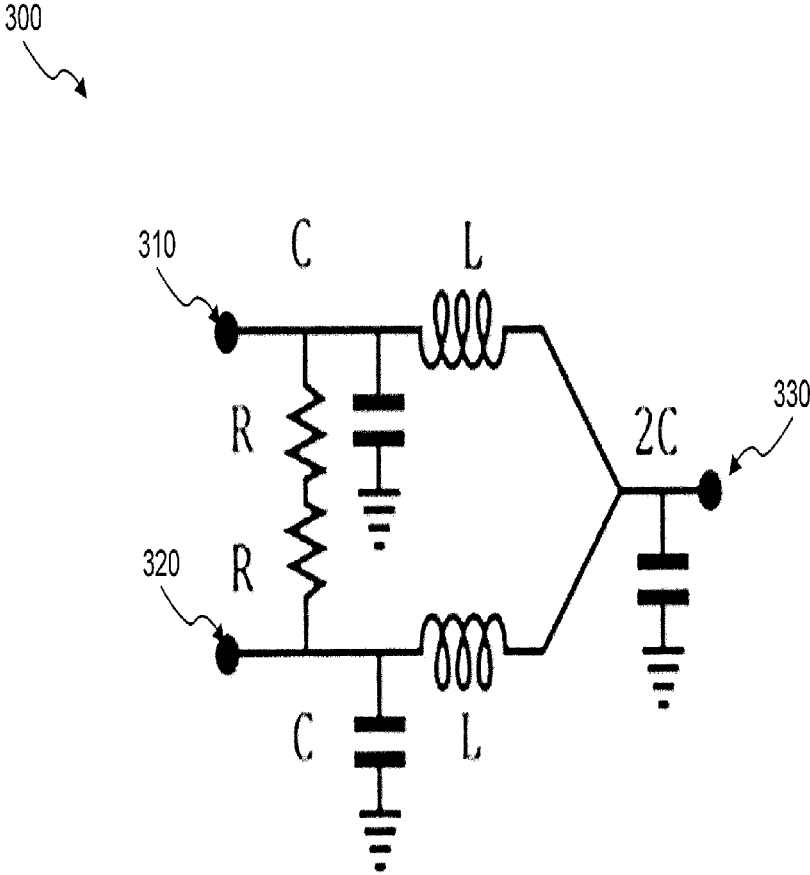


Fig. 3

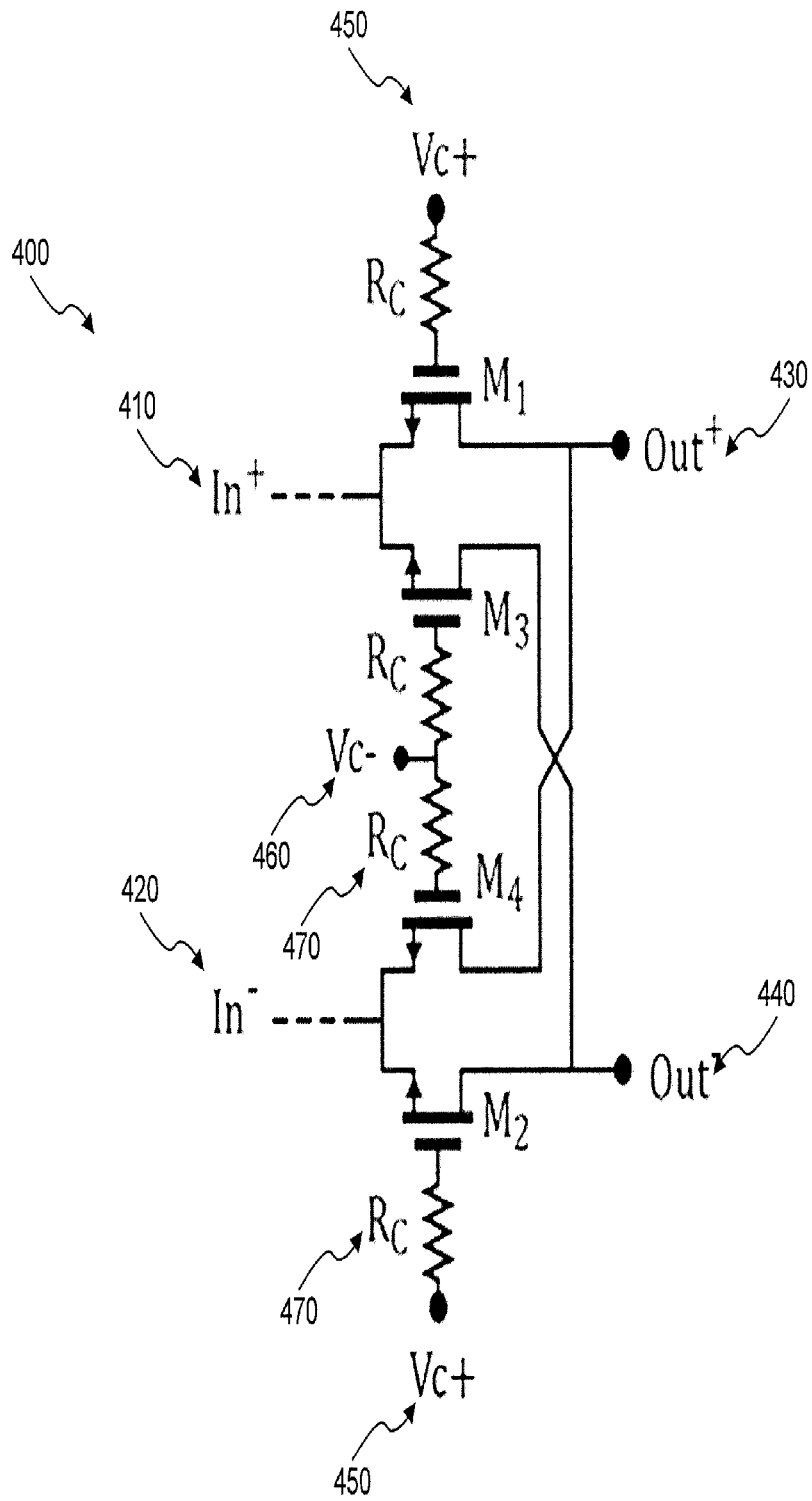


Fig. 4

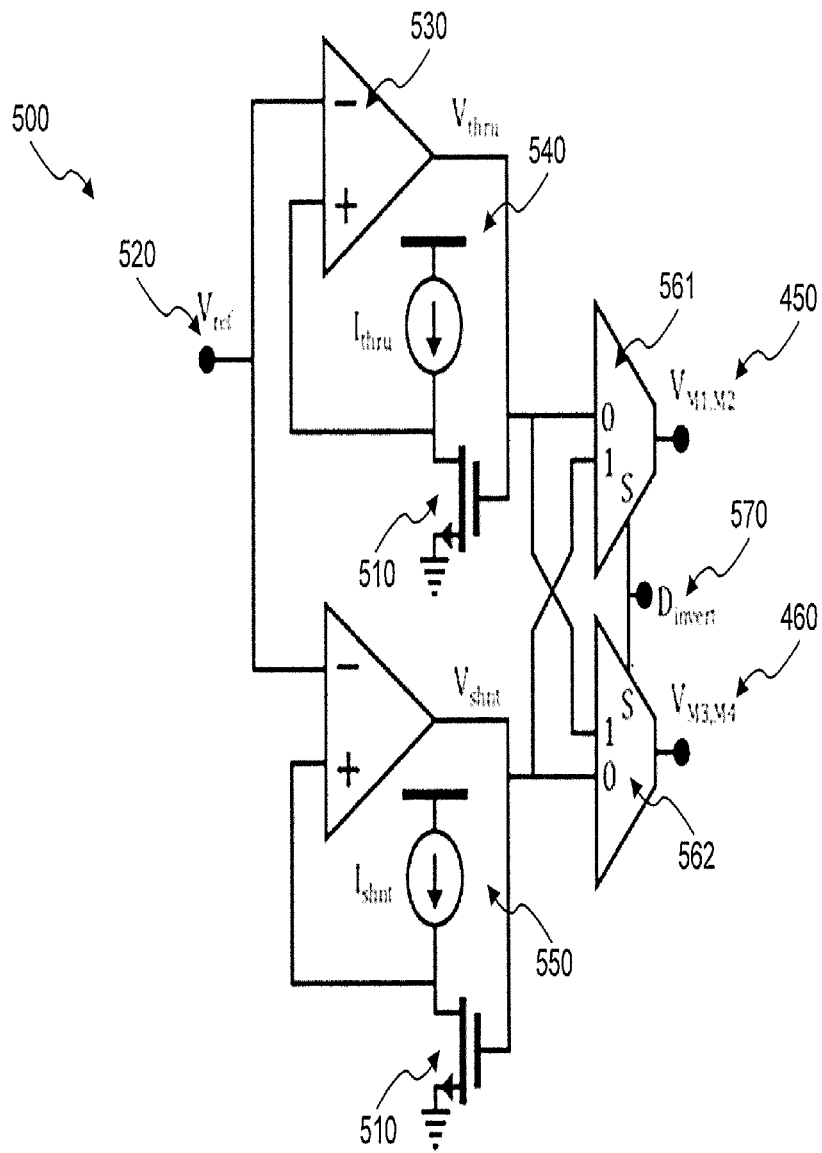


Fig. 5

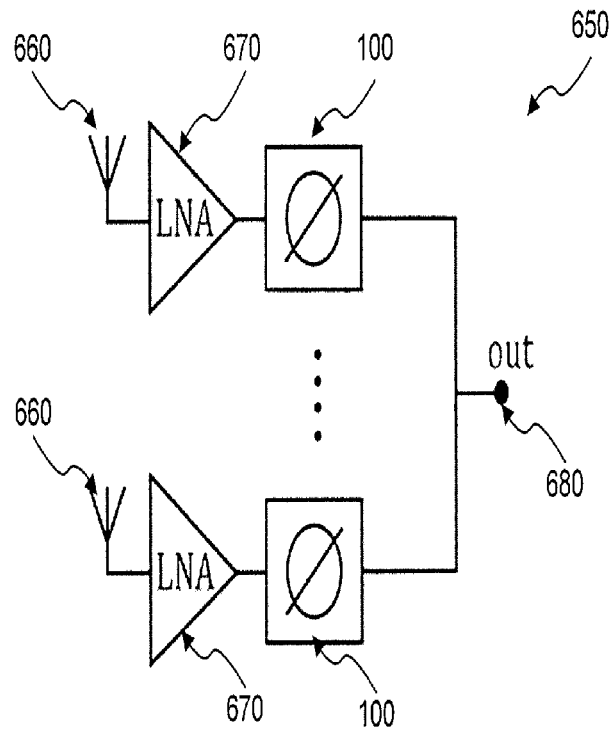
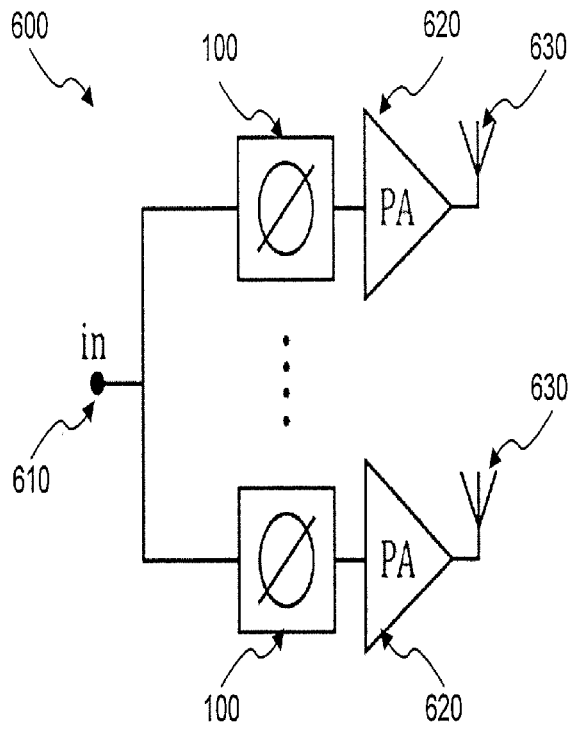


Fig. 6

HIGH-RESOLUTION PHASE SHIFTER

RELATED MATTERS

[0001] This application is a continuation of U.S. application Ser. No. 15/959,931, filed Apr. 23, 2018, having Attorney Docket No. 003955.00348, and entitled “HIGH-RESOLUTION PHASE SHIFTER,” and claims priority to U.S. Patent Application Ser. No. 62/490,251, filed on Apr. 26, 2017, having Attorney Docket No. 003955.00339, and entitled “HIGH-RESOLUTION PHASE SHIFTER,” the disclosure of which is incorporated by reference herein in its entirety and made part hereof.

FIELD

[0002] Aspects of the disclosure pertain to the design of phase shifters and to phased array antennas.

BACKGROUND

[0003] A phased array antenna usually includes an array of antenna elements. The radiation pattern of the phased array antenna can be dynamically modified by applying variable gain differences and/or phase shifts between the antenna elements. Unwanted variations in gain or in phase between the radiating elements result in off-axis emissions (side lobes) exceeding the regulation mask requirements. To prevent that, the necessary phase shifting and gain control should be applied at fine resolutions that are stable over temperature variations and over process variations.

[0004] A phased array antenna designed for satellite communications often requires a large number of radiating elements in order to achieve sufficient Effective Isotropic Radiated Power (EIRP) and Gain to (noise) Temperature (G/T) properties. Such specifications are derived from the distance between the terminal that uses such an antenna and the satellite, and due to strict satellite communications standards. In addition to the large number of radiating elements, such antenna also requires a large number of phase shifters and gain control devices (exhibiting fine resolution) that further contribute to high overall antenna power consumption. Therefore, the phase shifters and the gain control devices should be power-efficient.

[0005] Airborne radios (for in-flight connectivity) are required to operate over a wide range of temperatures with fast cycle time from hot temperatures (e.g., 50° C. while the aircraft is on the ground) to cold temperatures (e.g., -60° C. when the aircraft is at high altitudes). Gain controllers and phase shifters should tolerate such variations and present accurate performance over the entire temperature range.

[0006] The relatively large array size that is often needed for satellite communications and the power consumption considerations thereof, may create an incentive to use passive phase shifters for generating the necessary phase shifts between antenna elements of the array of antenna elements. Some known passive phase shifters are either of the reflective-type (i.e. a hybrid quadrature loaded by two reflective loads) or consist of a cascade of attenuators. Reflective-type phase shifters exhibit high gain variations over frequency and phase-shift settings, and are difficult to stabilize over temperature. Phase shifters consisting of cascades of attenuators are suitable for coarse phase resolution applications, however their insertion loss and size increase as the required phase shifting resolution increases (i.e. smaller phase shifting steps are needed).

SUMMARY

[0007] The following presents a simplified summary in order to provide a basic understanding of some aspects of the disclosure. The summary is not an extensive overview of the disclosure. It is neither intended to identify key or critical elements of the disclosure nor to delineate the scope of the disclosure. The following summary merely presents some aspects of the disclosure in a simplified form as a prelude to the description below.

[0008] Aspects of the disclosure are directed to a high resolution phase shifter. The high resolution phase shifter may be configured to exhibit fine phase-shifting resolution. Furthermore, the high resolution phase shifter may be configured to exhibit performance stability over a wide temperature range and over process variations. In some embodiments, the high resolution phase shifter may be configured to exhibit low (negligible) power consumption, small form factor, and/or low loss. In some embodiments, the high resolution phase shifter may comprise low insertion loss phase-inverting variable attenuators, which may be configured to exhibit high stability over a wide temperature range and over process variations.

[0009] Aspects of the disclosure are directed to a receiving phased array antenna and/or to a transmitting phased array antenna. Any of the receiving phased array antenna and the transmitting phased array antenna may comprise a plurality of antenna elements, wherein at least one antenna element of the plurality of antenna elements may comprise a high resolution phase shifter, e.g., as previously mentioned. In some embodiments, any of the receiving phased array antenna and the transmitting phased array antenna may be configured for satellite communications. In some embodiments, any of the receiving phased array antenna and the transmitting phased array antenna may be configured to be used as airborne antenna.

BRIEF DESCRIPTION OF THE DRAWINGS

[0010] Having thus described the disclosure in general terms, reference will now be made to the accompanying drawings, which are not necessarily drawn to scale, and wherein:

[0011] FIG. 1 shows a block diagram of an example phase shifter according to aspects of the disclosure.

[0012] FIG. 2 shows a schematic of an example of a quadrature splitter in accordance with aspects of the disclosure.

[0013] FIG. 3 shows a schematic of an example of a Wilkinson power combiner in accordance with aspects of the disclosure.

[0014] FIG. 4 shows a schematic of an example X-type attenuator in accordance with aspects of the disclosure.

[0015] FIG. 5 shows a schematic of an example calibration circuit in accordance with aspects of the disclosure.

[0016] FIG. 6 shows block diagrams of example transmitting phased array antenna and example receiving phased array antenna in accordance with aspects of the disclosure.

DETAILED DESCRIPTION

[0017] FIG. 1 shows a block diagram of a (high resolution) phase shifter 100. Phase shifter 100 may comprise a differential quadrature hybrid splitter 200 (shown in FIG. 2), two phase inverting variable (X-type) attenuators 400 (shown in FIG. 4), and a differential power combiner 300 (shown in

FIG. 3). In some embodiments, phase shifter 100 may be fabricated entirely on a single CMOS die.

[0018] The phase shifter 100 may be configured to apply a phase shift to an input signal using a Cartesian phase interpolation technique. A differential input signal 110 may be split into an I-component signal and a Q-component signal using the differential quadrature hybrid splitter 200. Amplitude scaling, either by amplification or attenuation, with or without phase inversion, may be separately applied to the I-component signal and to the Q-component signal using phase-inverting variable attenuators 400 to produce a scaled I-component signal and a scaled Q-component signal. The scaled component signals may be combined using differential power combiner 300 to produce a phase-shifted signal in reference to the differential input signal 110.

[0019] In reference to FIG. 2, the differential quadrature hybrid splitter 200 may be configured to receive an input signal 210 and to output (e.g., over two differential output ports) an I-component signal 220 and a Q-component signal 230 that may correspond to the input signal 210. In some embodiments, the differential quadrature hybrid splitter 200 may be an inductive-type lumped analog of a coupled-line hybrid coupler that may have smaller footprint than a distributed hybrid coupler.

[0020] Each of the two differential output ports of the differential quadrature hybrid splitter 200 (e.g., I and Q) may be coupled to the input terminals (410 and 420) of a phase-inverting variable attenuator 400 of the two phase inverting variable attenuators included in phase shifter 100. The output terminals (430 and 440) of each of the two phase inverting variable attenuators 400 may be coupled to a differential input port (e.g., of the two differential input ports 310 and 320) of the differential power combiner 300.

[0021] In reference to FIG. 3, the differential power combiner 300 may be configured to combine the signals provided at its input ports (310 and 320) and to output a combined signal through output port 330. In some embodiments, the differential power combiner 300 may be a lumped analog Wilkinson power combiner (e.g., as shown in FIG. 3), wherein a lumped analog Wilkinson power combiner may have smaller footprint than a standard (e.g., distributed) Wilkinson power combiner.

[0022] In reference to FIG. 4, the phase inverting variable attenuator 400 may comprise a differential input port comprising a first input terminal 410 and a second input terminal 420, and a differential output port comprising a first output terminal 430 and a second output terminal 440. The phase inverting variable attenuator 400 may comprise a first transistor M1 that may be coupled to the first input terminal 410 and to the first output terminal 430, a second transistor M2 that may be coupled to the second input terminal 420 and to the second output terminal 440, a third transistor M3 that may be coupled to the first input terminal 410 and to the second output terminal 440, and a fourth transistor M4 that may be coupled to the second input terminal 420 and to the first output terminal 430. In some embodiments, the first transistor M1, the second transistor M2, the third transistor M3 and the fourth transistor M4 (e.g., herein transistors M1 to M4) may be Field-Effect Transistors (FET).

[0023] The phase inverting variable attenuator 400 may be in one of two phase states, corresponding to a 0° phase (e.g., no phase inversion) and a 180° phase (e.g., phase inversion). In some embodiments, the phase state of the phase inverting variable attenuator 400 may be controlled by control volt-

ages V_{C+} (450) and V_{C-} (460). The phase state of phase inverting variable attenuator 400 may be flipped when the control voltages V_{C+} (450) and V_{C-} (460) are flipped. Control voltage 450 may be coupled to the gate terminals of transistors M1 and M2. Control voltage 460 may be coupled to the gate terminals of transistors M3 and M4. The control voltages 450 and 460 may be coupled to the respective gate terminals of transistors M1 to M4 through “choke” resistors 470, wherein using resistors 470 for said coupling may improve (e.g., reduce) an insertion loss characteristic of the phase inverting variable attenuator 400, and wherein the insertion loss may result from leakage through the gate capacitances of transistors M1 to M4. The source and drain terminals of transistors M1 to M4 may be biased at 0 Volts for at least the purpose of reducing a loss property of the phase inverting variable attenuator 400, e.g., by eliminating the Body Effect and maximizing the allowed gate-source voltage (V_{GS}).

[0024] The coupling of the control voltages V_{C+} (450) and V_{C-} (460) to the respective gate terminals of transistors M1 to M4 through resistors 470 may be advantageous. As described further herein, at least a phase-shifting resolution property of phase shifter 100 may be affected by a maximum attenuation (attenuation range) that phase inverting variable attenuator 400 may exhibit. Phase inverting variable attenuator 400 may be configured to exhibit maximum attenuation when the control voltages V_{C+} (450) and V_{C-} (460) may be of a same level. When the control voltages V_{C+} (450) and V_{C-} (460) may be of a same level, the (maximum) attenuation may be limited by signal leakage through parasitic capacitances (e.g., of transistors M1 to M4). Using resistors 470 may enable reducing the size of transistors M1 to M4 while maintaining low (minimum) insertion loss, wherein reducing the size of transistors M1 to M4 may result in lower parasitic capacitances and higher maximum attenuation (e.g., better phase-shifting resolution).

[0025] In some embodiments, a resistance value of resistors 470 (e.g., R_C) may be selected as high as possible for at least the purpose of reducing the insertion loss while maintaining a settling time of the control voltages 450 and 460 at the respective gates of transistors M1 to M4 as low as may be needed. For example, an antenna may comprise one or more phase shifters 100 and a steering speed property of the antenna may be limited, among other things, by a settling time of the one or more phase shifters 100 (that may depend on a settling time of the control voltages 450 and 460 at the respective gates of transistors M1 to M4). Thus, the selection of a resistance value for resistors 470 may comprise considering a required steering speed property of an antenna with one or more phase shifters 100 and selecting the resistance value so that the steering speed property of the antenna is not limited (or acceptably limited) by a settling time of the control voltages 450 and 460 at the respective gates of transistors M1 to M4.

[0026] In some embodiments, the phase-shifting resolution (θ_{min}) of phase shifter 100 may be determined by the full attenuation range (R) of the phase inverting variable attenuator 400, for example in accordance with the formula: $\theta_{min}=2*\text{ARCSIN}(1/R)$, wherein ARCSIN is the trigonometric inverse sine function. For example, a phase shifter 100 that may comprise a phase inverting variable attenuator 400 configured to exhibit an attenuation range of 40 dB (e.g., $1/R=1/100$) may exhibit a phase-shifting resolution of roughly 1.15 degrees. As previously described, using resis-

tors **470** may improve the attenuation range of the phase inverting variable attenuator **400**, hence allow achieving finer phase-shifting resolution (e.g., lower values of θ_{min}).

[0027] Let R_{M1} to R_{M4} denote the channel resistances of transistors **M1** to **M4**, respectively. Let R_{thru} and R_{shnt} be defined as follows:

$$R_{thru} = \begin{cases} R_{M1}, R_{M2}, & \text{phase} = 0^\circ \\ R_{M3}, R_{M4}, & \text{phase} = 180^\circ \end{cases}$$

$$R_{shnt} = \begin{cases} R_{M3}, R_{M4}, & \text{phase} = 0^\circ \\ R_{M1}, R_{M2}, & \text{phase} = 180^\circ \end{cases}$$

It may follow from the above definition that R_{thru} may always be lower than R_{shnt} . Neglecting parasitic resistances, the insertion loss (S_{21}), the input return loss (S_{11}) and the output return loss (S_{22}) characteristics of phase inverting variable attenuator **400** may be calculated as follows, wherein Z_0 may denote the characteristic impedance of the (differential) input and output ports of the phase inverting variable attenuator **400**:

$$S_{21} = \frac{R_{shnt} - R_{thru}}{(\sqrt{R_{thru}} + \sqrt{R_{shnt}})^2}$$

$$S_{11} = S_{22} = \frac{R_{thru} \cdot R_{shnt} - Z_0^2}{Z_0 \cdot (R_{thru} + R_{shnt} + Z_0) + R_{thru} \cdot R_{shnt}}$$

Two observations may be derived from the above equations. First, both the insertion loss (attenuation level) (S_{21}) and the return losses (S_{11} and S_{22}) characteristics of the phase inverting variable attenuator **400** are affected (determined) by R_{thru} and R_{shnt} . Second, if the minimum resistance values of R_{thru} and R_{shnt} are limited (e.g., for at least the purpose of maintaining low parasitic capacitances), there is a tradeoff between a range of possible attenuation levels and the return loss characteristics of phase inverting variable attenuator **400**.

[0028] In order to enable use of an entire range of sets of attenuation levels and return loss values, the channel resistances R_{thru} and R_{shnt} of transistors **M1** to **M4** may be controlled by two separate bias circuits, as shown in FIG. 5. Each bias circuit of the two bias circuits **500** may be configured to generate a gate control voltage, e.g., V_{thru} or V_{shnt} corresponding to a channel resistance R_{thru} or R_{shnt} respectively. Bias circuits **500** may comprise two multiplexers (**561** and **562**) that may be controlled by a common control signal **570** and configured to route any of the gate control voltages V_{thru} and V_{shnt} to transistors M_1 thru M_4 in accordance with the control signal **570** and the definitions of the corresponding channel resistances R_{thru} and R_{shnt} as provided above. The two input terminals of each of the two multiplexers may be coupled to both gate control voltages, V_{thru} or V_{shnt} , but in opposite orders. For example, the V_{thru} gate control voltage may be coupled to a first input of multiplexer **561** and to a second input of multiplexer **562**, whereas the V_{shnt} gate control voltage may be coupled to a second input of multiplexer **561** and to a first input of multiplexer **562**. Furthermore, the output terminal of multiplexer **561** may be coupled to provide the control voltage V_{C+} (**450**) to the phase inverting variable attenuator **400**, and

the output terminal of multiplexer **562** may be coupled to provide the control voltage V_{C-} (**460**) to the phase inverting variable attenuator **400**. Thus, the phase state of phase inverting variable attenuator **400** may be flipped using the common control signal **570**.

[0029] Each bias circuit of the two bias circuits **500** may comprise a transistor **510** that may be of similar characteristics as any of the transistors **M1** to **M4** of the phase inverting variable attenuator **400**. In some embodiments, where transistors **M1** to **M4** may be FET transistors, transistors **510** may also be FET transistors of characteristics similar to those of transistors **M1** to **M4**. The bias current of each transistor **510**, e.g., I_{thru} or I_{shnt} , may be set using a current digital to analog converter (IDAC). In addition, the drain voltage of each transistor **510** may be set in accordance with a reference voltage **520** (V_{ref}), for example using a control loop (**540**, **550**) that comprises an operational amplifier **530**. Each control loop (**540**, **550**) may be configured to maintain a gate control voltage, V_{thru} or V_{shnt} , for the respective transistor **510** so that:

$$R_{510} = \frac{V_{ref}}{I_{DAC}}$$

Wherein the bias current I_{DAC} is either I_{thru} or I_{shnt} as per the respective control loop. In some embodiments, the reference voltage **520** (V_{ref}) may be set to a lowest voltage that may be supported by the operational amplifier(s) **530**, e.g., for at least the purpose of operating any of the transistors **510** at roughly the same operating conditions as those of transistors **M1** to **M4** of the phase inverting variable attenuator **400**. In some embodiments, the reference voltage **520** (V_{ref}) may be set to approximately 100 millivolts (mV). In some embodiments, the physical gate width of transistors **510** may be smaller than the gate width of any of the transistors **M1** to **M4** of the phase inverting variable attenuator **400** for at least the purpose of reducing power consumption of transistors **510**.

[0030] Since R_{thru} may be always lower than R_{shnt} , the IDAC in the “thru” control loop **540** may always be required to provide higher current than the IDAC in the “shnt” control loop **550**. To maximize an attenuation range of phase inverting variable attenuator **400** per given silicon area and simplify control over the bias circuits **500** by maintaining a same number of control bits in both IDAC devices, bias circuits **500** may comprise a low current IDAC for the “shnt” control loop **550** and a high current IDAC for the “thru” control loop **540**. In some embodiments, both the low current IDAC and the high current IDAC may be 5-bit IDACs.

[0031] In some embodiments, the attenuation (S_{21}) and the return losses (S_{11} and S_{22}) characteristics of the phase inverting variable attenuator **400** may be maintained over temperature and process variations. Considering that temperature-dependent and process-dependent parasitic capacitances may be negligible, the said characteristics may be maintained as long as the reference voltage (V_{ref}) and the bias currents (I_{thru} and I_{shnt}) remain constant.

[0032] FIG. 6 shows a block diagram of an example phased array antenna **600** and a block diagram of an example

phased array antenna **650**. Phased array antenna **600** may be configured to be at least a transmitting antenna, whereas phased array antenna **650** may be configured to be at least a receiving antenna. In some embodiments, each of the phased array antennas **600** and **650** may be configured to use a dedicated aperture. In other embodiments, phased array antennas **600** and **650** may be configured to share a single (common) aperture. The phased array antennas **600** and **650**, whether using dedicated apertures or a common aperture, may also be configured for satellite communications in any of the Ku-band or the Ka-band. The phased array antennas **600** and **650**, whether using dedicated apertures or a common aperture, may also be configured to be used as airborne antennas.

[0033] Phased array antenna **600** may comprise a plurality of array elements coupled to an input port **610**. An input signal may be received via input port **610** and then split to feed each of the array elements of the plurality of array elements. Each array element of the plurality of array elements may comprise at least a (high resolution) phase shifter **100**, an amplifier **620** (e.g., a power amplifier), and a radiating (antenna) element **630**. The phase shifter **100** may be configured to apply at least a phase-shift to the signal fed to the array element, wherein the phase-shift may vary in accordance with variations in a radiation pattern of phased array antenna **600**. The phase-shifted signal may be amplified by amplifier **620** and the amplified signal may be transmitted using the radiating element **630**. In some embodiments, each array element of the plurality of array elements of antenna **600** may further comprise an up converter (not shown in FIG. 6), wherein a common local oscillator signal may be provided to the up converters in all the plurality of array elements. In such embodiments, in each of the array elements, the phase shifter **100** may be used for applying a phase-shift to the local oscillator signal rather than to the signal fed to the array element. In such embodiments, the phase shifter **100** may be used at a limited number of frequencies (for example, at a single frequency) and therefore would exhibit high phase-shifting performance stability (as one of the variables affecting phase-shifting performance is reduced or eliminated).

[0034] Phased array antenna **650** may comprise a plurality of array elements that may be coupled to an output port **680**. Each antenna element of the plurality of antenna elements may comprise at least a receiving (antenna) element **660**, a low-noise amplifier **670**, and a (high resolution) phase shifter **100**. In each array element, a signal received by the receiving element **660** may be amplified by the low-noise amplifier **670**, and the amplified signal may be phase-shifted by the phase shifter **100**, wherein the phase-shift may vary in accordance with variations in a reception pattern of phased array antenna **650**. The phase-shifted signals from the plurality of array elements may be combined together to form an output signal that may be transmitted at output port **680** of phased array antenna **650**. In some embodiments, each array element of the plurality of array elements of antenna **650** may further comprise a down converter (not shown in FIG. 6), wherein a common local oscillator signal may be provided to the down converters in all the plurality of array elements. In such embodiments, in each of the array elements, the phase shifter **100** may be used for applying a phase-shift to the local oscillator signal rather than to the amplified received signal. In such embodiments, the phase shifter **100** may be used at a limited number of frequencies

(for example, at a single frequency) and therefore would exhibit high phase-shifting performance stability.

1. An apparatus comprising:
 - a differential quadrature hybrid splitter;
 - a first phase inverting variable attenuator coupled to the differential quadrature hybrid splitter, wherein the first phase inverting variable attenuator comprises:
 - a first control voltage input configured to provide a first control voltage; and
 - a second control voltage input configured to provide a second control voltage,
 wherein the first control voltage and the second control voltage control a phase state of the first phase inverting variable attenuator;
 - a second phase inverting variable attenuator coupled to the differential quadrature hybrid splitter; and
 - a differential power combiner coupled to the first phase inverting variable attenuator and the second phase inverting variable attenuator.
2. The apparatus of claim 1, wherein the first phase inverting attenuator is configured to be in one of two phase states.
3. The apparatus of claim 1, wherein the first phase inverting variable attenuator further comprises:
 - a first transistor coupled to an input port and an output port;
 - a second transistor coupled to the input port and to the output port;
 - a third transistor coupled to the input port and the output port; and
 - a fourth transistor coupled to the input port and the output port;
4. The apparatus of claim 3, wherein:
 - a gate terminal of the first transistor and a gate terminal of the second transistor are coupled to the first control voltage input via a first resistor and a second resistor, respectively; and
 - a gate terminal of the third transistor and a gate terminal of the fourth transistor are coupled to the second control voltage input via a third resistor and a fourth resistor, respectively.
5. The apparatus of claim 4, wherein a plurality of the first resistor, the second resistor, the third resistor and the fourth resistor are of a same resistance value.
6. The apparatus of claim 3, further comprising biasing circuitry configured to control one or more channel resistances of the first transistor, second transistor, third transistor, and fourth transistor.
7. An apparatus comprising:
 - a plurality of array elements coupled to a common input port, wherein each array element of the plurality of array elements comprises:
 - an amplifier;
 - a radiating antenna element coupled to the amplifier; and
 - a phase shifter comprising at least one phase inverting variable attenuator, wherein the at least one phase inverting variable attenuator comprises:
 - a first control voltage input configured to provide a first control voltage; and
 - a second control voltage input configured to provide a second control voltage,

wherein the first control voltage and the second control voltage control a phase state of the at least one phase inverting variable attenuator.

8. The apparatus of claim 7, wherein the at least one phase inverting attenuator is configured to be in one of two phase states.

9. The apparatus of claim 7, wherein the at least one phase inverting variable attenuator further comprises:

- a first transistor coupled to an input port and an output port;
- a second transistor coupled to the input port and to the output port;
- a third transistor coupled to the input port and the output port; and
- a fourth transistor coupled to the input port and the output port;

10. The apparatus of claim 9, wherein:

a gate terminal of the first transistor and a gate terminal of the second transistor are coupled to the first control voltage input via a first resistor and a second resistor, respectively; and

a gate terminal of the third transistor and a gate terminal of the fourth transistor are coupled to the second control voltage input via a third resistor and a fourth resistor, respectively.

11. The apparatus of claim 10, wherein a plurality of the first resistor, the second resistor, the third resistor and the fourth resistor are of a same resistance value.

12. The apparatus of claim 9, further comprising biasing circuitry configured to control one or more channel resistances of the first transistor, second transistor, third transistor, and fourth transistor.

13. An apparatus comprising:

a plurality of array elements coupled to a common output port, wherein each array element of the plurality of array elements comprises:

- a receiving antenna element;
- a low-noise amplifier coupled to the receiving antenna element; and

a phase shifter comprising at least one phase inverting variable attenuator, wherein the at least one phase inverting variable attenuator comprises:

- a first control voltage input configured to provide a first control voltage; and
- a second control voltage input configured to provide a second control voltage,

wherein the first control voltage and the second control voltage control a phase state of the at least one phase inverting variable attenuator.

14. The apparatus of claim 13, wherein the at least one phase inverting attenuator is configured to be in one of two phase states.

15. The apparatus of claim 13, wherein the at least one phase inverting variable attenuator further comprises:

a first transistor coupled to an input port and an output port;

a second transistor coupled to the input port and to the output port;

a third transistor coupled to the input port and the output port; and

a fourth transistor coupled to the input port and the output port.

16. The apparatus of claim 15, wherein:

a gate terminal of the first transistor and a gate terminal of the second transistor are coupled to the first control voltage input via a first resistor and a second resistor, respectively; and

a gate terminal of the third transistor and a gate terminal of the fourth transistor are coupled to the second control voltage input via a third resistor and a fourth resistor, respectively.

17. The apparatus of claim 16, wherein a plurality of the first resistor, the second resistor, the third resistor and the fourth resistor are of a same resistance value.

18. The apparatus of claim 15, further comprising biasing circuitry configured to control one or more channel resistances of the first transistor, second transistor, third transistor, and fourth transistor.

19. An apparatus comprising:

a first transistor coupled to an input port and an output port;

a second transistor coupled to the input port and to the output port;

a third transistor coupled to the input port and the output port;

a fourth transistor coupled to the input port and the output port;

a first control voltage input configured to provide a first control voltage; and

a second control voltage input configured to provide a second control voltage,

wherein the first control voltage and the second control voltage control a phase state of the apparatus.

20. The apparatus of claim 19, wherein:

a gate terminal of the first transistor and a gate terminal of the second transistor are coupled to the first control voltage input via a first and a second resistors respectively; and

a gate terminal of the third transistor and a gate terminal of the fourth transistor are coupled to the second control voltage input via a third and a fourth resistors respectively.

21. The apparatus of claim 20, wherein the first resistor, the second resistor, the third resistor and the fourth resistor are all of a same resistance value.

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