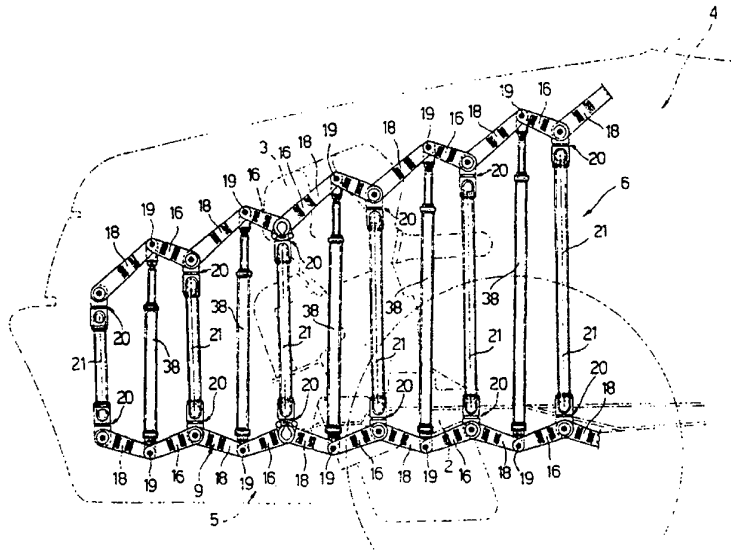




INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

<p>(51) International Patent Classification⁵ : G01M 17/00</p>	<p>A1</p>	<p>(11) International Publication Number: WO 95/00828 (43) International Publication Date: 5 January 1995 (05.01.95)</p>
<p>(21) International Application Number: PCT/IT94/00091 (22) International Filing Date: 21 June 1994 (21.06.94) (30) Priority Data: TO93A000451 22 June 1993 (22.06.93) IT (71) Applicant (for all designated States except US): FIAT AUTO S.P.A. [IT/IT]; Corso Giovanni Agnelli, 200, I-10135 Torino (IT). (72) Inventor; and (75) Inventor/Applicant (for US only): DA RE', Mario [IT/IT]; Via Cristoforo Colombo, 9, I-10100 Torino (IT). (74) Agents: BONGIOVANNI, Guido et al.; Studio Torta, Via Viotti, 9, I-10121 Torino (IT).</p>		<p>(81) Designated States: BR, JP, US, European patent (AT, BE, CH, DE, DK, ES, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE). Published With international search report.</p>

(54) Title: APPARATUS, METHOD AND REUSABLE MODEL-STRUCTURE FOR IMPACT TESTING VEHICLE COMPONENTS



(57) Abstract

The front body assembly of a vehicle is simulated by a reusable model-structure featuring a pair of side members collapsible accordion fashion and each comprising a number of arms hinged in series with one another by respective articulating means, and a number of hydraulic friction joints constituting at least some of the articulating means. Each hydraulic joint presents an adjustable sliding torque by virtue of being connected to pressurized fluid supply means via a respective pressure regulating valve. Once calibrated the model-structure, which thus presents the same collapse performance as the front body assembly being simulated, is fitted with the test component and used for impact testing; and, following impact, the collapsed model-structure is restored to its original configuration by means of hydraulic actuators, after first zeroing the pressure of the hydraulic joints.

FOR THE PURPOSES OF INFORMATION ONLY

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AT	Austria	GB	United Kingdom	MR	Mauritania
AU	Australia	GE	Georgia	MW	Malawi
BB	Barbados	GN	Guinea	NE	Niger
BE	Belgium	GR	Greece	NL	Netherlands
BF	Burkina Faso	HU	Hungary	NO	Norway
BG	Bulgaria	IE	Ireland	NZ	New Zealand
BJ	Benin	IT	Italy	PL	Poland
BR	Brazil	JP	Japan	PT	Portugal
BY	Belarus	KE	Kenya	RO	Romania
CA	Canada	KG	Kyrgystan	RU	Russian Federation
CF	Central African Republic	KP	Democratic People's Republic of Korea	SD	Sudan
CG	Congo	KR	Republic of Korea	SE	Sweden
CH	Switzerland	KZ	Kazakhstan	SI	Slovenia
CI	Côte d'Ivoire	LI	Liechtenstein	SK	Slovakia
CM	Cameroon	LU	Luxembourg	SN	Senegal
CN	China	LK	Sri Lanka	TD	Chad
CS	Czechoslovakia	LV	Latvia	TG	Togo
CZ	Czech Republic	MC	Monaco	TJ	Tajikistan
DE	Germany	MD	Republic of Moldova	TT	Trinidad and Tobago
DK	Denmark	MG	Madagascar	UA	Ukraine
ES	Spain	ML	Mali	US	United States of America
FI	Finland	MN	Mongolia	UZ	Uzbekistan
FR	France			VN	Viet Nam
GA	Gabon				

5

APPARATUS, METHOD AND REUSABLE MODEL-STRUCTURE FOR
IMPACT TESTING VEHICLE COMPONENTS

10 TECHNICAL FIELD

The present invention relates to an apparatus for
impact testing the mechanical performance of vehicle
components, in particular the front load-bearing
components of a vehicle body or structure, such as the
15 front cross member, engine supporting frame and similar,
but without involving total destruction of the vehicle.

The present invention also relates to a test
method employing the above apparatus, and to a reusable,
collapsible model-structure forming the main part of the
20 apparatus, designed to receive the test component, and
which, with the component on board, provides for
standard impact testing by accurately simulating the
dynamic performance of any existing front vehicle body
assembly.

25 BACKGROUND ART

Before launching a new model on to the market, or
whenever improvements or changes are made to the
load-bearing components of existing models, all car

- 2 -

manufacturers conduct "live" impact tests to determine the mechanical response of vehicle body and internal passenger compartment components to dynamic design stress. At present, these tests involve a good deal of expense in that simply determining the response of one component (e.g. the engine supporting frame, front cross member, bumper, seat guide, safety belt fasteners, etc.) involves the total destruction of vehicles identical to those for marketing. For, even though the deformation performance of the overall vehicle structure may be determined easily and cheaply by means of full-vehicle impact tests conducted for other purposes (e.g. passenger safety tests using a manikin), this is not sufficient for extrapolating the performance of individual components.

DISCLOSURE OF INVENTION

It is an object of the present invention to provide an apparatus for "live" impact testing vehicle components, particularly single front vehicle body components, without requiring total destruction of the vehicle.

In particular, it is an object of the present invention to provide a mechanical "model" structure for simulating, without damage, the impact performance of any front vehicle assembly, so as it may be reused in numerous tests, in order to be used in conjunction with the above apparatus for determining the resistance of vehicle body and internal passenger compartment

- 3 -

components, providing for drastically reducing the cost of current test methods.

Finally, it is a further object of the present invention to provide a test method employing the above apparatus and wherein the above model-structure is used
5 in lieu of the complete vehicle.

According to the present invention, there is provided an apparatus for impact testing vehicle components, characterized by the fact that it comprises
10 a reusable trestle type model-structure designed, on impact, to switch from an extended to a collapsed configuration with the same dynamic performance as the front vehicle body assembly being simulated, the model-structure comprising a number of substantially
15 rigid, load-bearing elements articulated by means of friction elements with an adjustable sliding torque; the apparatus also comprising means for supporting the model-structure; means for selectively calibrating the sliding torque of each friction element to a
20 predetermined value above which the friction element permits relative rotation of the load-bearing elements connected by it, and hence collapse of the model-structure; and at least one actuator for restoring the model-structure, after impact, from the collapsed
25 configuration to the same extended configuration prior to impact; the model-structure being designed, at least in the extended configuration, to receive at least one vehicle test component.

- 4 -

As opposed to using, and hence destroying, a high-cost production vehicle, the test apparatus according to the present invention thus provides for employing a low-cost model-structure which is in no way
5 damaged during testing and may thus be reused for any number of tests.

The above apparatus is employed in a vehicle component impact test method, characterized by the fact that it comprises the following stages:

- 10 - setting up a reusable model-structure for simulating the dynamic collapse performance of the vehicle of which the test component forms part; the model-structure being formed by connecting a number of substantially rigid, load-bearing elements in articulated manner by means of
15 friction elements with an adjustable sliding torque;
- so calibrating said model-structure as to enable it, upon impact, to switch from an extended to a collapsed configuration with the same dynamic performance as the front vehicle body assembly being simulated; said
20 calibrating stage being performed by trial and error, by subjecting the model-structure to a predetermined amount of dynamic stress, determining the dynamic collapse performance of the structure, restoring the structure to the extended configuration, and separately adjusting the
25 sliding torque of each friction element until the dynamic collapse performance of the model-structure corresponds with the known performance of the body assembly being simulated;

- 5 -

- fitting the test component to the extended model-structure, and conducting a normal impact test using the model-structure in lieu of the vehicle to which the test component is to be mounted.

5 The known deformation performance of each vehicle as a whole is thus used for accordingly calibrating a single model-structure which, once calibrated, provides for accurately simulating the deformation performance of the front assembly of a given vehicle model. As such,
10 one model-structure and one test apparatus according to the present invention provide for all-round testing of substantially any existing vehicle model.

In particular, a reusable model-structure is employed, characterized by the fact that it comprises a
15 first and second trestle type side member collapsible accordion fashion, located parallel to each other, and each comprising a number of arms hinged in series with one another by respective articulating means, and a number of hydraulic friction joints constituting at
20 least some of the articulating means.

BRIEF DESCRIPTION OF THE DRAWINGS

A non-limiting embodiment of the present invention will be described by way of example with reference to the accompanying drawings, in which:

25 Figures 1 and 2 respectively show an elevation and top plan view of a test apparatus in accordance with the present invention;

 Figures 3 and 4 respectively show an enlarged rear

- 6 -

view of the front, and an enlarged, partially sectioned detail, of a model-structure employed on the Figure 1 and 2 apparatus;

Figures 5 and 6 respectively show an elevation and top plan view of the Figure 3 and 4 model-structure in use.

BEST MODE FOR CARRYING OUT THE INVENTION

With reference to Figures 1, 2 and 5, 6, number 1 indicates an apparatus for destructive impact testing vehicle components - in the non-limiting example shown, the front frame 2 supporting the engine 3 of a vehicle 4 (Figures 5, 6) of which the dynamic deformation performance of at least the front body assembly 5 is known.

According to the main characteristic of the present invention, apparatus 1 comprises a twin-trestle type model-structure 6, designed to receive test component 2 and to simulate, during normal impact testing, the known dynamic collapse performance of front body assembly 5 of vehicle 4. As such, known impact testing for determining the on-vehicle mechanical performance of component 2, and consisting in driving vehicle 4 as a whole, complete with component 2, at a given speed against a fixed obstacle, may be performed using, in lieu of vehicle 4, model-structure 6 which provides in every way for mechanically simulating front body assembly 5.

According to the present invention,

- 7 -

model-structure 6 is formed, on the one hand, so as to undergo no damage during impact testing, thus enabling it to be reused, as will be seen, for any number of tests; and, on the other hand, so as to selectively
5 simulate the performance of the front body assembly of vehicles 4 of different types and models, by simply "setting up" or calibrating model-structure 6 on apparatus 1 prior to testing.

With reference also to Figures 3 and 4,
10 model-structure or mechanical simulator 6 according to the present invention comprises two side members 8, 9 in the form of three-dimensional trestle structures collapsible lengthwise in accordion fashion (i.e. in the direction of respective axes A and B - Figure 6); and
15 two rigid, respectively front and rear cross members 10, 11 defined by load-bearing base elements in the form of a plate. Cross members 10, 11 are useful for achieving unity of model-structure 6 even when detached from apparatus 1, and for protecting side members 8, 9 during
20 impact, but are not strictly indispensable as regards operation of structure 6.

More specifically, side members 8, 9 and cross members 10, 11 are arranged parallel to each other so that, viewed from above, structure 6 presents the form
25 of a quadrilateral; and are connected to one another at the corners of quadrilateral structure 6 by hinge type articulating means defined, for cross member 10, by a pair of idle vertical-axis pins 12, and, for cross

- 8 -

member 11, by a pair of known hydraulic friction joints 13 with a rotation axis parallel to that of pins 12, so that, viewed from above, model-structure 6 defines an articulated quadrilateral.

5 Each identical side member 8, 9 comprises a number of substantially rigid, load-bearing elements defined by pairs of parallel arms 16, 18 hinged in series and in zig-zag fashion to one another by respective articulating means, the axes of rotation of which are
10 all parallel to one another, and perpendicular to axes A, B and to the rotation axes of pins 12 and friction joints 13. According to the present invention, said articulating means consist alternately of respective idle pins 19, and a number of hydraulic friction joints
15 20 of the same type as joints 13 but a different model.

To support joints 20 and ensure the structural solidity of side members 8, 9, these also comprise a number of rigid rectangular frames 21, e.g. made of bent, welded tubular metal elements, increasing in size
20 from cross member 10 towards cross member 11 (Figures 3 and 6), and the respective top and bottom horizontal portions 22 of which are fitted integral with hydraulic friction joints 20, e.g. by means of brackets 23 either welded or locked by further joints 25, so that, on
25 either side of each frame 21, two pairs of arms 18 (one from bottom horizontal portion 22, and one from top portion 22) extend towards cross member 11, and two pairs of arms 16 towards cross member 10. Further end

- 9 -

pairs of arms 16 and 18 provide for connecting side members 8, 9 in articulated manner to cross members 10, 11 by means of pins 26 parallel to pins 19, and via pins 12 and friction joints 13 described previously.

5 As shown particularly in Figure 4, known hydraulic friction joints 20 - e.g. of the type known as SAFESET marketed by MONDIAL of Milan - present an adjustable sliding torque below which any relative movement of connected arms 16, 18 is prevented, and above which arms
10 16 are permitted to rotate, with a predetermined amount of friction, in relation to arms 18 and about mutual hinge axes D (Figures 3 and 4) parallel to the axes of pins 19.

In the example shown, each joint 20 comprises a
15 pin 30 housed idly inside a fluidtight housing 31 integral with respective frame 21. Arms 16, 18 are fitted angularly integral with pin 30, and cooperate laterally, on either side, with respective friction disks 32 fitted inside and integral with housing 31 and
20 therefore angularly fixed but axially slidable in relation to pin 30. Friction disks 32 and arms 16, 18 are acted on by a piston 33 activated by the hydraulic pressure inside a chamber 34 formed inside housing 31 and connected by a pipe 35 to a pressurized fluid, e.g.
25 oil, source. Friction disks 32 thus exert on arms 16, 18 a retaining torque proportional to the hydraulic pressure inside chamber 34 and, hence, to the axial pressure exerted by piston 33; and said sliding torque

- 10 -

of the joint is that which, applied to pins 30 by arms 16, 18, exceeds the retaining torque exerted by friction disks 32 by just enough to slide friction disks 32 and hence rotate arms 16, 18 in relation to housing 31.

5 Structure 6 therefore behaves as a statically determined structure as long as the stress applied to it (e.g. by cross member 10) is such that the torques transmitted to arms 16, 18 are below the sliding torque of each joint; whereas it becomes a reticulated
10 structure with at least a few weak nodes when said stress is such that the torque transmitted to even only one arm 16 or 18 is greater than the retaining torque exerted by friction disks 32, i.e. greater than the sliding torque of the respective joint 20. As the latter
15 torque is proportional to the hydraulic pressure in respective chamber 34, by appropriately regulating this pressure differently from one joint to another, it is possible to achieve different responses of the same structure 6 to the same system of external mechanical
20 stress applied to it.

The same also applies to joints 13 (not shown in detail) only in this case relative to axes perpendicular to axes D and parallel to pins 12. Consequently, when a side member 8, 9 as a whole transmits to respective
25 joint 13 a torque greater than the sliding torque of the joint, the quadrilateral defined by side members 8, 9 and cross members 10, 11 becomes statically weak, thus enabling rotation about the axes of pins 12 and joints

- 11 -

13. As such, model-structure 6 may selectively assume two configurations: an extended configuration (Figures 1, 2 and 5, 6) wherein arms 16, 18 are arranged at an angle to each other, the size of structure 6 as a whole is comparable with that of the front body assembly being simulated (Figures 5, 6), and structure 6 may be fitted with at least one vehicle test component (in this case, frame 2); and a collapsed configuration (not shown) wherein structure 6 is compressed accordion fashion along axes A, B, and possibly also positioned obliquely in relation to axes A, B by virtue of also rotating about joints 13 and pins 12.

For restoring it from the collapsed to the extended position, structure 6 as shown comprises a number of hydraulic actuators 38 mounted, in the example shown, between each top and bottom pair of arms 16, 18 of each joint 20, at connecting pins 19, and which, when withdrawn/extended, provide for moving in relation to each other the arms 16, 18 connected to the opposite ends of each actuator.

It should be stressed that model-structure 6 as described above is purely indicative, and may differ widely in design with no effect on performance. For example, according to variations not shown, actuators 38 may be replaced by a single actuator connected to the opposite ends of cross members 10 and 11, or by one or more actuators forming part of apparatus 1; four-armed friction joints 20 may be replaced by twice as many

- 12 -

hydraulic friction joints, each having one arm 16 and one arm 18 arranged side by side in pairs on each portion 22 of frame 21; for achieving even greater articulation of structure 6, joints 25 of brackets 23
5 may also be in the form of hydraulic friction joints (Figure 4) similar to joints 20, thus enabling pairs of arms 16, 18 in each set to rotate about an axis E (Figure 3) perpendicular to respective rotation axis D of respective joint 20.

10 For better exploiting model-structure 6, apparatus 1 also comprises means for supporting structure 6 and defined, in the example shown, by a frame type slide 40 (Figures 1 and 2) mounted in fixed manner (or permitted to slide by releasing appropriate lock means) on a
15 supporting bed 41; means for selectively calibrating the sliding torque of each friction disk 32 of joints 20 and 13; and, if not provided on model-structure 6, at least one actuator for restoring structure 6, after impact, from the collapsed configuration to the same extended
20 configuration prior to impact.

In particular, said calibrating means comprise respective known valves 42 for regulating the hydraulic supply pressure of each hydraulic friction joint 13, 20 between a minimum zero value and a maximum value equal,
25 for example, to the head of a pump 43 supplying pressurized oil for activating friction joints 13, 20; means, consisting for example of known coiled tubes (not shown), for supplying said pressurized oil produced by

- 13 -

pump 43 to hydraulic friction joints 13, 20 via valves 42, and so enabling hydraulic connection while at the same time permitting relative movement of the various components of structure 6; a thrust device 46 for
5 "hammering", and so exerting predetermined dynamic stress on, structure 6; and means for displaying a quantity proportional to the sliding torque of each joint 13, 20 - in the example shown, a set of gauges 47 showing the supply pressure of each friction joint 13,
10 20, and mounted together with valves 42 on a console 48 fixed to bed 41.

In the example shown, device 46 is fitted integral with bed 41 (possibly in removable manner), and consists of a hammer or ram 49 powered by a known, e.g.
15 hydraulic, actuating device 50 by which model-structure 6, fixed to bed 41 by supporting slide 40, is subjected via hammer or ram 49 to dynamic stress similar to that produced by impact of structure 6 at a predetermined speed against a fixed obstacle.

20 According to the present invention, apparatus 1 and structure 6 are employed in a method for destructive impact testing vehicle components such as frame 2 by simulating real on-vehicle impact conditions of the test component. The first stage in the method consists in
25 fixing reusable model-structure 6 in the extended position to bed 41, after which joints 13, 20 of structure 6 are calibrated using device 46, also fixed to bed 41, as shown in Figures 1 and 2. More

- 14 -

specifically, the calibrating stage consists in so setting valves 42 as to supply friction joints 13, 20 with oil at predetermined pressures as required; structure 6 is then subjected, by hammer or ram 49 striking cross member 10, to sufficient impact to collapse it, while at the same time determining, using known, e.g. optical and/or electromechanical means (not shown), the dynamic collapse performance of structure 6 as a result of impact; and, finally, structure 6 is restored to the original extended configuration by adjusting friction disks 32 so that each presents a sliding torque of zero (i.e. the supply pressure of joints 13, 20 is zeroed by fully closing valves 42 or a main valve for cutting off supply by pump 43) and by immediately operating actuators 38.

At this point, the above operations are repeated in trial-and-error fashion, each time adjusting the supply pressure of each joint 13, 20 by means of respective valve 42, until the passage of structure 6 from the extended to the collapsed configuration as a result of the blow inflicted by hammer 49 is identical to the known performance of front body assembly 5 being simulated. When this is achieved, structure 6 is ready for use, after first assembling the test component.

The actual impact test may be performed on apparatus 1 using hammer 49, or in conventional manner by driving structure 6 against a fixed obstacle. For example, structure 6, still connected by extendible

- 15 -

hoses to valves 42 and pump 43 for pressurizing joints 13, 20, is removed from fixed slide 40 and mounted on an identical slide (not shown) movable along bed 41 or a similar bed of a conventional test station to the side of apparatus 1; the slide with structure 6 fitted with the test component is driven at predetermined speed against a known fixed stop (not shown) so as to collapse structure 6; the test component is recovered and examined; and, according to the present invention, structure 6 is restored to the original extended configuration (by zeroing the supply pressure of joints 13, 20 and operating actuators 38) ready for testing another similar or different component.

According to one characteristic of the above test method, joints 13, 20 are so designed that the maximum sliding torque of friction disks 32 is always less than the minimum value which, during impact testing or even the calibrating stage, would stress the load-bearing elements 10, 11, 16, 18, 21 of structure 6 over and above their yield point, thus preventing any possibility of damage to model-structure 6 during impact testing, and so enabling it to be reused any number of times. Moreover, by simply repeating the calibrating stage, the same model-structure 6 may be used for simulating the performance of different vehicle body structures 5, thus further enhancing the versatility and reducing the cost of the method according to the present invention.

CLAIMS

1) An apparatus for impact testing vehicle components, characterized by the fact that it comprises
5 a reusable trestle type model-structure designed, on impact, to switch from an extended to a collapsed configuration with the same dynamic performance as the front vehicle body assembly being simulated, the model-structure comprising a number of substantially
10 rigid, load-bearing elements articulated by means of friction elements with an adjustable sliding torque; the apparatus also comprising means for supporting the model-structure; means for selectively calibrating the sliding torque of each friction element to a
15 predetermined value above which the friction element permits relative rotation of the load-bearing elements connected by it, and hence collapse of the model-structure; and at least one actuator for restoring the model-structure, after impact, from the collapsed
20 configuration to the same extended configuration prior to impact; the model-structure being designed, at least in the extended configuration, to receive at least one vehicle test component.

2) An apparatus as claimed in Claim 1,
25 characterized by the fact that said friction elements are hydraulic friction elements; and by the fact that said calibrating means comprise respective valves for regulating the hydraulic supply pressure of each said

hydraulic friction element of the model-structure between a minimum zero value and a maximum value; and means for supplying the hydraulic friction elements with pressurized fluid via said valves.

5 3) An apparatus as claimed in Claim 1 or 2, characterized by the fact that said calibrating means comprise a thrust device for subjecting said model-structure, fixed to said supporting means, to predetermined dynamic stress of the type resulting from
10 impact; and means for displaying a quantity proportional to the sliding torque of each said friction element.

4) A method of impact testing vehicle components, characterized by the fact that it comprises the following stages:

15 - setting up a reusable model-structure for simulating the dynamic collapse performance of the vehicle of which the test component forms part; the model-structure being formed by connecting a number of substantially rigid, load-bearing elements in articulated manner by means of
20 friction elements with an adjustable sliding torque;
- so calibrating said model-structure as to enable it, upon impact, to switch from an extended to a collapsed configuration with the same dynamic performance as the front vehicle body assembly being simulated; said
25 calibrating stage being performed by trial and error, by subjecting the model-structure to a predetermined amount of dynamic stress, determining the dynamic collapse performance of the structure, restoring the structure to

the extended configuration, and separately adjusting the sliding torque of each friction element until the dynamic collapse performance of the model-structure corresponds with the known performance of the body assembly being simulated;

- fitting the test component to the extended model-structure, and conducting a normal impact test using the model-structure in lieu of the vehicle to which the test component is to be mounted.

5) A method as claimed in Claim 4, characterized by the fact that, following impact testing, the model-structure is restored to the extended configuration for further testing.

6) A method as claimed in Claim 5, characterized by the fact that the extended configuration is restored by so adjusting the friction elements that each presents a zero sliding torque, and by acting on at least two opposite said load-bearing elements by means of an actuator so as to produce a relative movement of the two load-bearing elements.

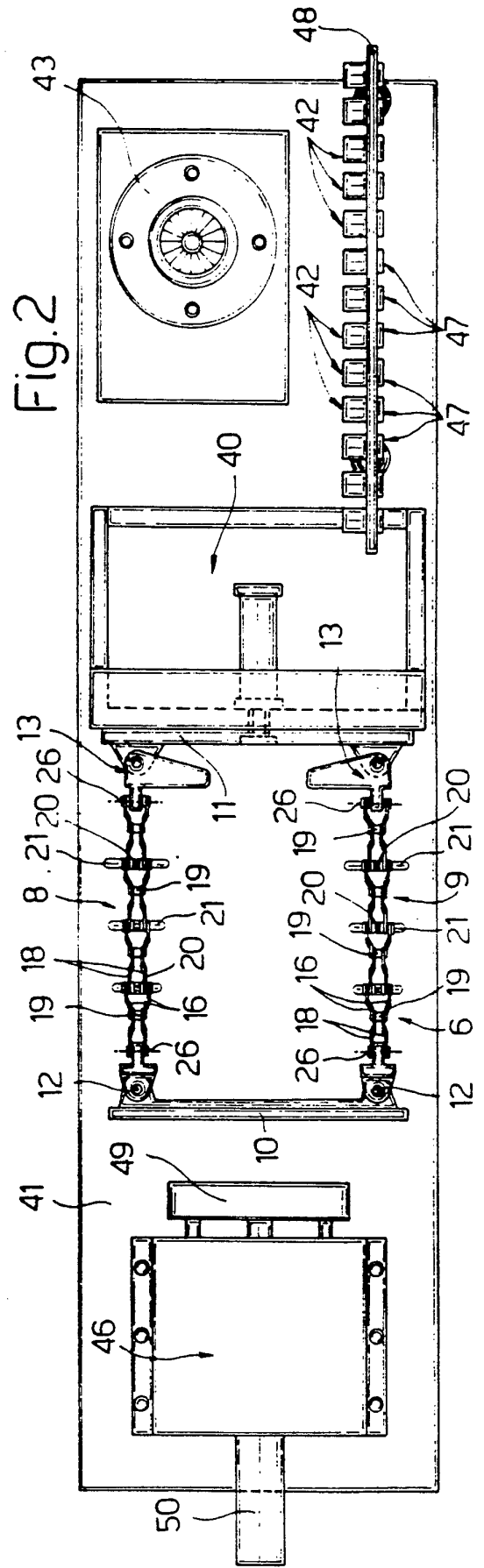
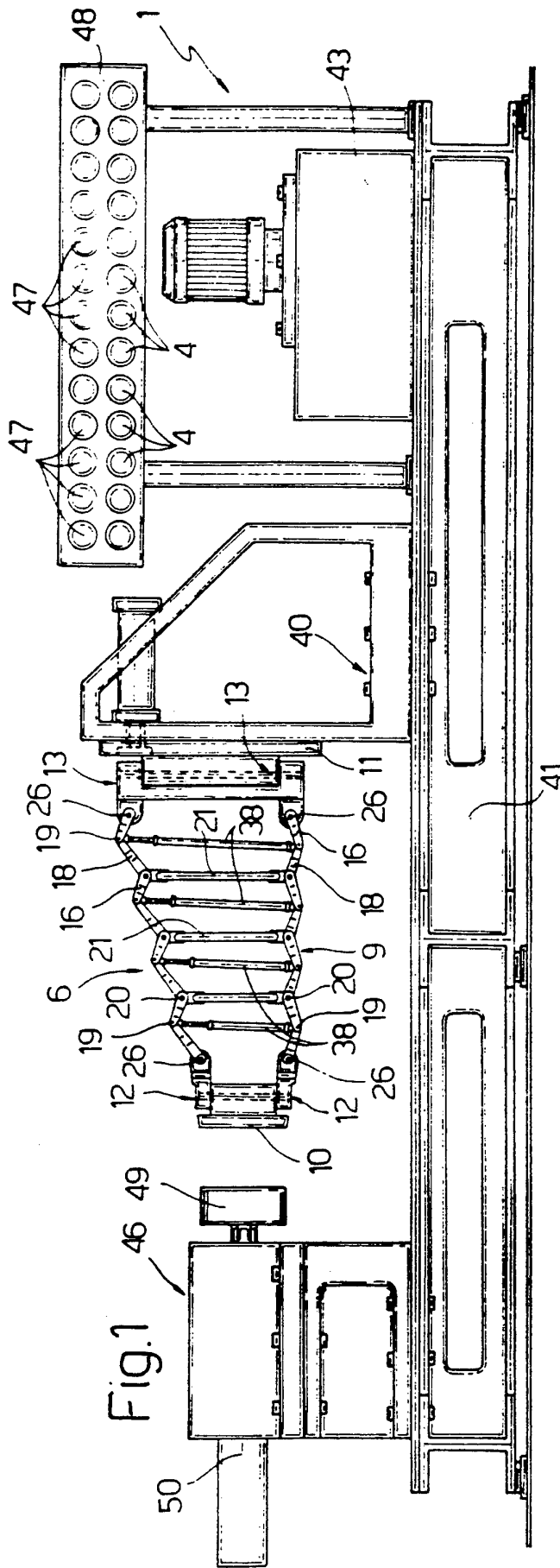
7) A method as claimed in Claim 4, 5 or 6, characterized by the fact that the friction elements are so adjusted as to present a maximum sliding torque below the value which, during impact testing, would stress the load-bearing elements over and above their yield point.

8) A reusable model-structure for simulating, during impact testing, the dynamic collapse performance of a vehicle front body assembly; characterized by the

fact that it comprises a first and second trestle type side member collapsible accordion fashion, located parallel to each other, and each comprising a number of arms hinged in series with one another by respective articulating means, and a number of hydraulic friction joints constituting at least some of the articulating means.

9) A model-structure as claimed in Claim 8, characterized by the fact that each said hydraulic joint is connected by a respective pressure regulating valve to pressurized fluid supply means, so that each presents an adjustable sliding torque below which any relative movement of the connected arms is prevented, and above which the arms are permitted to rotate in relation to one another with a predetermined amount of friction and about their mutual hinge axes.

10) An apparatus, method and reusable model-structure for impact testing vehicle components, substantially as described and illustrated herein with reference to the accompanying drawings.



2 / 5

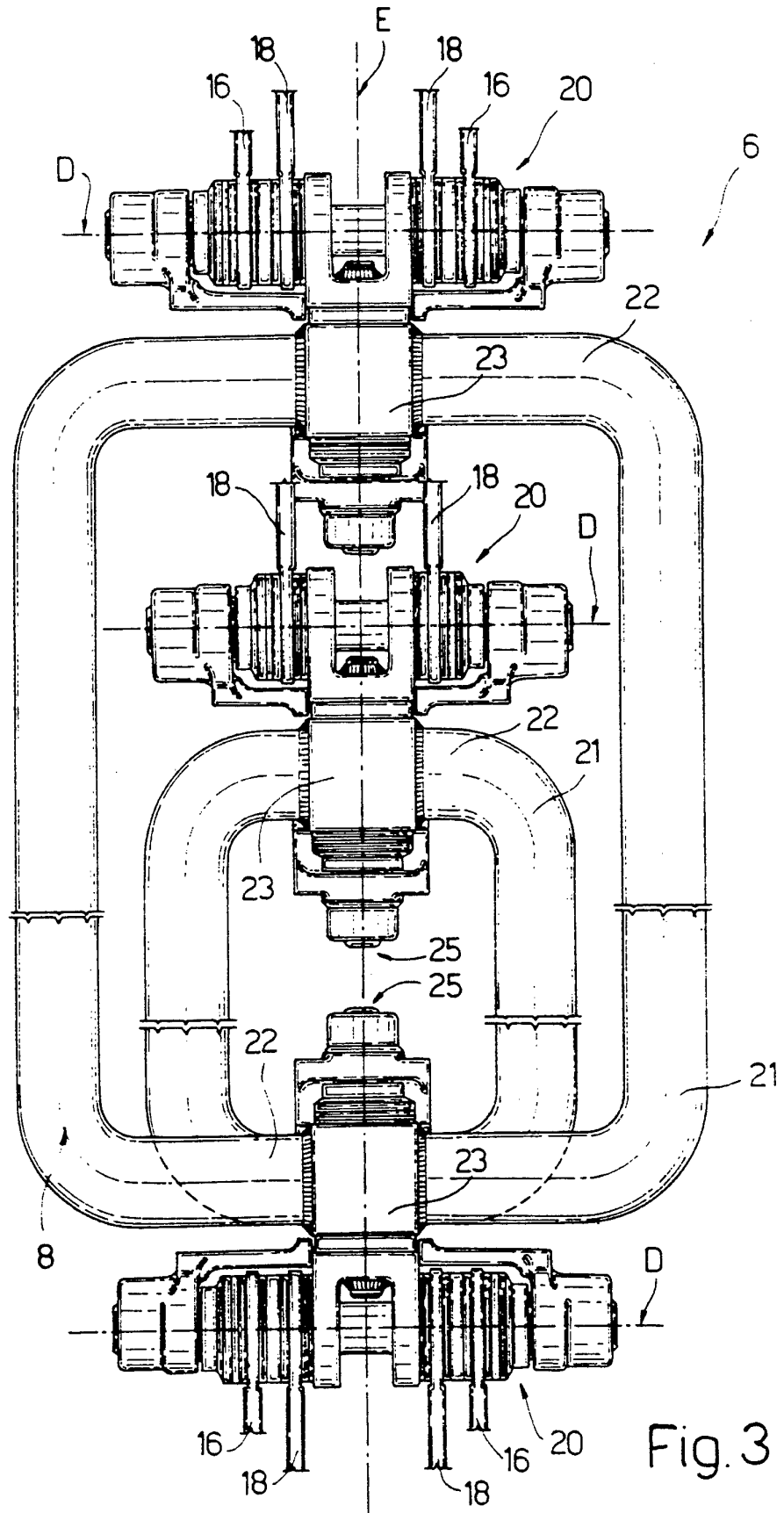


Fig. 3

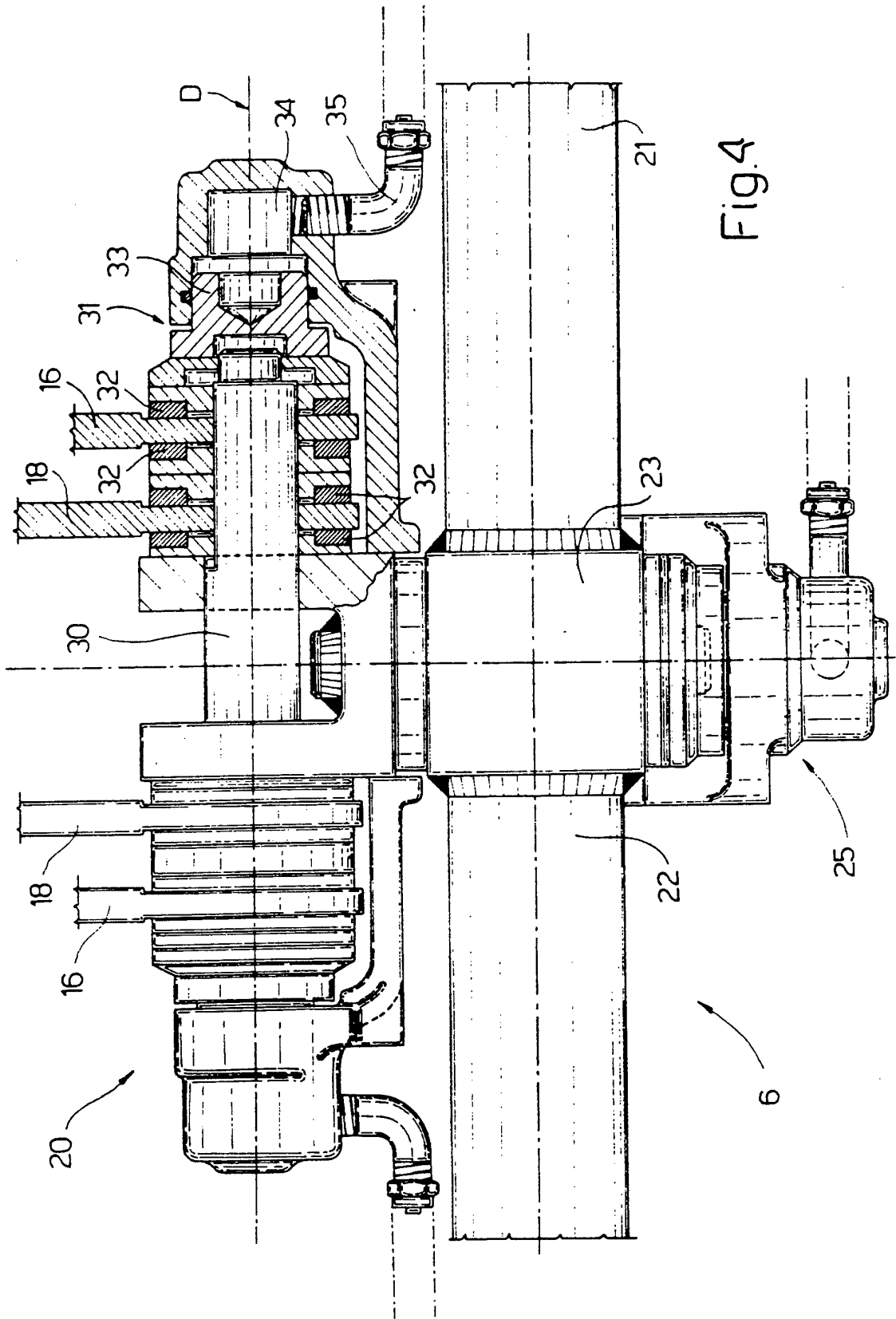
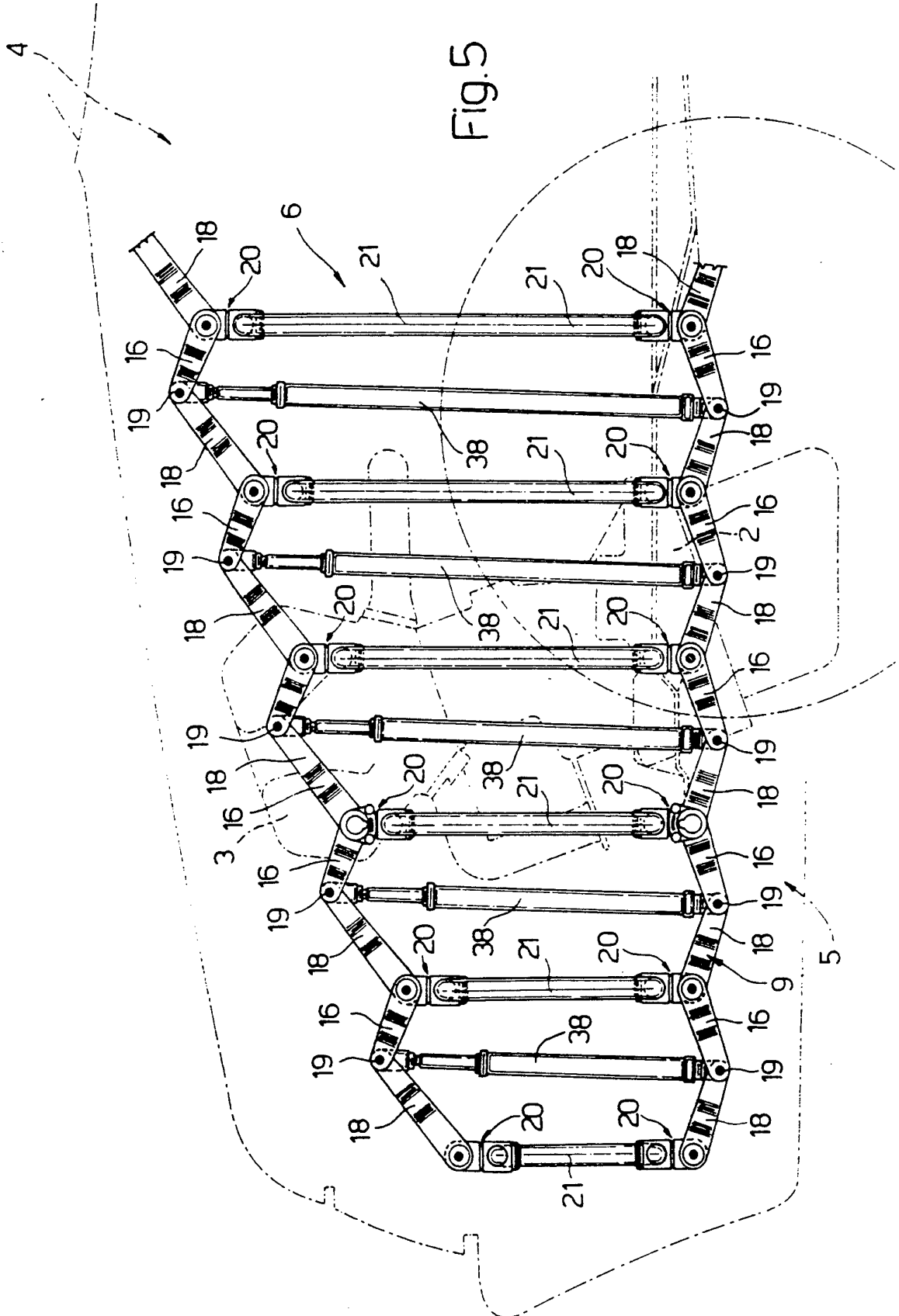


FIG. 5



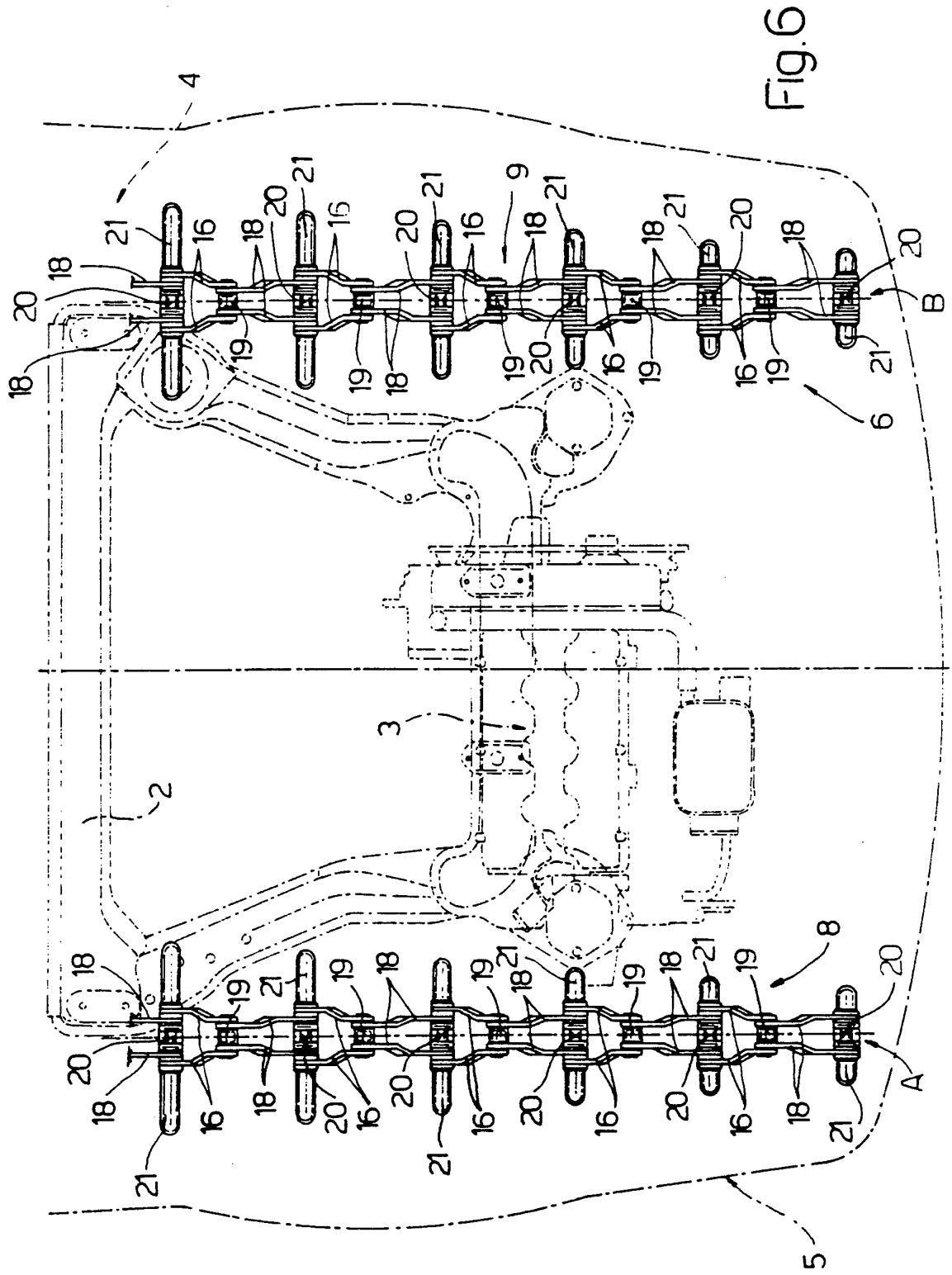


Fig. 6

INTERNATIONAL SEARCH REPORT

Intern. Application No

PCT/IT 94/00091

<p>A. CLASSIFICATION OF SUBJECT MATTER IPC 5 G01M17/00</p>		
<p>According to International Patent Classification (IPC) or to both national classification and IPC</p>		
<p>B. FIELDS SEARCHED</p>		
<p>Minimum documentation searched (classification system followed by classification symbols) IPC 5 G01M</p>		
<p>Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched</p>		
<p>Electronic data base consulted during the international search (name of data base and, where practical, search terms used)</p>		
<p>C. DOCUMENTS CONSIDERED TO BE RELEVANT</p>		
Category °	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	EP,A,0 474 432 (ENERGY ABSORPTION SYSTEMS) 11 March 1992 see claims 1,13; figure 9 ---	1-10
P,A	DE,A,43 30 122 (MESSRING PRÜFANLAGEN) 10 March 1994 see column 2, line 29 - column 5, line 16; figure 9 -----	1-10
<p><input type="checkbox"/> Further documents are listed in the continuation of box C. <input checked="" type="checkbox"/> Patent family members are listed in annex.</p>		
<p>° Special categories of cited documents :</p>		
<p>"A" document defining the general state of the art which is not considered to be of particular relevance</p>		<p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p>
<p>"E" earlier document but published on or after the international filing date</p>		<p>"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone</p>
<p>"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p>		<p>"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.</p>
<p>"O" document referring to an oral disclosure, use, exhibition or other means</p>		<p>"&" document member of the same patent family</p>
<p>"P" document published prior to the international filing date but later than the priority date claimed</p>		
<p>Date of the actual completion of the international search 17 October 1994</p>		<p>Date of mailing of the international search report 21.10.94</p>
<p>Name and mailing address of the ISA European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+ 31-70) 340-2040, Tx. 31 651 epo nl, Fax (+ 31-70) 340-3016</p>		<p>Authorized officer Mucs, A</p>

INTERNATIONAL SEARCH REPORT

International Application No

PCT/IT 94/00091

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
EP-A-0474432	11-03-92	US-A- 5112028 AU-B- 635152 AU-A- 8347291 CA-A, C 2050227 JP-A- 6073714	12-05-92 11-03-93 12-03-92 05-03-92 15-03-94
DE-A-4330122	10-03-94	NONE	