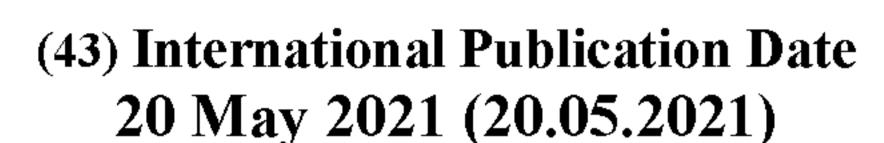
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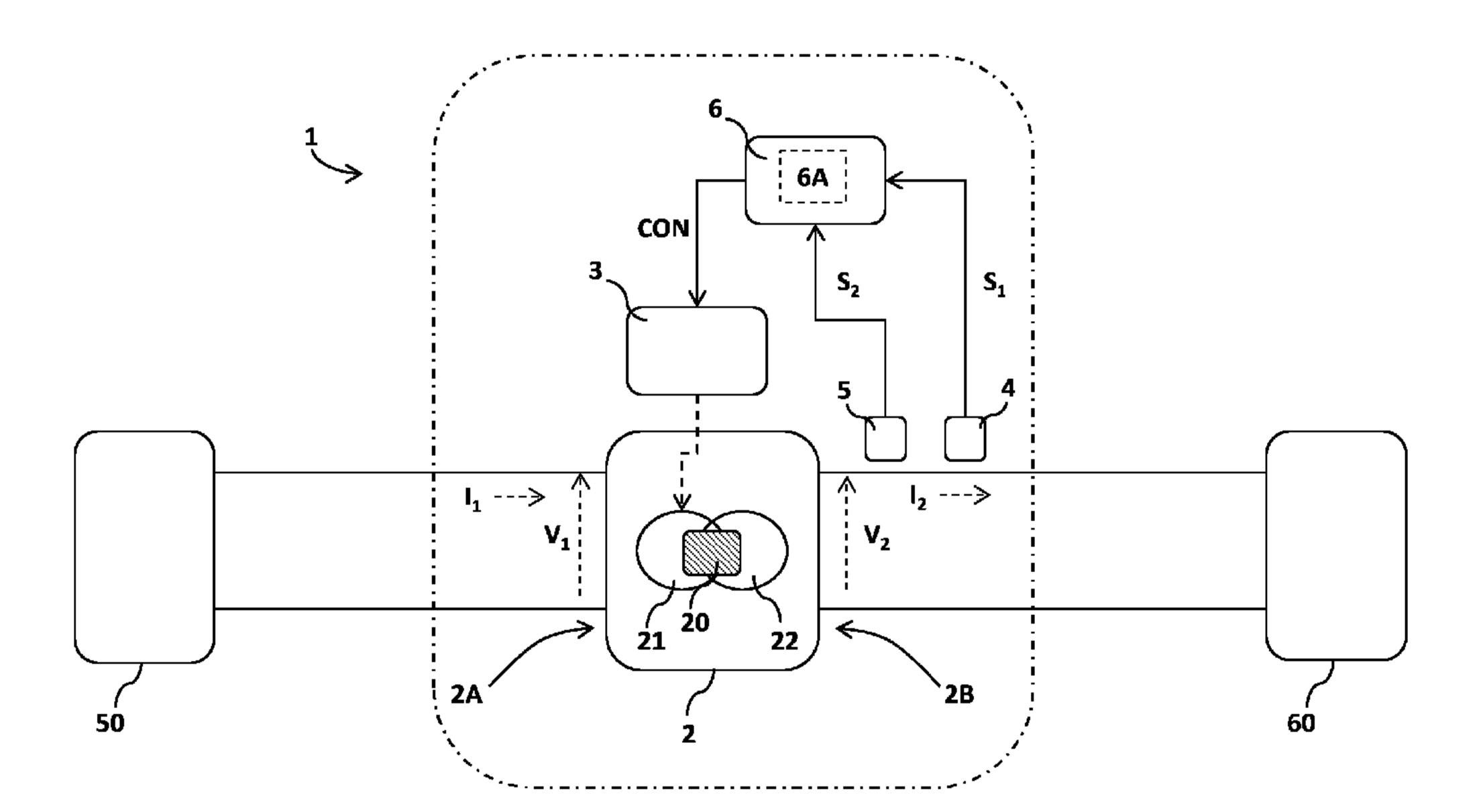


FIG. 1

(57) **Abstract:** A transformer assembly (1) for electric grids comprising: - an electric transformer (2) comprising a magnetic core (20), a first side (2A) including one or more first windings (21) enchained with said magnetic core and adapted to be electrically connected to a first grid section (50) and a second side (2B) including one or more second windings (22) enchained with said magnetic core and adapted to be electrically connected to a second grid section (60); - a tap changer (3) operatively associated with said electric transformer (2) to vary the number of turns enchained with said magnetic core (20) for said first windings (21). The transformer assembly comprises a control unit (6) operatively coupled with said tap changer (3) to control the operation of said tap changer, said control unit being configured to: - acquire input data (IN) indicative of an electrical connectivity condition of said second grid section (60) with said second windings (22); - basing on said input data (IN), determine whether said transformer (2) is in a load condition or in a no-load



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condition; - if said transformer (2) is in a no-load condition, command said tap changer to set a maximum available number of turns for said first windings (21).

# A TRANSFORMER ASSEMBLY FOR ELECTRIC GRIDS AND A RELATED CONTROL METHOD

### **DESCRIPTION**

The present invention relates to a transformer assembly for electric grids, e.g. electric power transmission and distribution grids.

In a further aspect the present invention relates to a method for controlling a tap changer included in said transformer assembly.

Electric transformers are widely used in electric grids to transmit electric power between grid sections operating at different nominal voltages.

As it is known, transformers are subject to power losses in operation.

Power losses generally include the so-called "load power losses", arising only when the voltage transformer operates in a so-called "load condition" (i.e. it is electrically connected with a corresponding grid section at the primary side and with a corresponding grid section at the secondary side), and the so-called "no-load power losses", which are always present when a voltage transformer operates.

No-load power losses can be observed when a transformer is in a so-called "no-load condition", i.e. it is electrically connected with a corresponding grid section at the primary side and it is electrically disconnected from a corresponding grid section at the secondary side. In this situation, due to the induced magnetic flux generated by the primary windings, a current (the so called "no-load current") circulates along the magnetic core even if the secondary windings of the transformer are disconnected from any electric load. Said no-load current generates power losses in the magnetic core and along the primary windings, which are strongly dependent on the magnetic flux.

No-load power losses represent a relevant issue, particularly when the transformer is frequently subject to a no-load condition, as it occurs when it is installed in renewable energy production facilities or in electric grids provided with redundancy systems.

As an example, energy dissipation costs due to no-load power losses in a medium-size power transformer intended for use in a renewable energy production facility are normally estimated in the order of thousands EUR/kW per year.

A simple solution to reduce no-load power losses would be designing the magnetic core of the transformer in such a way to generate a lower magnetic flux. However, such an approach would unacceptably limit the performances of the transformer where this latter is in a load condition, in practice when exploiting its major function of transferring electric power between different grid sections.

The main aim of the present invention is providing a transformer assembly for electric grids, which allows solving or mitigating the technical issues evidenced above.

Within this aim, an object of the present invention is providing a transformer assembly, in which it is possible to reduce no-load power losses effectively, when the electric transformer operates in a no-load condition.

A further object of the present invention is providing transformer assembly that can be industrially realized at competitive costs.

These aim and objects are achieved by a transformer assembly for electric grids, according to the following claim 1 and the related dependent claims.

In a general definition, the transformer assembly, according to the invention, comprises:

- an electric transformer comprising a magnetic core, a first side including one or more first windings enchained with said magnetic core and adapted to be electrically connected to a first grid section and a second side including one or more second windings enchained with said magnetic core and adapted to be electrically connected to a second grid section;
- a tap changer operatively associated with said electric transformer to vary the number of turns enchained with said magnetic core for said first windings or for said second windings;

- a control unit operatively coupled with said tap changer to control the operation of said tap changer.

-

The control unit is configured to:

- acquire input data indicative of an electrical connectivity condition of said second grid section with said second windings;

- basing on said input data, determine whether said transformer is in a load condition or in a no-load condition;

- if said transformer is in a no-load condition, command said tap changer to set a maximum available number of turns for said first windings or for said second windings.

Preferably, said control unit is configured to control said tap changer in such a way to carry out a regulation of a second voltage provided at said second windings, if said transformer is in a load condition.

Preferably, the transformer assembly, according to the invention, comprises:

- current sensing means adapted to provide first sensing signals indicative of a second current circulating along said second windings;
- voltage sensing means adapted to provide second sensing signals indicative of a second voltage provided at said second windings.

Conveniently, said control unit is operatively coupled with said voltage sensing means.

Preferably, said control unit is configured to acquire said input data by processing the first sensing signals provided by said current sensing means.

Preferably, the transformer assembly, according to the invention, comprises signalling means adapted to receive the first sensing signals provided by said current sensing means and provide third sensing signals indicative of the level of the current circulating along said second windings.

Preferably, said control unit is configured to acquire said input data by processing said third

sensing signals.

Preferably, said signalling means include an electronic relay.

Preferably, said transformer assembly comprises a suitable Station Service Voltage Transformer (SSVT) for providing an auxiliary power supply, e.g. for feeding said control unit. Said SSVT can be a capacitive voltage transformer (typically oil-filled insulated) or an inductive voltage transformer (typically gas insulated).

In a further aspect, the present invention relates to an electric grid, according to the following claim 8.

In a further aspect, the present invention relates to a method for controlling a tap changer included in a transformer assembly as illustrated above, according to the following claim 9 and the related dependent claims.

The method, according to the invention, comprises the following steps:

- acquiring input data indicative of an electrical connectivity condition of said second grid section with said second windings;
- basing on said input data, determining whether said transformer is in a load condition or in a no-load condition;
- if said transformer is in a no-load condition, commanding said tap changer to set a maximum available number of turns for said first windings or for said second windings.

Preferably, the method, according to the invention, comprises the following step:

- controlling said tap changer in such a way to carry out a regulation of a second voltage provided at said second windings, if said transformer is in a load condition.

Preferably, said step of acquiring said input data includes processing the first sensing signals provided by said current sensing means.

Preferably, said step of acquiring said input data includes processing the third sensing signals

provided by said signalling means.

Further characteristics and advantages of the present invention will be more apparent with reference to the description given below and to the accompanying figures, provided purely for explanatory and non-limiting purposes, wherein:

- Fig. 1 schematically illustrates a transformer assembly, according to an embodiment of the present invention;
- Fig. 2 schematically illustrates a transformer assembly, according to another embodiment of the present invention;
- Fig. 3 schematically illustrates a method for controlling a tap changer included in the transformer assembly, according to the present invention.

With reference to the aforesaid figures, the transformer assembly 1, according to the invention, will now be described in details.

The transformer assembly 1 is particularly adapted for use in electric grids, more particularly in electric power transmission and distribution grids.

The transformer assembly 1 comprises an electric transformer 2 basically operating as a voltage transformer configured to transmit electric power between different grid sections operating at different nominal voltages.

The transformer 2 comprises a magnetic core 20, a first side 2A including one or more first windings 21 enchained with the magnetic core 20 and adapted to be electrically connected to a first grid section 50 and a second side 2B including one or more second windings 22 enchained with the magnetic core 20 and adapted to be electrically connected to a second grid section 60.

In operation, the transformer 2 shows a first voltage  $V_1$  and a first current  $I_1$  at the first windings 21 and a second voltage  $V_2$  and a second current  $I_2$  at the second windings 22.

Preferably, the first side 2A and the first windings 21 respectively form the primary side and the primary windings of the electric transformer 2 while the second side 2B and the second

windings 22 respectively form the secondary side and the secondary windings of the transformer 2.

The transformer 2 is preferably adapted to transfer electric power from the first grid section 50 operating at a higher nominal voltage (e.g. 100 kV) to the second grid section 60 operating at a lower nominal voltage (e.g. 30 kV).

Therefore, preferably, the transformer 2 receives a first voltage  $V_1$  at the first windings 21, which is higher than a second voltage  $V_2$  provided at the second windings 22. The first windings 21 will thus preferably have a higher number of turns than the second windings 22.

A second current I<sub>2</sub> circulates along the secondary windings 22 when the transformer 2 is in a load condition. When the transformer 2 operates in a no-load condition (no electric loads are present), such a second current I<sub>2</sub> is null.

For the sake of clarity, it is specified that:

- the transformer 2 is in a "load condition" when there is an equivalent electric load electrically with the second windings 22, i.e. the second grid section 60 is electrically connected with the second windings 22;
- the transformer 2 is in a "no-load condition" when there are no electric loads electrically connected with the second windings 22, i.e. the second grid section 60 is electrically disconnected from the second windings 22.

The grid sections 50, 60 may include a single electric phase (as shown in the cited figures for simplicity) or, more frequently, multiple electric phases (typically three electric phases).

The transformer 2 (and thus the voltages  $V_1$ ,  $V_2$  and the currents  $I_1$ ,  $I_2$ ) may thus be of single-phase type (as shown in the cited figures) or multiple-phase type (typically of three-phase type).

In principle, the transformer 2 may be of any type adapted for use in electric grids. As an example, the transformer 2 may be a power transformer, a distribution transformer or an isolation transformer, according to the needs.

The electric transformer 2 may be industrially manufactured according to solutions of known type. Therefore, hereinafter, it will be described only in relation to the aspects relevant to the invention, for the sake of brevity.

The transformer assembly 1 further comprises a tap changer 3 operatively associated with the electric transformer 2 at the first windings 21 or at the second windings 22.

In general, the tap changer 3 is adapted to vary the number of turns enchained with the magnetic core 20 for the first windings 21 or the second windings 22. In this way, it acts on the turn ratio of the transformer 2 in order to maintain (when first voltage V1 is varying at the first winding 21) a desired second voltage V2 at the second windings 22 (CFVV – Constant Flux Voltage Variation) or it acts in order to vary the magnetic flux circulating along the magnetic core, so consequently varying the second voltage V2 at the second windings 22 (VFVV – Variable Flux Voltage Variation).

According to preferred embodiments of the invention, the tap changer 3 is arranged in such a way to vary the number of turns of the first windings 21, which are enchained with the magnetic core 20. In the following description, a particular reference will be made to this solution (see figures 1-2), for the sake of simplicity.

According to other embodiments of the invention, however, the tap changer 3 may be arranged in such a way to vary the number of turns of the second windings 22, which are enchained with the magnetic core 20.

According to preferred embodiments of the invention, the tap-changer 3 is configured to operate as an on-load tap changer (OLTC). In this way, it is not necessary to electrically disconnect the transformer 2 from both first and second grid sections to operate the tap changer 3.

Preferably, the tap-changer 3 comprises a plurality of connection points (taps) with the first windings 21 (or the second windings 22) of the transformer 2. Each tap conveniently allows a certain number of additional turns to be selected for the first windings 21 (or the second

windings 22).

In principle, the tap changer 3 may be of any type adapted for use in electric power grids.

As an example, the tap-changer 3 may be of mechanical type. In this case, it will comprise a tap selector mechanism capable of moving one or more movable contacts couplable with corresponding taps to electrically connect in a selective manner said taps with the transformer windings. The tap selector mechanism is conveniently moved by a kinematic chain that is in turn actuated by a actuation unit (e.g. a motorized unit). Said actuation unit is conveniently controllable through suitable control signals.

As a further example, the tap-changer 3 may be of electronic type. In this case, it will comprise suitable power electronics circuits including power electronic switches (such as transistor or thyristor) capable of electrically connecting in selective manner said taps with the transformer windings. Said power electronic circuits may be conveniently driven by suitable control signals.

As a further example, the tap-changer 3 may be of hybrid type. In this case, it will comprise both mechanical and electronic arrangements to electrically connect in a selective manner above-mentioned taps with the transformer windings.

In general, the tap changer 3 may be industrially manufactured according to solutions of known type. Therefore, hereinafter, it will be described only in relation to the aspects relevant to the invention, for the sake of brevity.

The transformer assembly 1 comprises a control unit 6 operatively coupled with the tap changer 3 to control the operation of this latter.

If the tap changer 3 is of mechanical type, the control unit 6 can control the operation of the tap changer 3 by sending suitable control signals CON to the actuation unit actuating the mechanic arrangements of the tap changer.

If the tap changer 3 is of electronic type, the control unit 6 can control the operation of the tap

changer 3 by sending suitable control signals CON to power electronic circuits (in particular to the power switches) of the tap changer.

If the tap changer 3 is of hybrid type, the control unit 6 can control the operation of the tap changer 3 by sending suitable control signals CON to the actuation unit and to the power electronic circuits of the tap changer.

The control unit 6 is conveniently provided with data processing resources 6A, preferably of digital type, e.g. including one or more microprocessors capable of executing software instructions stored or storable in a storage medium (e.g. a memory of said control unit). The control unit 6 can thus carry out its functionalities (for example the functionalities described in the following) by executing suitable sets of software instructions stored in a memory.

The control unit 6 is preferably arranged on board the tap changer 3. In this case, the transformer assembly 1 may include suitable power supply arrangements (not shown) to feed the control unit 6.

According to other embodiments of the invention, however, the control unit 6 may be arranged in a remote location with respect to the tap changer 3. For example, it may be part of a remote suitable control panel or control platform.

According to preferred embodiments of the invention, the transformer assembly 1 comprises current sensing means 4 adapted to provide first sensing signals  $S_1$  indicative of the second current  $I_2$  circulating along the second windings 22 of the transformer and voltage sensing means 5 adapted to provide second sensing signals  $S_2$  indicative of the second voltage  $V_2$  at the second windings 22 of the transformer.

Preferably, the current sensing means 4 comprise a current sensor (e.g. a current transformer or a resistive shunt circuit) for each electric phase of the second windings 22 of the transformer.

Preferably, the current sensing means 4 are operatively coupled with the control unit 6, so that this latter can receive and process the first sensing signals  $S_1$ .

Preferably, the voltage sensing means 5 comprise a voltage sensor (e.g. a capacitive sensor or a resistive shunt circuit) for each electric phase of the second windings 22 of the transformer.

Preferably, the voltage sensing means 5 are operatively coupled with the control unit 6, so that this latter can receive and process the second sensing signals  $S_2$ .

An important aspect of the invention resides in that the control unit 6 is capable of carrying out control functionalities of the tap changer 3, which allow remarkably reducing no-load power losses, when the transformer 2 is a no-load condition.

A further important aspect of the invention resides in that the control unit is capable of carrying out different control functionalities (or control logics) of the tap changer 3, depending on whether the transformer 2 in a load-condition or in a no-load condition.

As it will be better emerging from the following, this solution allows remarkably improving the performances of the transformer 2, both when this latter is in a load condition and in a noload condition.

According to the invention, the control unit 6 is configured to acquire input data IN indicative of an electrical connectivity condition of the second grid section 60 with the second windings 22 of the transformer.

Input data IN are indicative of whether the second grid section 60 is electrically connected or not with the second windings 22 of the transformer.

According to possible embodiments of the invention, the control unit 6 is configured to acquire the input data IN by directly processing the first sensing signals S<sub>1</sub> provided by the current sensing means 4. To this aim, the data processing means 6A of the control unit 6 may conveniently carry out simple detection algorithms of known type.

According to preferred embodiments of the invention (figure 2), the transformer assembly 1 comprises signalling means 7 adapted to receive the first sensing signals S<sub>1</sub> provided by the

current sensing means 4 and provide third sensing signals  $S_3$  indicative of the level of the second current  $I_2$  circulating along the second windings 22. Conveniently, the third sensing signals  $S_3$  may be logic signals indicative of whether the second current  $I_2$  circulating along the second windings 22 is null or not.

Preferably, the signalling means 7 comprise an electronic relay, such as a minimum current relay.

According to these embodiments of the invention, the control unit 6 is operatively coupled with the signalling means 7 to receive the third sensing signals S<sub>3</sub>.

Conveniently, the control unit 6 is adapted to acquire the input data IN by suitably processing the third sensing signals  $S_3$  (figure 3) and, possibly, the first sensing signals  $S_1$  described above.

The control unit 6 thus determines whether the transformer 2 is in a load condition or in an unload condition by determining whether the second grid section 60 is electrically connected or disconnected with the second windings 22 of the transformer 2.

According to the invention, the control unit 6 determines whether the transformer 2 is in a load condition or in a no-load condition basing on the acquired input data IN.

In order to carry out the above-mentioned determination step, the control unit 6 suitably processes the acquired input data IN. To this aim, the data processing means 6A of the control unit 6 may conveniently carry out simple determination algorithms of known type.

If the transformer 2 is in a no-load condition (second grid section 60 electrically disconnected from the second windings 22), the control unit 6 commands the tap changer 3 to set the maximum available number of turns for the first windings 21 (or for the second windings 22). Thus, when the transformer 2 is in a no-load condition, the control unit 6 controls the tap changer 3 according to a first control logic, which is basically aimed at reducing power losses without considering the behavior of the second voltage V<sub>2</sub> provided by the transformer 2 at the second windings 22.

The above-mentioned first control logic is based on the observation that, in the transformer 2, the magnetic flux depends on the volt per turn ratio (V/N), according to the following relation:

$$\frac{V}{N} = \frac{V_1}{N_1} = \frac{V_2}{N_2} = 4.44 * f * Afe * B$$

where f is the grid frequency, Afe is a constant, B is the magnetic flux,  $V_1$  is the first voltage at the first windings 21,  $V_2$  is the second voltage at the second windings 22,  $N_1$  is the number of turns of the first windings 21 and  $N_2$  is the number of turns of the second windings 22 and V/N is the voltage ratio of the transformer.

It is evident from the above relation that setting the maximum available number of turns for the first windings 21 (or for the second windings 22) necessarily implies a reduction of magnetic flux B.

On the other hand, such a reduction of the magnetic flux B entails a remarkable reduction of the power losses, as these latter strongly depend on the magnetic flux.

Therefore, when the control unit 6 commands the tap changer 3 to set a maximum available number of turns for the first windings 21 (or for the second windings 22) with the transformer 2 in a no-load condition, a remarkable reduction of power losses is obtained.

According to preferred embodiments of the invention, if the transformer 2 is in a load condition (second grid section 60 electrically connected with the second windings 22), the control unit 6 controls the tap changer 6 in such a way to carry out a voltage regulation of the second voltage  $V_2$  at the second windings 22.

Thus, when the transformer 2 is in a load condition, the control unit 6 controls the tap changer 3 according to a second control logic, which is completely different from the first control logic illustrated above.

Such a second control logic is basically aimed at regulating the second voltage V<sub>2</sub> provided by the transformer 2 at the second windings 22, so that an optimal power transfer between the first grid section 50 and the second grid section 60 is constantly ensured.

Preferably, the control unit 6 commands the tap changer 3 to set a number of turns for the first windings 21 (or for the second windings 22) with the transformer 2, which depends on the detected second voltage V<sub>2</sub> at the second windings 22, when the transformer 2 is in a load condition.

Preferably, the control unit 6 processes the second sensing signals S<sub>2</sub> received from the second sensing means 5 and, basing on the voltage detection data so obtained, commands the tap changer 3 to vary (if necessary) the number of turns enchained with the magnetic core 20 for said first windings 21 (or for the second wings 22).

Voltage regulation can be carried out in a known manner, for example in according to a method compliant to international regulations (e.g. IEC60076.1).

Conveniently, voltage regulation may involve a range of  $\pm 20\%$  of the nominal value of the second voltage  $V_2$  at the second windings 22 and it can be performed in a plurality of steps (e.g. from 9 to 35 steps) depending on the type of the changer 3.

Conveniently, voltage regulation may be carried out 10 to 20 times a day in normal applications, depending on fluctuations of the second voltage  $V_2$ , which may due to changes in the operating conditions of the grid sections 50 and 60.

The transformer assembly, according to the invention, may be subject to variants falling within the scope of the invention.

As mentioned above, the tap changer 3 may be arranged in such a way to vary the number of turns of the second windings 22, which are enchained with the magnetic core 20. It is evidenced that, also in this case, the control unit 6 implements the same control logics illustrated above to control the operation of the tap changer 3, when the transformer 2 is in a no-load condition or in a load condition.

In the embodiments in which the control unit 6 is arranged on board or in proximity of the tapchanger 3, electronic circuitry capable of deriving an auxiliary power supply from the first windings 21 or the second windings 22 of the transformer 2 may be suitably arranged (e.g.

according to solutions of known type).

In these embodiments of the invention, a reduction of the auxiliary power supply of the control unit 6 may occur when the tap changer 3 sets a maximum available number of turns for the first windings 21 (or for the second windings 22) as illustrated above.

It has been seen that such an inconvenient may be suitably overcome by arranging a suitable Station Service Voltage Transformer (SSVT) for providing an auxiliary power supply, e.g. to feed the control unit 6. Said SSVT (not shown) can be a capacitive voltage transformer (typically oil-filled insulated) or an inductive voltage transformer (typically gas insulated).

In a further aspect, the present invention relates to a method 100 for controlling the tap changer 3 included in the transformer assembly 1 described above (figure 3).

The method 100 is suitable for being implemented in practice by the data processing means 6A of the control unit 6, which can conveniently carry out a suitable set of software instructions to this purpose.

The method 100, according to the invention, comprises a step 101 of acquiring input data IN indicative of a condition of electrical connection of the second grid section 60 with the second windings 22.

According to some embodiments of the invention (figure 1), the step 101 of acquiring the input data IN includes processing the first sensing signals S1 provided by the current sensing means 4.

According to some embodiments of the invention (figure 2), the step 101 of acquiring the input data IN includes processing the third sensing signals S<sub>3</sub> provided by the signalling means 7.

The method 100, according to the invention, comprises a step 102 of determining whether the second grid section 60 is electrically connected with or disconnected from the second windings 22, basing on the acquired input data IN.

The method 100, according to the invention, comprises a step 103 of commanding the tap changer 3 to set a maximum number of turns for the first windings 21 (or for the second windings 22), if the second grid section 60 is electrically disconnected from the second windings 22.

Preferably, the method 100, according to the invention, comprises a step 104 of controlling the tap changer 3 in such a way to carry out a regulation of the second voltage V<sub>2</sub> provided at the second windings 22, if the second grid section 60 is electrically connected with the second windings 22.

Preferably, in the step 104 of the method 100, the tap changer 3 is commanded to set a number of turns for the first windings 21 (or for the second windings 22) with the transformer 2, which depends on the detected second voltage  $V_2$  at the second windings 22.

The transformer assembly, according to the invention, provides relevant advantages with respect to corresponding systems of the state of the art.

The above-illustrated improved control functionalities of the tap changer 3 allow obtaining a strong reduction of power losses of the transformer 2, when this latter is in a no-load condition.

Experimental tests have shown that power losses can be reduced up to 48% (with respect to traditional solutions of the state of the art) when the transformer 2 operates in a no-load condition (with a magnetic flux excursion down to -20% of the nominal value), depending on the type of the transformer and type of network's fluctuation range.

Reduction of power losses can reach about 65% (with respect to traditional solutions of the state of the art) when the transformer 2 operates in a no-load condition (with a magnetic flux excursion down to -40% of the nominal value), again depending on the type of the transformer and type of network's fluctuation range.

Obviously, the above-mentioned features allow simplifying the management of the operating life of the transformer 2 with a remarkable reduction of overall industrial costs.

As an example, energy cost savings have been estimated in the order of several thousands EUR per year for a medium-size power transformer intended for use in a renewable energy production facility.

The solution provided by the invention further allows simplifying the design of the transformer 2 without having strong constraints for its behavior in no-load conditions. In this situation, in fact, power losses are reduced by properly controlling the tap changer 3 according to the first control logic illustrated above.

The magnetic core 20 of the transformer 2 can thus be designed in such a way to optimize the circulating magnetic flux in such a way that an optimal electric power transfer between different sides of the transformer 2 is obtained, when this latter is in a load condition.

The transformer assembly 1 has a simple and compact structure and it may be easily arranged, even for retrofitting purposes.

The transformer assembly 1 can be easily manufactured at industrial level with production costs quite competitive with respect to traditional devices of the same type.

## **CLAIMS**

- 1. A transformer assembly (1) for electric grids comprising:
  - an electric transformer (2) comprising a magnetic core (20), a first side (2A) including one or more first windings (21) enchained with said magnetic core and adapted to be electrically connected to a first grid section (50) and a second side (2B) including one or more second windings (22) enchained with said magnetic core and adapted to be electrically connected to a second grid section (60);
  - a tap changer (3) operatively associated with said electric transformer (2) to vary the number of turns enchained with said magnetic core (20) for said first windings (21);
  - a control unit (6) operatively coupled with said tap changer (3) to control the operation of said tap changer;

characterised in that said control unit (6) is configured to:

- acquire input data (IN) indicative of an electrical connectivity condition of said second grid section (60) with said second windings (22);
- basing on said input data (IN), determine whether said transformer (2) is in a load condition or in a no-load condition;
- if said transformer (2) is in a no-load condition, command said tap changer to set a maximum available number of turns for said first windings (21).
- 2. Transformer assembly, according to claim 1, characterised in that said control unit (6) is configured to control said tap changer (3) in such a way to carry out a regulation of a second voltage (V<sub>2</sub>) provided at said second windings (22), if said transformer (2) is in a load condition.
- 3. Transformer assembly, according to one or more of the previous claims, characterised in that it comprises:
  - current sensing means (4) adapted to provide first sensing signals (S<sub>1</sub>) indicative of a second current (I<sub>2</sub>) circulating along said second windings (22);
  - voltage sensing means (5) adapted to provide second sensing signals (S<sub>2</sub>) indicative of a second voltage (V<sub>2</sub>) provided at said second windings (22);

wherein said control unit (6) is operatively coupled with said voltage sensing means.

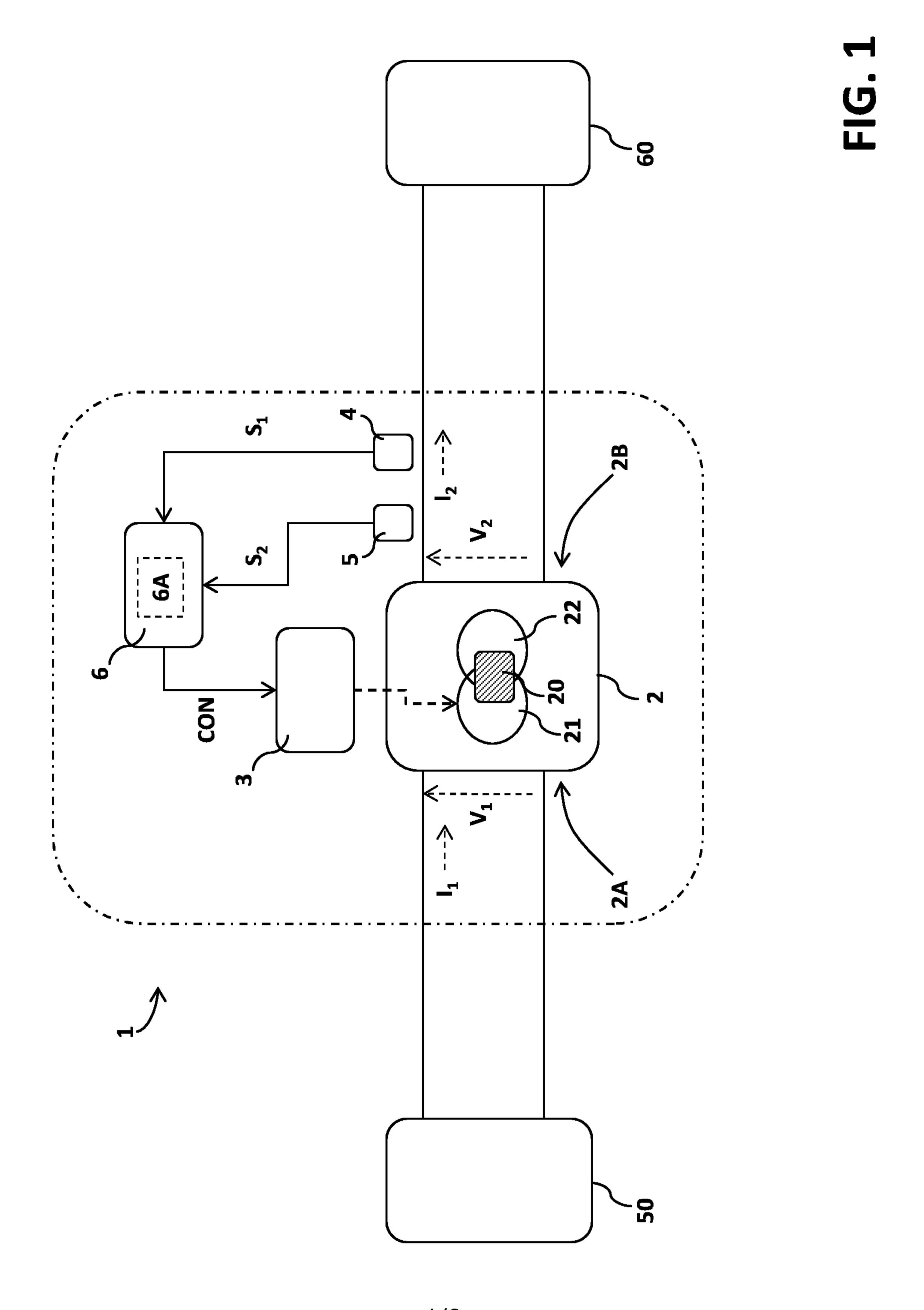
4. Transformer assembly, according to claim 3, characterised in that said control unit (6) is

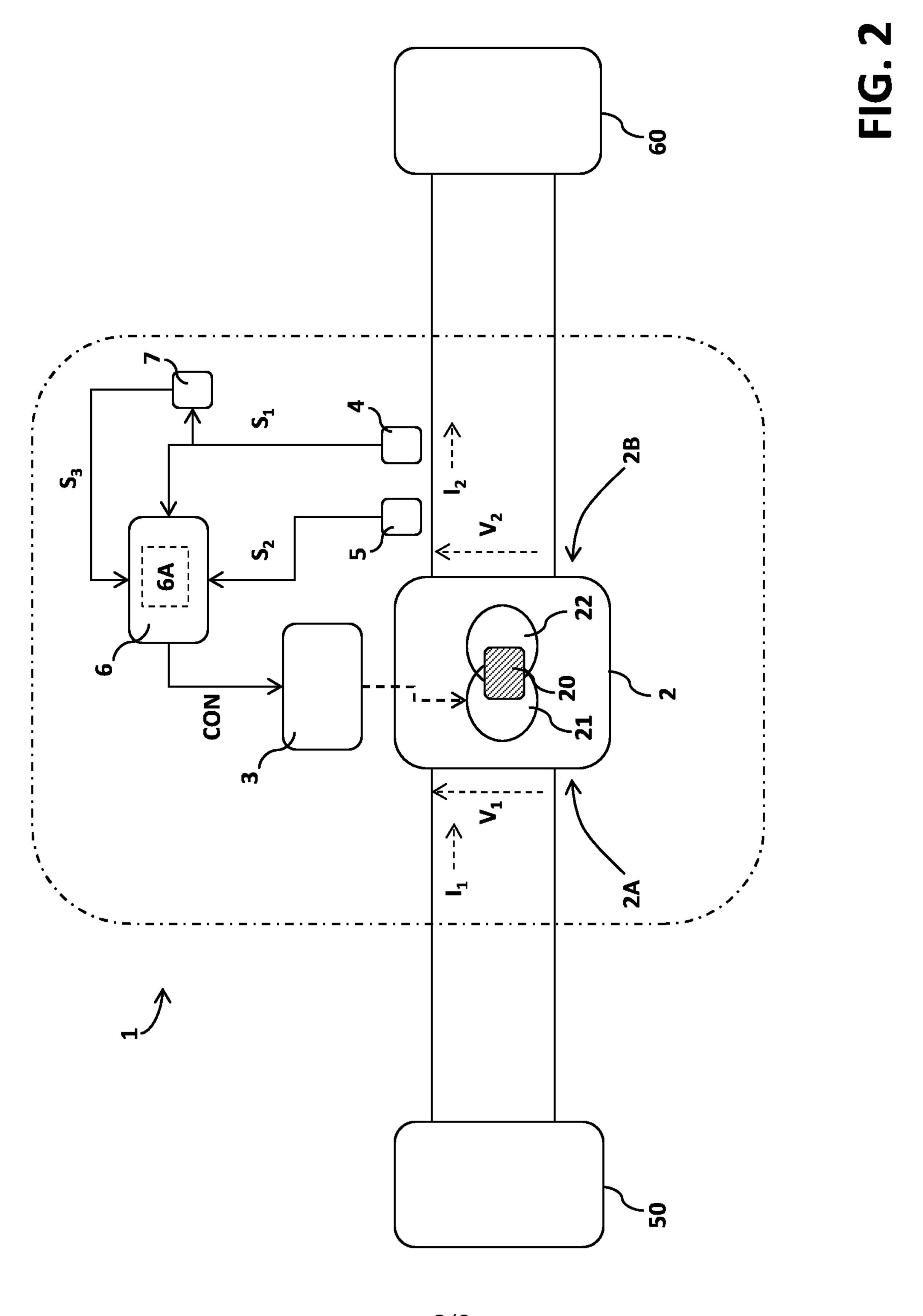
configured to acquire said input data (IN) by processing the first sensing signals ( $S_1$ ) provided by said current sensing means (4).

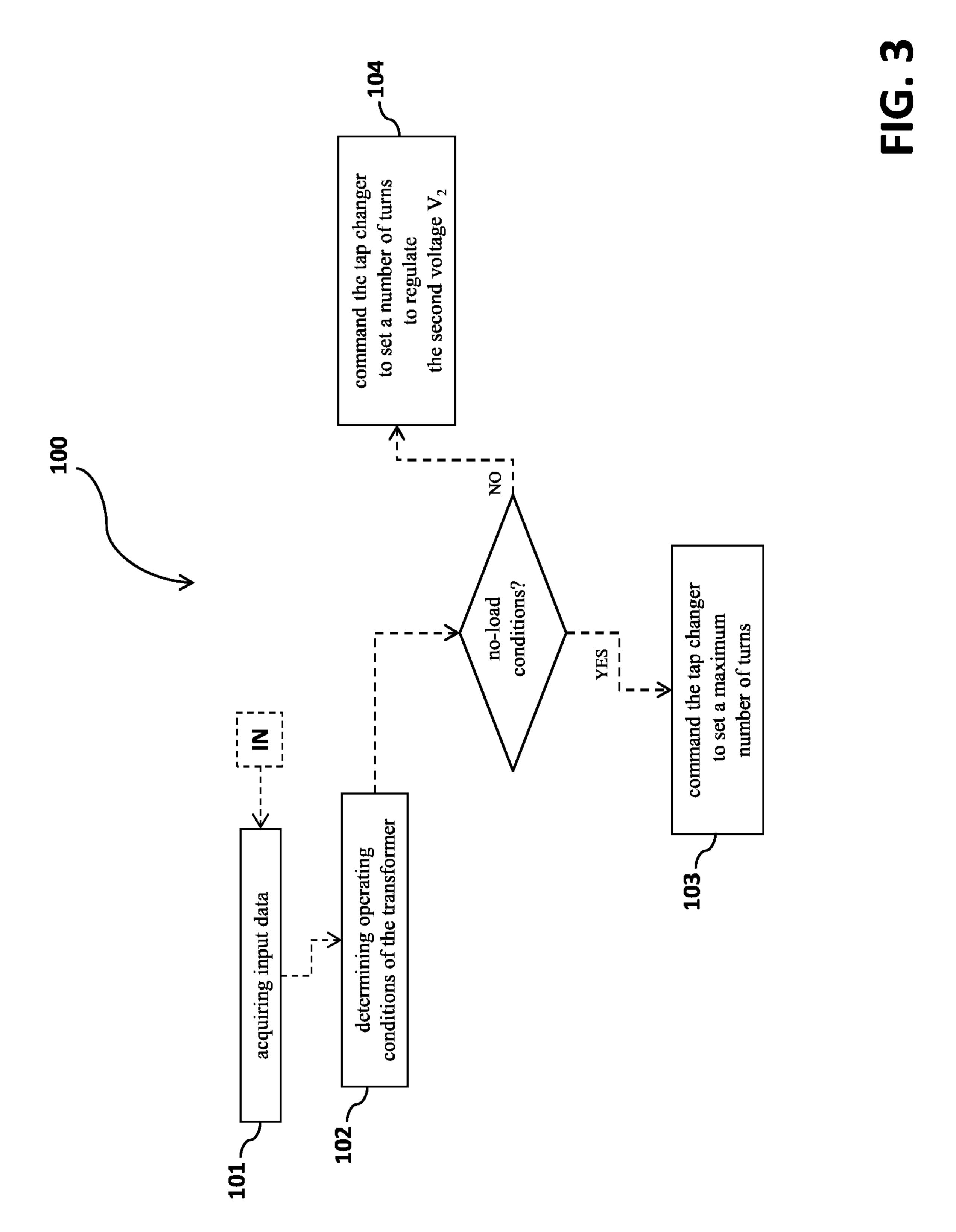
- 5. Transformer assembly, according to claim 3 or 4, characterised in that it comprises signalling means (7) adapted to receive the first sensing signals (S<sub>1</sub>) provided by said current sensing means (4) and provide third sensing signals (S<sub>3</sub>) indicative of the level of the current (I<sub>2</sub>) circulating along said second windings (22), said control unit (6) being configured to acquire said input data (IN) by processing said third sensing signals (S<sub>3</sub>).
- 6. Transformer assembly, according to claim 5, characterised in that said signalling means (7) include an electronic relay.
- 7. Transformer assembly, according to one or more of the previous claims, characterised in that it comprises a Station Service Voltage Transformer for providing an auxiliary power supply.
- 8. An electric power grid characterised in that it comprises a transformer assembly (1), according to one or more of the previous claims.
- 9. A method (100) for controlling a tap changer (3) included in a transformer assembly (1) for electric grids, said transformer assembly comprising:
  - an electric transformer (2) comprising a magnetic core (20), a first side (2A) including one or more first windings (21) enchained with said magnetic core and adapted to be electrically connected to a first grid section (50) and a second side (2B) including one or more second windings (22) enchained with said magnetic core and adapted to be electrically connected to a second grid section (60);
  - a tap changer (3) operatively associated with said electric transformer (2) to vary the number of turns enchained with said magnetic core (20) for said first windings (21); characterised in that it comprises the following steps:
  - acquiring (101) input data (IN) indicative of an electrical connectivity condition of said second grid section (60) with said second windings (22);
  - basing on said input data (IN), determining whether said transformer (2) is in a load condition or in a no-load condition;

- if said transformer (2) is in a no-load condition, commanding (102) said tap changer to set a maximum available number of turns for said first windings (21).

- 10. Method, according to claim 9, characterised in that it comprises the following step:
  - controlling said tap changer (3) in such a way to carry out a regulation of a second voltage (V<sub>2</sub>) provided at said second windings (22), if said transformer (2) is in a load condition.
- 11. Method, according to one of the claims from 9 to 10, characterised in that said transformer assembly (1) comprises:
  - current sensing means (4) adapted to provide first sensing signals (S1) indicative of a second current (I<sub>2</sub>) circulating along said second windings (22);
  - voltage sensing means (5) adapted to provide second sensing signals (S2) indicative of a second voltage (V2) provided at said second windings (22).
- 12. Method, according to claim 11, characterised in that said step (101) of acquiring said input data (IN) includes processing the first sensing signals (S1) provided by said current sensing means (4).
- 13. Method, according to claim 11 or 12, characterised in that said transformer assembly (1) comprises signalling means (7) adapted to receive the first sensing signals (S<sub>1</sub>) provided by said current sensing means (4) and adapted to provide third sensing signals (S<sub>3</sub>) indicative of the level of the current (I<sub>2</sub>) circulating along said second windings (22), said step (101) of acquiring said input data (IN) includes processing the third sensing signals (S<sub>3</sub>) provided by said signalling means (7).
- 14. Method, according to claim 13, characterised in that said signalling means (7) include an electronic relay.
- 15. Method, according to one or more of the claims from 9 to 14, characterised in that said transformer assembly comprises a Station Service Voltage Transformer for providing an auxiliary power supply.







3/3

#### INTERNATIONAL SEARCH REPORT

International application No PCT/EP2020/080056

A. CLASSIFICATION OF SUBJECT MATTER INV. G05F1/14 H02M5/12 H02P13/06 ADD.

According to International Patent Classification (IPC) or to both national classification and IPC

#### B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

G05F H02M H02P

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

EPO-Internal, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT					
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.			
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A	EP 2 889 998 A2 (GEN ELECTRIC [US]) 1 July 2015 (2015-07-01) abstract; figure 6	1-15			
A	US 5 136 233 A (KLINKENBERG JERRY R [US] ET AL) 4 August 1992 (1992-08-04) abstract	1-15			
A	GB 236 596 A (MICHEL DOLOUKHANOFF) 3 June 1926 (1926-06-03) page 1, lines 36-58; figure 1	1-15			

Further documents are listed in the continuation of Box C.	See patent family annex.			
* Special categories of cited documents :				
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"P" document published prior to the international filing date but later than the priority date claimed	"&" document member of the same patent family			
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18 December 2020	13/01/2021			
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International application No PCT/EP2020/080056

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	NNACHI G U ET AL: "Estimation of no-Load Losses in Distribution Transformer Design Finite Element Analysis Techniques in Transformer Design", 2018 IEEE PES/IAS POWERAFRICA, IEEE, 28 June 2018 (2018-06-28), pages 1-532, XP033438935, DOI: 10.1109/POWERAFRICA.2018.8521142 page 528 - page 529	1-15
	EDWARD J CHAM ET AL: "Current Regulators for Large Rectifier Prower Supplies Used on Electrochemical Processing Lines", IEEE TRANSACTIONS ON INDUSTRY AND GENERAL APPLICATIONS,, vol. IGA-4, no. 6, 1 November 1968 (1968-11-01), pages 609-618, XP001405495, abstract; figure 1	1-15

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