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(54) **RECEIVER CIRCUIT**

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CPC ***H04B 17/21*** (2015.01); ***H04B 1/16*** (2013.01); ***H04W 52/02*** (2013.01)

(57) **ABSTRACT**

A receiver circuit includes: a local signal generation circuit that generates a local signal; and a test signal generation circuit that generates a test signal having a frequency close to a frequency of the local signal, wherein the test signal generation circuit includes an oscillator that generates the test signal, a mixer that mixes the local signal with an output of the oscillator to generate a low-frequency signal which is a difference signal between the local signal and the output of the oscillator, a phase detector that detects a phase difference between the low-frequency signal output by the mixer and a reference signal, and a filter that extracts a low-frequency component from an output of the phase detector, and controls an oscillation frequency of the oscillator by using an output of the filter.

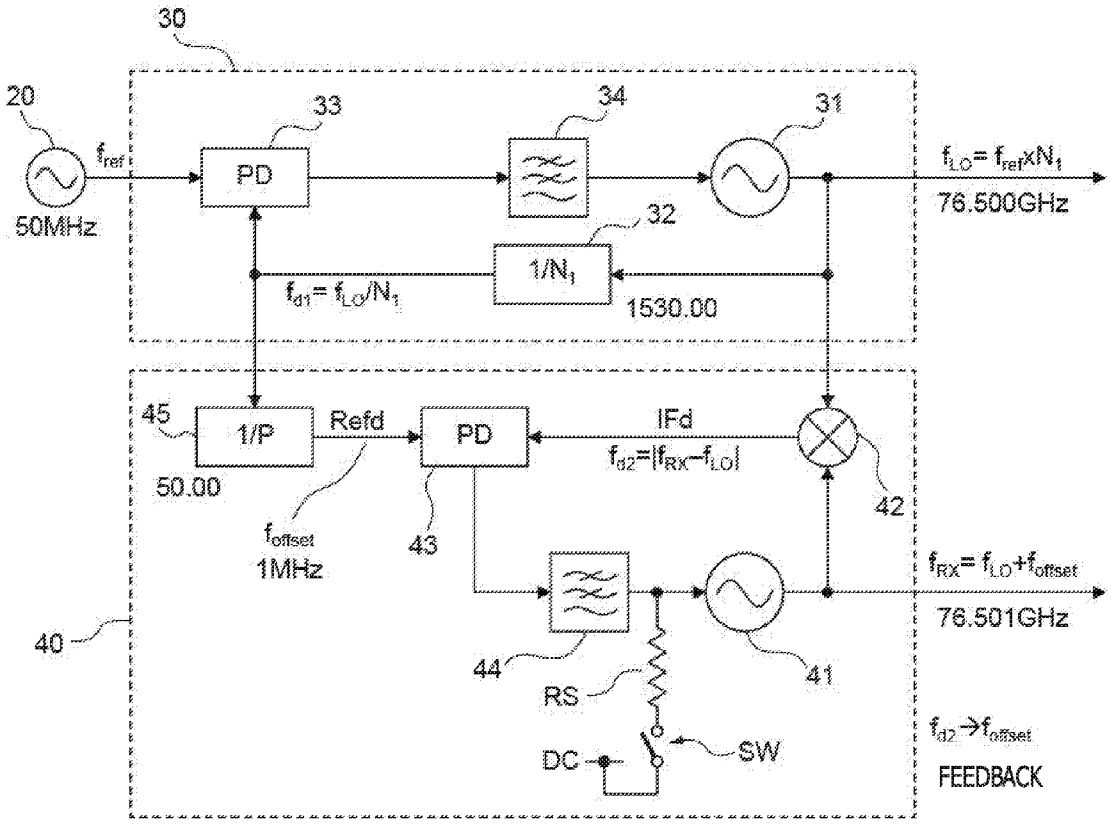


FIG. 1

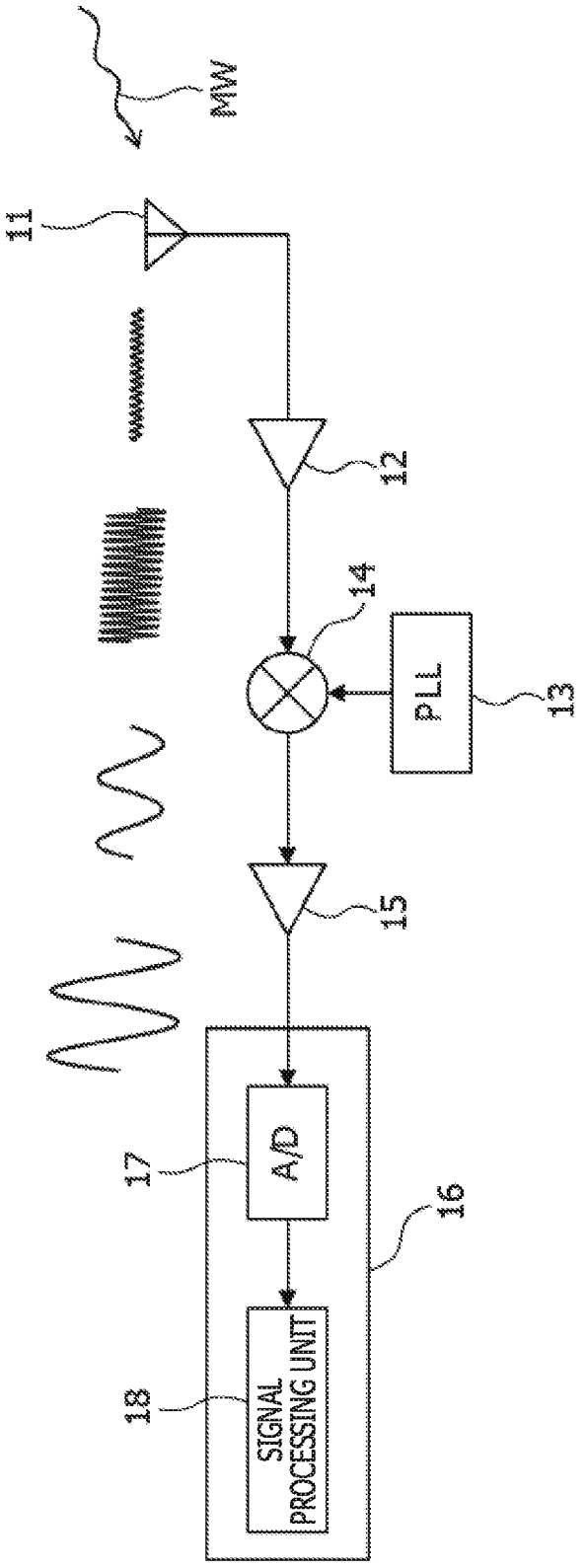


FIG. 2

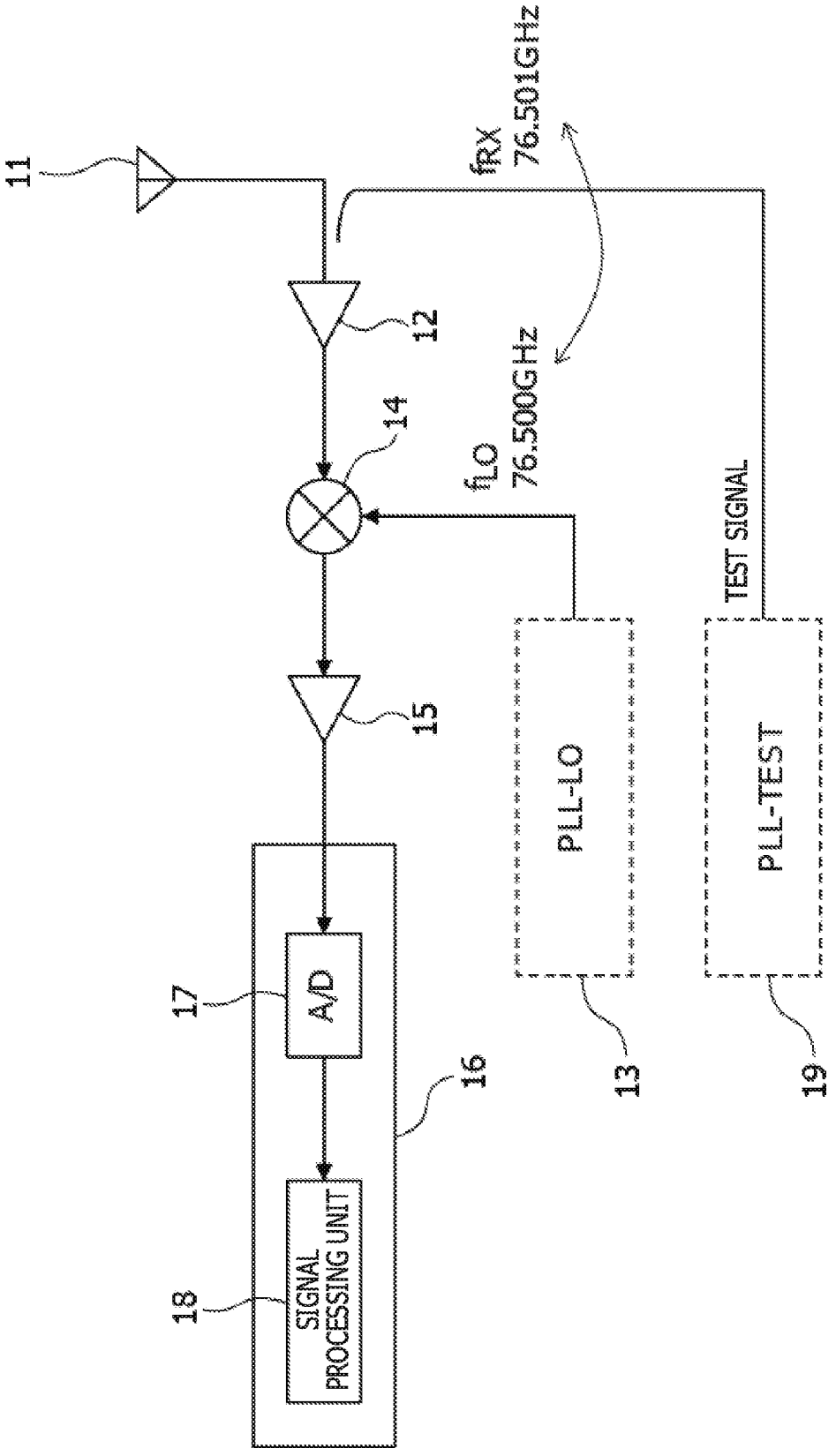

11
12
14
15
16
17
18
13
19
fRX
76.501GHz
fLO
76.500GHz
TEST SIGNAL
PLL-LO
PLL-TEST
A/D
SIGNAL PROCESSING UNIT

FIG. 3

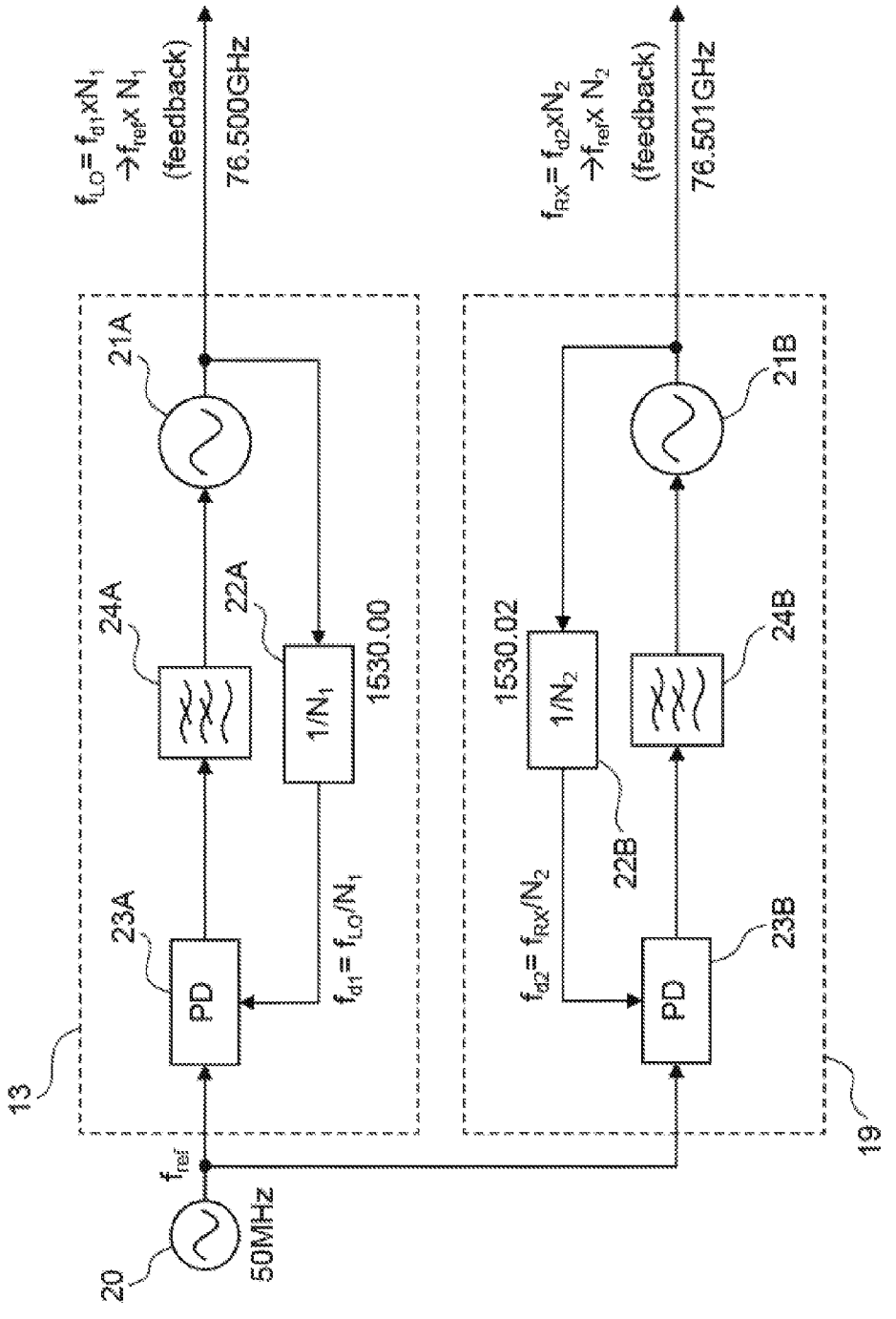

$f_{LO}= f_{d1}xN_1$
$\rightarrow f_{ref}x\ N_1$
(feedback)
76.500GHz
$f_{RX}= f_{d2}xN_2$
$\rightarrow f_{ref}x\ N_2$
(feedback)
76.501GHz
21A
21B
24A
22A
1530.00
$1/N_1$
1530.02
$1/N_2$
24B
22B
23A
PD
$f_{d1}= f_{LO}/N_1$
$f_{d2}= f_{RX}/N_2$
PD
23B
13
19
f_{ref}
50MHz
20

FIG. 4

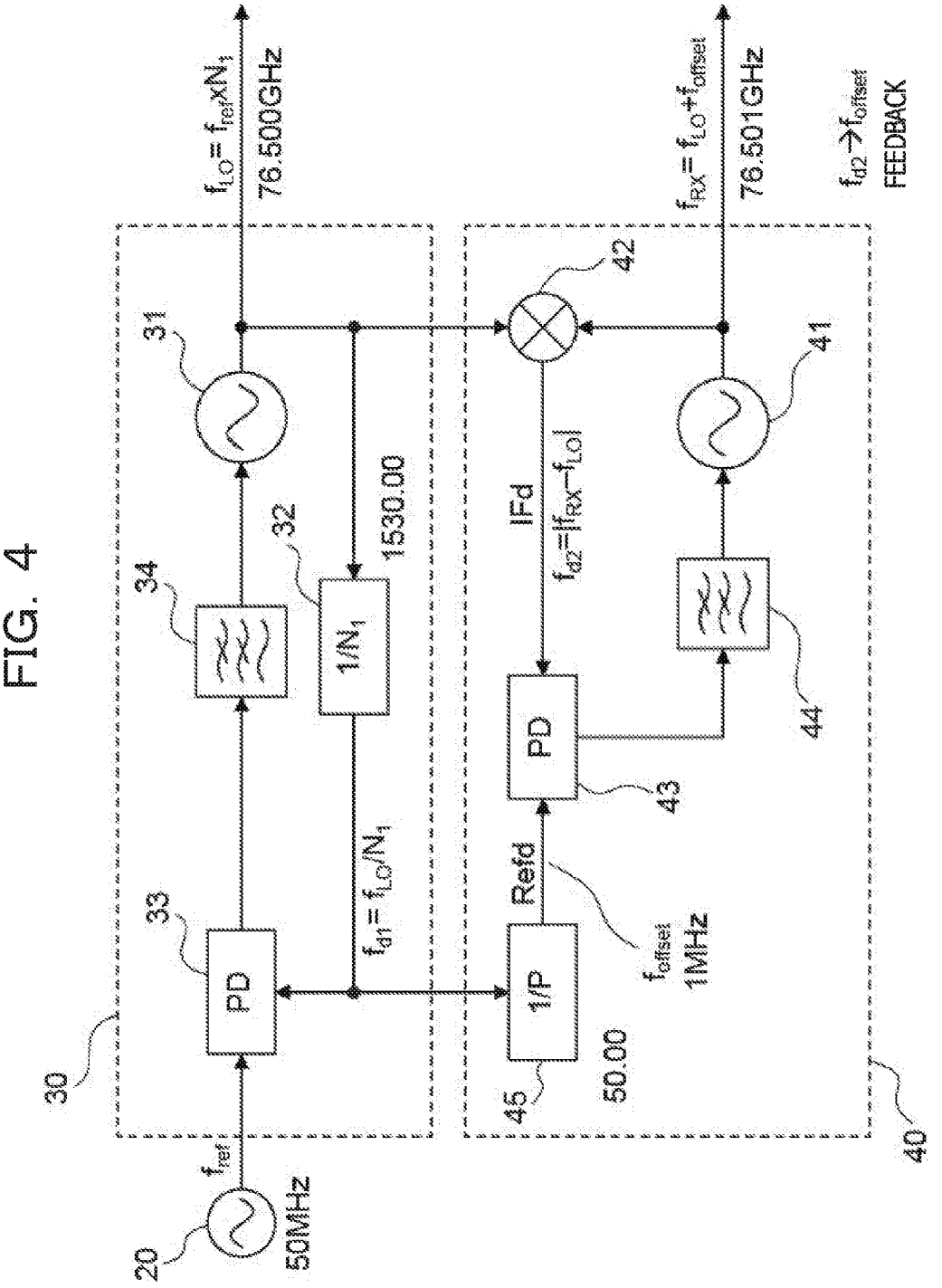

20
50MHz
f_{ref}
30
33
PD
34
31
32
$1/N_1$
1530.00
$f_{d1}=f_{LO}/N_1$
$f_{LO}=f_{ref}xN_1$
76.500GHz
40
45
1/P
50.00
Refd
f_{offset}
1MHz
IFd
$f_{d2}=|f_{RX}-f_{LO}|$
PD
43
42
41
44
$f_{RX}=f_{LO}+f_{offset}$
76.501GHz
$f_{d2}\rightarrow f_{offset}$
FEEDBACK

FIG. 5

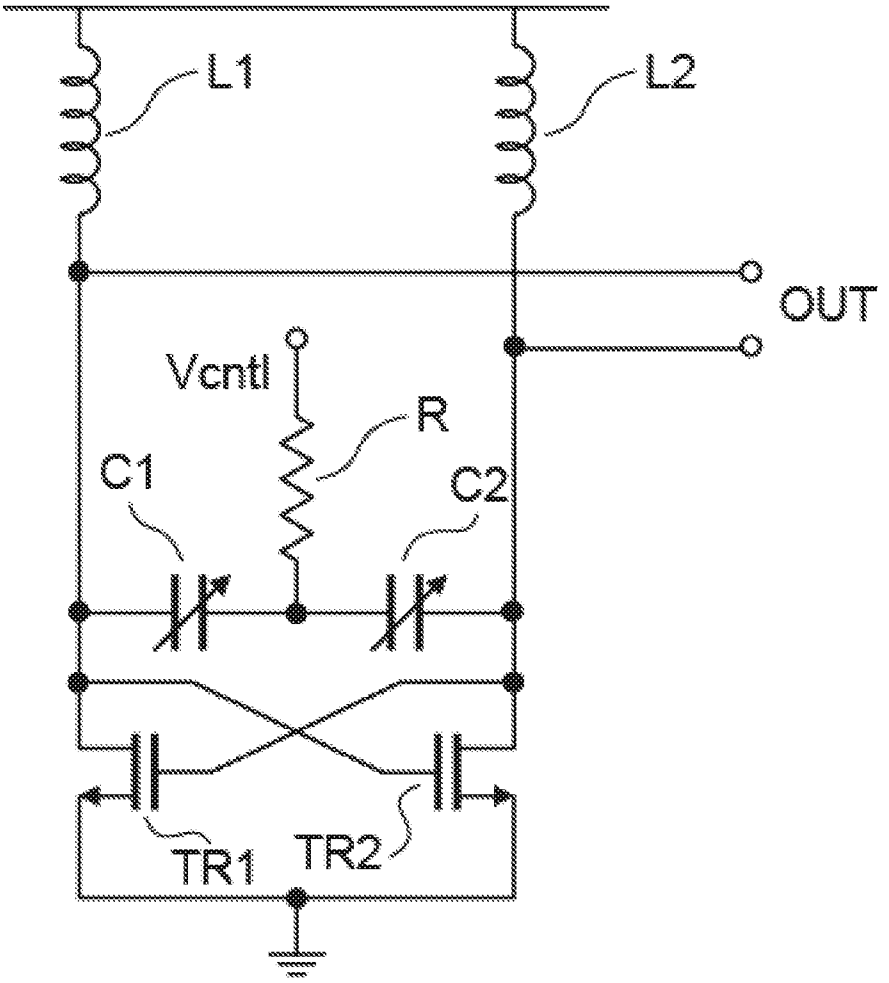


FIG. 6

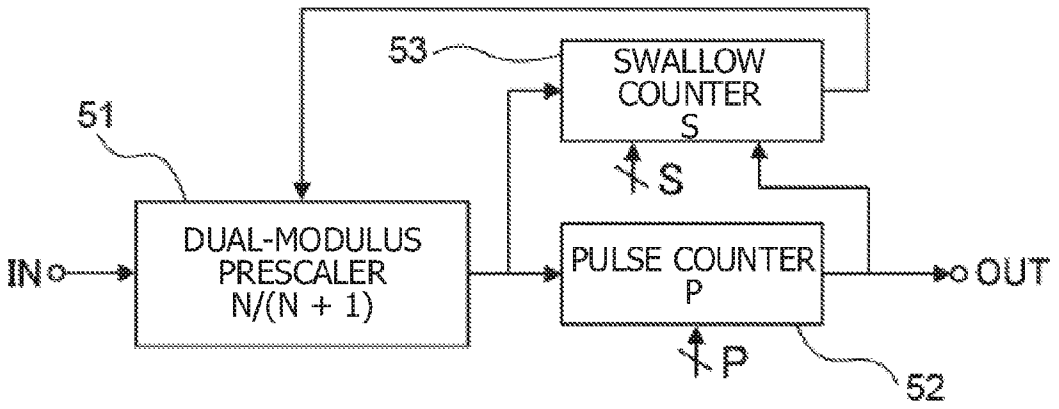

53
SWALLOW COUNTER S
51
S
DUAL-MODULUS PRESCALER N/(N + 1)
IN
PULSE COUNTER P
OUT
P
52

FIG. 7A

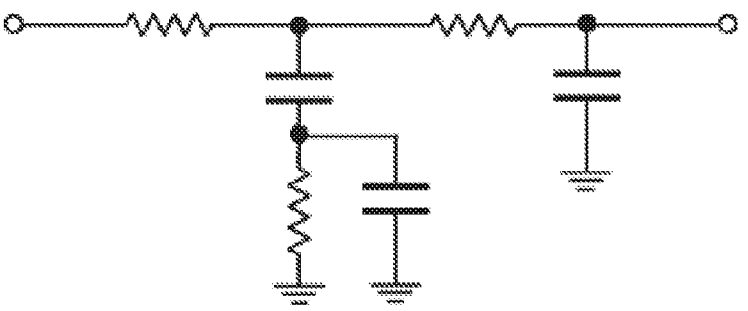


FIG. 7B

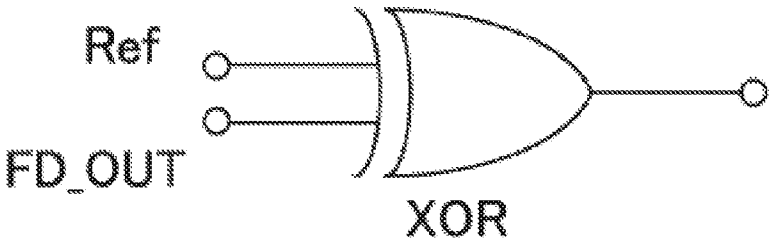


FIG. 7C

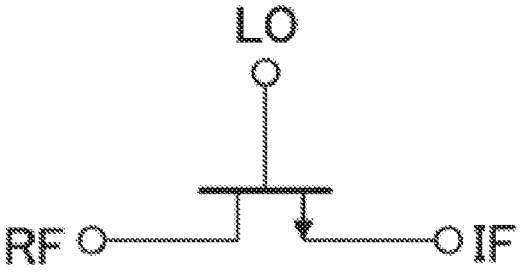


FIG. 8

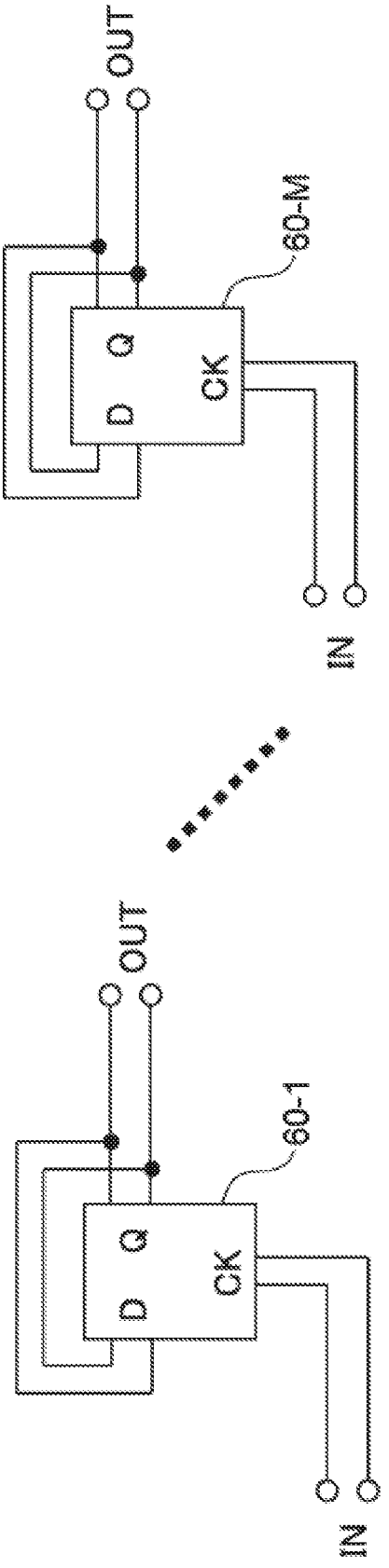


FIG. 9

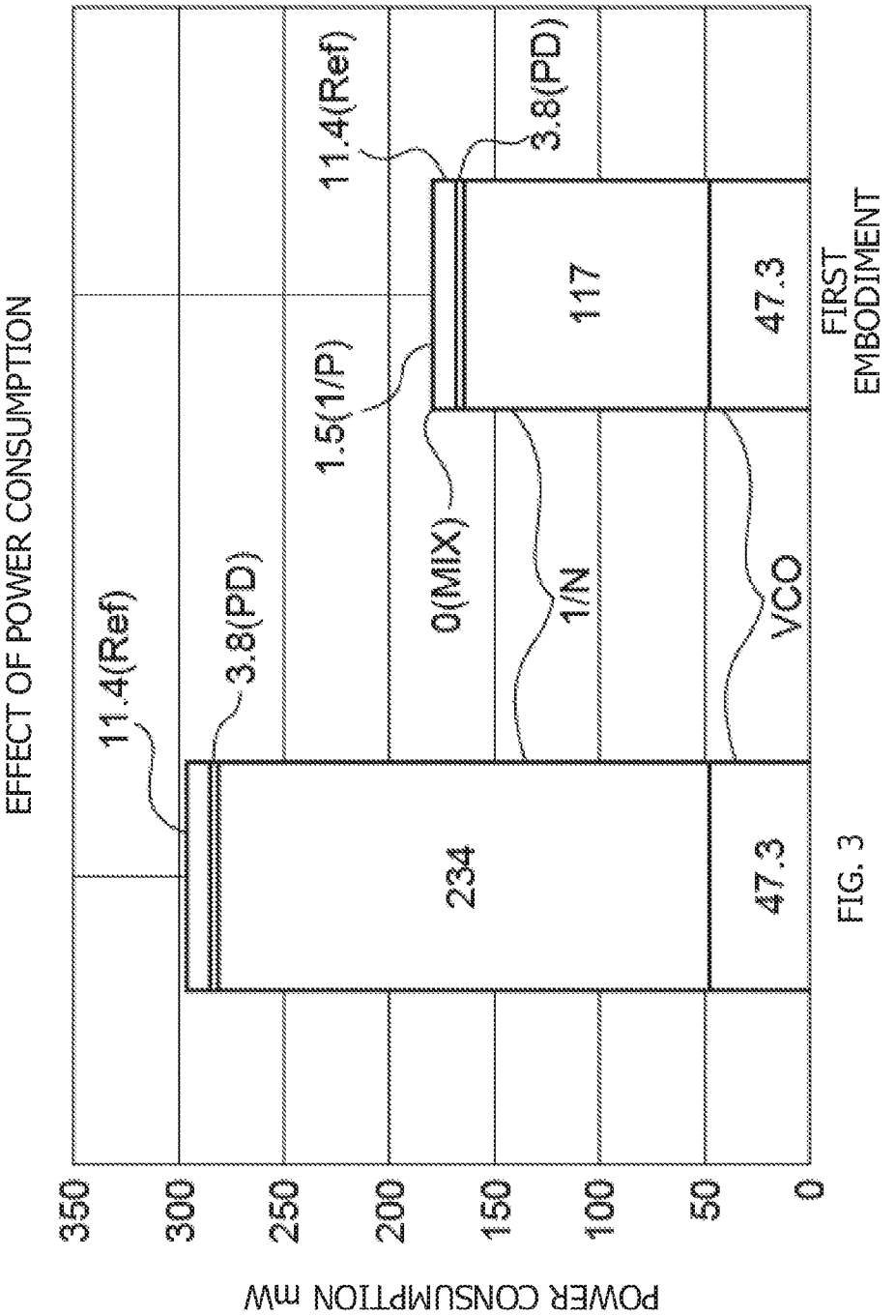

EFFECT OF POWER CONSUMPTION
FIRST EMBODIMENT
POWER CONSUMPTION mW
350
300
250
200
150
100
50
0
11.4(Ref)
3.8(PD)
234
47.3
1.5(1/P)
0(MIX)
1/N
VCO
117
47.3
11.4(Ref)
3.8(PD)

FIG. 3

FIG. 10

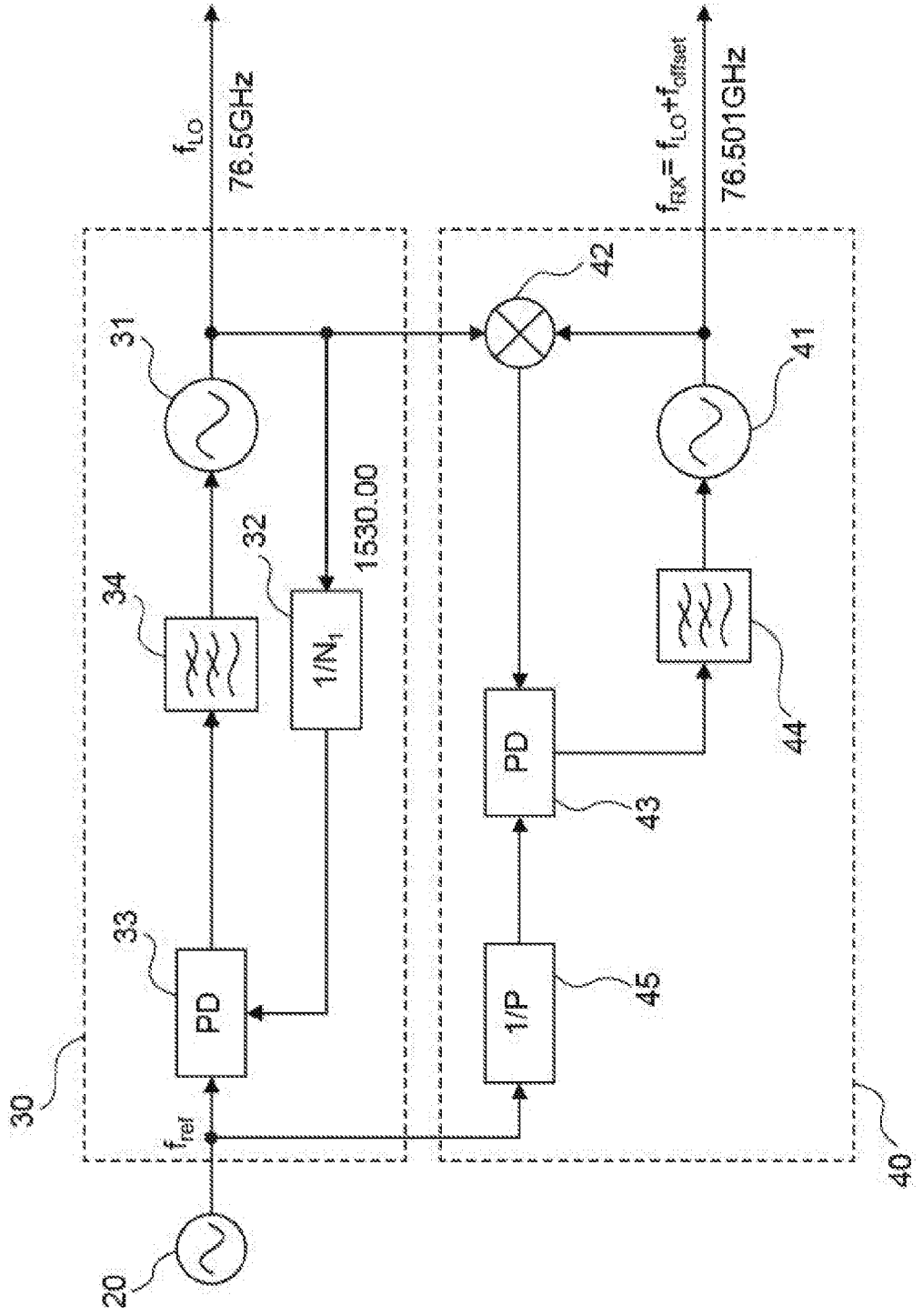
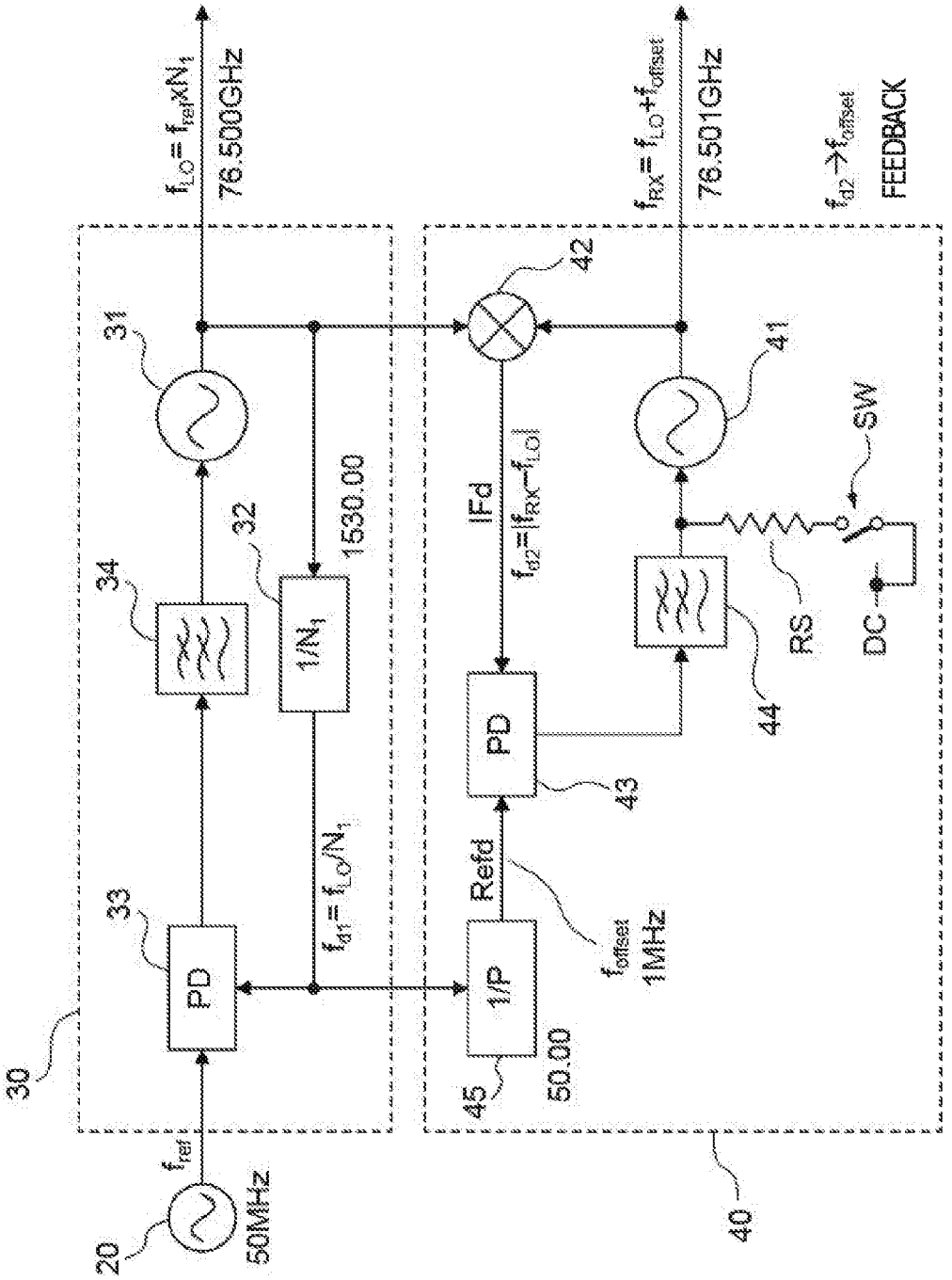

20
30
40
31
32
33
34
41
42
43
44
45
PD
PD
1/P
1/N1
1530.00
fref
fLO
76.5GHz
fRX= fLO+foffset
76.501GHz

FIG. 11


20
50MHz
f_{ref}
30
33
PD
34
32
1/N_1
1530.00
31
$f_{LO}=f_{ref}\times N_1$
76.500GHz
$f_{d1}=f_{LO}/N_1$
40
45
1/P
50.00
Refd
f_{offset}
1MHz
43
PD
IFd
$f_{d2}=|f_{RX}-f_{LO}|$
42
41
$f_{RX}=f_{LO}+f_{offset}$
76.501GHz
44
RS
SW
DC
$f_{d2}\rightarrow f_{offset}$
FEEDBACK

RECEIVER CIRCUIT

CROSS-REFERENCE TO RELATED APPLICATION

[0001] This application is based upon and claims the benefit of priority of the prior Japanese Patent Application No. 2015-047365, filed on Mar. 10, 2015, the entire contents of which are incorporated herein by reference.

FIELD

[0002] The embodiments discussed herein are related to a receiver circuit.

BACKGROUND

[0003] In wireless devices, reception characteristics are measured at any time, self-correction is performed based on the measured reception characteristics, and thus high performance and high stability are achieved with low power consumption. To do this, a test signal generation circuit that generates a test signal is provided in a receiver circuit of a wireless device, and the generated test signal is supplied to the receiver circuit. A receiver circuit having such a test signal generation circuit is referred to as a receiving built-in-self-test (BIST) circuit.

[0004] In a receiver circuit, a local signal having a frequency close to that of an incoming signal is supplied to a mixer together with the incoming signal, a baseband process is performed in the mixer, and a transmission signal component is thereby extracted. In order to inspect reception characteristics, a signal simulating an incoming signal has to be generated separately, and be input from the immediate vicinity of an antenna.

[0005] Thus, a test signal generation circuit having a configuration similar to that of a local signal generation circuit that generates a local signal is installed, and a test signal is input from the immediate vicinity of the antenna by using a coupler or the like. The test signal is received by the receiver circuit, and is subjected to a baseband process. This enables measurement of reception gain, a phase change, and so forth.

[0006] The local signal generation circuit and the test signal generation circuit are each typically constituted by a phase locked loop (PLL) circuit, and control output frequencies by changing their respective division ratios. For example, a frequency of a signal generated by a voltage-controlled oscillator (VCO) is divided, a phase of this frequency-divided signal is compared with a phase of a reference signal, and a comparison result is fed back. Thus, feedback is applied so that a frequency of the frequency-divided signal becomes equal to a frequency of the reference signal. When a feedback loop is stabilized, an output frequency of the VCO is stabilized.

[0007] A frequency of a test signal has to be different from a frequency of a local signal. Hence, a signal source for test signal generation is installed separately from a local signal source, and frequency dividers installed in these respective signal sources have to be controlled so that their respective division ratios differ from each other. For this reason, the test signal generation circuit results in increases in power consumption and circuit area. In particular, in a frequency divider circuit provided in the test signal generation circuit, the conversion from an output frequency to a reference frequency has to be carried out, high-speed operation is demanded, and a significantly large division ratio is also demanded. Thus, the frequency divider circuit provided in the test signal generation circuit is large in size, and also consumes a large amount of power.

[0008] The following is a reference document.

[Document 1] Japanese Laid-open Patent Publication No. 2011-130174.

SUMMARY

[0009] According to an aspect of the invention, a receiver circuit includes: a local signal generation circuit that generates a local signal; and a test signal generation circuit that generates a test signal having a frequency close to a frequency of the local signal, wherein the test signal generation circuit includes an oscillator that generates the test signal, a mixer that mixes the local signal with an output of the oscillator to generate a low-frequency signal which is a difference signal between the local signal and the output of the oscillator, a phase detector that detects a phase difference between the low-frequency signal output by the mixer and a reference signal, and a filter that extracts a low-frequency component from an output of the phase detector, and controls an oscillation frequency of the oscillator by using an output of the filter.

[0010] The object and advantages of the invention will be realized and attained by means of the elements and combinations particularly pointed out in the claims.

[0011] It is to be understood that both the foregoing general description and the following detailed description are exemplary and explanatory and are not restrictive of the invention, as claimed.

BRIEF DESCRIPTION OF DRAWINGS

[0012] FIG. **1** illustrates a basic configuration of a receiver circuit of a wireless device;

[0013] FIG. **2** illustrates a typical configuration of a receiver circuit in which a test signal generation circuit is installed and which enables reception characteristics inspection;

[0014] FIG. **3** illustrates a circuit configuration of a local signal generation circuit (PLL-LO) and a test signal generation circuit (PLL-TEST);

[0015] FIG. **4** is a circuit diagram illustrating configurations of a local signal generation circuit (PLL-LO) and a test signal generation circuit (PLL-TEST) in a receiver circuit according to a first embodiment;

[0016] FIG. **5** is a circuit diagram illustrating an example of each of VCOs of the PLL-LO and the PLL-TEST;

[0017] FIG. **6** is a block diagram illustrating an example of a frequency divider circuit of the PLL-LO;

[0018] FIGS. **7**A to **7**C are circuit diagrams of other circuit components, FIG. **7**A is a circuit diagram of a filter, FIG. **7**B is a circuit diagram of a phase detector (PD), and FIG. **7**C is a circuit diagram of a mixer;

[0019] FIG. **8** illustrates an exemplary circuit of a reference frequency divider circuit;

[0020] FIG. **9** illustrates constituent ratios of power consumed by each component in a receiver circuit in FIG. **3** and the receiver circuit according to the first embodiment in FIG. **4**;

[0021] FIG. **10** is a circuit diagram illustrating configurations of a local signal generation circuit (PLL-LO) and a test signal generation circuit (PLL-TEST) in a receiver circuit according to a second embodiment; and

[0022] FIG. **11** is a circuit diagram illustrating configurations of a local signal generation circuit (PLL-LO) and a test signal generation circuit (PLL-TEST) in a receiver circuit according to a third embodiment.

DESCRIPTION OF EMBODIMENTS

[0023] Before a receiver circuit according to each embodiment is described, a typical receiver circuit of a wireless device will be described.

[0024] FIG. **1** illustrates a basic configuration of a receiver circuit of a wireless device.

[0025] The receiver circuit includes an antenna **11**, a linear amplifier (LA) **12**, a phase locked loop (PLL) circuit **13**, a mixer **14**, an intermediate frequency (IF) amplifier **15**, and a baseband signal processing circuit **16**. The antenna **11** receives a radio signal transmitted from a radio transmitter. Here, the case where a millimeter-wave signal is used as a radio signal will be described as an example. The linear amplifier **12** amplifies a high-frequency signal from the antenna **11**. The PLL circuit **13** generates a local signal for reception operation. The mixer **14** mixes the high-frequency signal amplified by the linear amplifier **12** with the local signal to generate an intermediate frequency (IF) signal. The IF amplifier **15** amplifies the IF signal.

[0026] The baseband signal processing circuit **16** includes an analog-to-digital (A/D) converter circuit **17**, and a signal processing unit **18**. The A/D converter circuit **17** converts the IF signal into a digital signal to generate a baseband signal data. The signal processing unit **18** performs a digital process on the baseband signal data to acquire incoming data.

[0027] The basic configuration of the receiver circuit illustrated in FIG. **1** is widely known, and further description thereof is therefore omitted. It is noted that a receiver circuit according to each embodiment to be described below is a circuit used as the receiver circuit of the wireless device or the like illustrated in FIG. **1**.

[0028] As illustrated in FIG. **1**, a local signal generated by the PLL circuit **13** is supplied to the mixer **14** for normal reception operation. In order to inspect reception characteristics, a signal simulating an incoming signal has to be generated separately, and be input from the immediate vicinity of the antenna **11**. For this reason, typically, a test signal generation circuit equivalent to a PLL circuit that generates a local signal is installed, and a test signal is input from the immediate vicinity of an antenna by using a coupler or the like. The test signal is received by a typical receiver circuit, and is subjected to a baseband process, and reception gain and a phase change may thereby be obtained.

[0029] FIG. **2** illustrates a typical configuration of a receiver circuit in which a test signal generation circuit is installed and which enables reception characteristics inspection.

[0030] The receiver circuit illustrated in FIG. **2** differs from the receiver circuit illustrated in FIG. **1** in that a test signal generation circuit **19** is provided and a test signal is input from the immediate vicinity of the antenna **11**, and the receiver circuit illustrated in FIG. **2** and the receiver circuit illustrated in FIG. **1** are the same in other respects. The test signal generation circuit **19** is constituted by a PLL circuit. Hereinafter, as illustrated in FIG. **2**, the PLL circuit (also referred to as a local signal generation circuit) **13** that generates a local signal is represented by PLL-LO, and the test signal generation circuit **19** is represented by PLL-TEST.

[0031] FIG. **3** illustrates a circuit configuration of the local signal generation circuit (PLL-LO) **13** and the test signal generation circuit (PLL-TEST) **19**.

[0032] The PLL-LO **13** includes a voltage-controlled oscillator (VCO) **21**A, a frequency divider circuit **22**A, a phase detector (PD) **23**A, and a filter **24**A. The VCO **21**A oscillates at a frequency based on a control voltage, and outputs a local signal having a frequency f_{LO}. The frequency divider circuit **22**A divides a frequency of the local signal output by the VCO **21**A by N_1, and generates a frequency-divided signal having a frequency of $f_{d1}=f_{LO}/N_1$. A reference signal source **20** outputs an original reference signal Ref having a frequency f_{ref}. The PD **23**A compares a phase of the original reference signal Ref from the reference signal source **20** with a phase of the frequency-divided signal, and outputs a phase difference signal. The filter **24**A extracts a low-frequency component of the phase difference signal to generate a control voltage Vcntl, and outputs the control voltage Vcntl to the VCO **21**A. In the PLL-LO **13**, feedback is applied so that the frequency of the frequency-divided signal becomes equal to the frequency of the original reference signal. When a feedback loop is stabilized, the frequency f_{LO} of the local signal, which is an oscillation frequency of the VCO **21**A, is represented by the following form: $f_{LO}=f_{d1}\times N_1=f_{ref}\times N_1$. In the PLL-LO **13**, a frequency of a local signal to be output is controlled by changing a division ratio.

[0033] The PLL-TEST **19** includes a VCO **21**B, a frequency divider circuit **22**B, a PD **23**B, and a filter **24**B, and forms a feedback loop similar to that in the PLL-LO **13**. A frequency f_{RX} of a test signal to be output is represented by the following form: $f_{RX}=f_{d2}\times N_2=f_{ref}\times N_2$. The frequency f_{LO} of the local signal and the frequency f_{RX} of the test signal have to be different from each other although they are close to each other, and thus $N_1=1530.00$ is set, whereas $N_2=1530.02$ is set. In an example illustrated in FIG. **3**, because of $f_{ref}=50$ MHz and $N_1=1530.00$, $f_{LO}=50$ MHz×1530=76.500 GHz is obtained. In contrast to this, because of $N_2=1530.02$, $f_{RX}=50$ MHz×1530.02=76.501 GHz is obtained.

[0034] As described above, since a frequency of a test signal has to be different from a frequency of a local signal, a test signal generation circuit is installed separately from a local signal generation circuit, and frequency divider circuits installed in the respective signal generation circuits have to be controlled so that their respective division ratios differ from each other. The local signal generation circuit is a circuit that is large in size and consumes a large amount of power, and thus installation of two such circuits results in increases in power consumption and circuit area. In particular, in a frequency divider circuit, a significantly large division ratio at which the conversion from an output frequency (for example, 80 GHz) to an original reference frequency (for example, 50 MHz) is carried out is demanded, and high-speed operation is also demanded. Thus, the frequency divider circuit is large in size, and consumes a large amount of power.

[0035] A receiver circuit according to each embodiment to be described below is used as a receiver circuit of a wireless device, performs self-correction of reception characteristics with a simple circuit configuration, and achieves high performance and high stability with low power consumption.

[0036] FIG. **4** is a circuit diagram illustrating configurations of a local signal generation circuit (PLL-LO) and a test signal generation circuit (PLL-TEST) in a receiver circuit according to a first embodiment.

[0037] The receiver circuit according to the first embodiment is used as a receiver circuit of a wireless device like that illustrated in FIG. **2**. The receiver circuit according to the first embodiment includes a reference signal source **20**, a local signal generation circuit (PLL-LO) **30**, and a test signal generation circuit (PLL-TEST) **40**. The reference signal source **20** outputs an original reference signal Ref having a frequency f_{ref}.

[0038] The PLL-LO **30** includes a VCO **31**, a frequency divider circuit **32**, a phase detector (PD) **33**, and a filter **34**, changes a division ratio N_1 of the frequency divider circuit **32**, and thereby changes a frequency f_{LO} of a local signal to be output. In other words, the PLL-LO **30** forms a feedback loop similar to that in the PLL-LO **13** illustrated in FIG. **3**.

[0039] The PLL-TEST **40** includes a VCO **41**, a mixer **42**, a phase detector (PD) **43**, a filter **44**, and a reference frequency divider circuit **45**. The VCO **41** oscillates at a frequency based on a control voltage Vcntl, and outputs a test signal having a frequency f_{RX}. The mixer **42** mixes the local signal output by the VCO **31** of the PLL-LO **30** with the test signal to generate a low-frequency signal IFd. A frequency f_{d2} of the low-frequency signal IFd is an absolute value of a difference between the frequency f_{RX} of the test signal and the frequency f_{LO} of the local signal. That is, the frequency f_{d2} is represented by the following form: $f_{d2}=|f_{RX}-f_{LO}|$. Assuming f_{RX}=76.501 GHz and f_{LO}=76.500 GHz, f_{d2}=1 MHz is obtained.

[0040] The reference frequency divider circuit **45** divides a frequency of a frequency-divided signal output by the frequency divider circuit **32** of the PLL-LO **30** so as to result in a frequency close to the frequency f_{d2} of the low-frequency signal IFd further to generate a reference signal Refd. The frequency of the frequency-divided signal output by the frequency divider circuit **32** here is 50 MHz which is equal to the frequency of the original reference signal, and assuming that a division ratio P of the reference frequency divider circuit **45** is 50.00, a frequency f_{offset} of the reference signal Refd is 1 MHz. Hence, the frequency f_{offset} of the reference signal Refd is a frequency close to the frequency f_{d2} of the low-frequency signal IFd.

[0041] The PD **43** compares a phase of the reference signal Refd with a phase of the low-frequency signal IFd, and generates a phase difference signal, which is a comparison result. The filter **44** extracts a low-frequency component from the phase difference signal to generate a control voltage Vcntl, and supplies the control voltage Vcntl to the VCO **41**.

[0042] In the PLL-TEST **40**, the VCO **41**, the mixer **42**, the PD **43**, and the filter **44** constitute a PLL circuit in which the phase of the low-frequency signal IFd is compared with the phase of the reference signal Refd and a comparison result is fed back. In this PLL circuit, feedback is applied so that the frequency f_{d2} of the low-frequency signal IFd becomes equal to the frequency f_{offset} of the reference signal Refd. When a feedback loop is stabilized, the frequency f_{RX} of the test signal output by the VCO **41** becomes equal to a frequency obtained by offsetting the frequency f_{LO} of the local signal by the amount of f_{offset}. That is, the frequency f_{RX} is represented by the following form: $f_{RX}=f_{LO}+f_{offset}$. In the PLL-TEST **40**, a frequency of a test signal to be output is controlled by changing a division ratio of the reference frequency divider circuit **45**.

[0043] FIG. **5** is a circuit diagram illustrating an example of each of the VCO **31** of the PLL-LO **30** and the VCO **41** of the PLL-TEST **40**. The voltage-controlled oscillator includes a series circuit including an inductor L**1** and a transistor TR**1**, and a series circuit including an inductor L**2** and a transistor TR**2**, and two series circuits form a differential pair. Sources of the transistors TR**1** and TR**2** are connected to a common ground, and terminals of the inductors L**1** and L**2** are connected to a common VCC. Capacitors C**1** and C**2** are connected in series between a connection node (a drain of the transistor TR**1**) of the inductor L**1** and the transistor TR**1** and a connection node (a drain of the transistor TR**2**) of the inductor L**2** and the transistor TR**2**, and a control voltage Vcntl is supplied to a connection node of the capacitors C**1** and C**2**. Oscillation signals are output from the connection node of the inductor L**1** and the transistor TR**1** and the connection node of the inductor L**2** and the transistor TR**2**.

[0044] The VCO circuit illustrated in FIG. **5** is widely known, and further description thereof is therefore omitted. It is noted that the VCO circuit illustrated in FIG. **5** is an example, and the VCOs used in each embodiment are not limited to this.

[0045] FIG. **6** is a block diagram illustrating an example of the frequency divider circuit **32** of the PLL-LO **30**.

[0046] The frequency divider circuit **32** is called a pulse-swallow programmable frequency divider, and includes a dual-modulus prescaler **51**, a pulse counter **52**, and a swallow counter **53**. The dual-modulus prescaler **51** is a circuit that generates and outputs a signal having a frequency of 1/N or 1/(N+1) of a frequency of an input signal. Which of frequencies of 1/N and 1/(N+1) of the input signal frequency a signal to be output has is controlled by an output from the swallow counter **53**.

[0047] The pulse counter **52** is a programmable counter that counts pulses of an input signal received from the dual-modulus prescaler **51**, and a count number P is externally set. When the count of the set count number P is reached, the pulse counter **52** changes an output signal (OUT). When the pulse counter **52** completes the count of the count number P, the pulse counter **52** automatically starts the count of a subsequent count number P.

[0048] The swallow counter **53** is a programmable counter that counts pulses of an input signal received from the dual-modulus prescaler **51**, and a count number S is externally set. When the swallow counter **53** completes the count of the count number S, the swallow counter **53** stops count operation, and the output is kept low. The swallow counter **53** resumes (reloads) count operation in accordance with a change in the output signal of the pulse counter **52**.

[0049] A total division ratio N_{tot} obtained in the frequency divider circuit **32** illustrated in FIG. **6** is represented by the following form: $N_{tot}=N\cdot P+S$. Thus, in the frequency divider circuit **32**, a desired division ratio is obtained by appropriately setting N, P, and S.

[0050] For example, assume that N=16 and N+1=17 are set in the dual-modulus prescaler **51**, the pulse counter **52** is a 7-bit programmable counter, and the swallow counter **53** is a 4-bit programmable counter. Assuming that the count number P set in the pulse counter **52** is represented by P=96 and the count number S set in the swallow counter **53** is represented by S=4, the total division ratio $N_{tot}=16\cdot 96+4=1540$ is obtained. When the frequency f_{ref} of the original reference signal Ref is represented by f_{ref}=50 MHz, $f_{LO}=N_{tot}\cdot f_{ref}=1540\times 50$ MHz=77.000 GHz is obtained.

[0051] The frequency divider circuit illustrated in FIG. **6** is widely known, and further description thereof is therefore omitted. It is noted that the frequency divider circuit illus-

trated in FIG. **6** is an example, and the frequency divider circuit used in each embodiment is not limited to this.

[0052] FIGS. **7**A to **7**C are circuit diagrams of other circuit components, FIG. **7**A is a circuit diagram of each of the filters **34** and **44**, FIG. **7**B is a circuit diagram of each of the phase detectors (PDs) **33** and **43**, and FIG. **7**C is a circuit diagram of the mixer **42**.

[0053] The filter illustrated in FIG. **7**A is a third-order loop filter including combinations of resistors and capacitors. FIG. **7**B illustrates an exclusive OR (XOR) logic circuit that is generally widely used as a simple PD, a reference signal (or an original reference signal) is input to an input Ref which is one input of the XOR logic circuit, and a low-frequency signal is input to an input FD_OUT which is the other input of the XOR logic circuit. FIG. **7**C illustrates a resistive mixer circuit in which a transistor which does not supply power is used as a nonlinear resistor. When a local signal LO and a test signal RF are respectively supplied to a gate of the transistor and one controlled terminal, a low-frequency signal IF subjected to frequency conversion by the nonlinearity of the resistor is obtained from the other controlled terminal.

[0054] The circuits illustrated in FIGS. **7**A to **7**C are widely known, and further description thereof is therefore omitted. It is noted that the circuits illustrated in FIGS. **7**A to **7**C are examples, and the filters, the phase detectors (PDs), and the mixer which are used in each embodiment are not limited to these.

[0055] FIG. **8** illustrates an exemplary circuit of the reference frequency divider circuit **45**.

[0056] The reference frequency divider circuit **45** illustrated in FIG. **8** is a frequency divider circuit constituted by M stages of divide-by-two frequency dividers **60-1** to **60**-M which are connected in series. For example, connection of six stages results in a division ratio of 64, and thus a frequency of 50 MHz of an input is divided down to a frequency of 0.78 MHz. A signal to be input to the reference frequency divider circuit **45** is a signal of 50 MHz, and the reference frequency divider circuit **45** is a lower-speed circuit than the frequency divider circuit **32**, and also includes a small number of stages.

[0057] The frequency divider circuit illustrated in FIG. **8** is widely known, and further description thereof is therefore omitted. It is noted that the frequency divider circuit illustrated in FIG. **8** is an example, and the reference frequency divider circuit **45** used in each embodiment is not limited to this.

[0058] As described above, in contrast to the typical circuit illustrated in FIG. **3**, the test signal generation circuit (PLL-TEST) **40** in the receiver circuit according to the first embodiment does not include a high-speed frequency divider circuit, and newly includes the mixer **42** and the reference frequency divider circuit **45**. Thus, the high-speed frequency divider circuit **22**B used in the circuit illustrated in FIG. **3** does not have to be included. The mixer **42** is a circuit whose power consumption is zero if a resistive mixer is used, and the reference frequency divider circuit **45** is a low-speed frequency divider circuit whose operation speed is such a low speed that the conversion from 50 MHz to 1 MHz is carried out. Thus, power consumption in this case is smaller than that in the case where the high-speed frequency divider circuit is provided.

[0059] FIG. **9** illustrates constituent ratios of power consumed by each component in the receiver circuit in FIG. **3** and the receiver circuit according to the first embodiment in FIG. **4**.

[0060] In the receiver circuit illustrated in FIG. **3**, the total of the power consumption of the VCO **21**A of the PLL-LO **13** and the VCO **21**B of the PLL-TEST **19** is 47.3 mW. The total of the power consumption of the frequency divider circuit **22**A of the PLL-LO **13** and the frequency divider circuit **22**B of the PLL-TEST **19** is 234 mW. The total of the power consumption of the PD **23**A of the PLL-LO **13** and the PD **23**B of the PLL-TEST **19** is 3.8 mW. The total of the power consumption of the reference signal source **20** is 11.4 mW. Thus, the frequency divider circuits **22**A and **22**B make up a sizable proportion of the sum total of power consumption.

[0061] In contrast to this, in the receiver circuit according to the first embodiment, the power consumption of the VCOs **31** and **41**, the power consumption of the PDs **33** and **43**, and the power consumption of the reference signal source **20** are respectively 47.3 mW, 3.8 mW, and 11.4 mW, which are the same as those in the receiver circuit illustrated in FIG. **3**. The power consumption of the frequency divider circuit **32** is 117 mW, which is equal to half the total of the power consumption of the frequency divider circuits **22**A and **22**B illustrated in FIG. **3** because no frequency divider circuit is provided in the PLL-TEST **40**. On the other hand, the power consumptions of the mixer **42** and the reference frequency divider circuit **45** which are newly included in the PLL-TEST **40** according to the first embodiment are respectively 0 mW and 1.5 mW. Hence, the sum total of power consumption in the circuit illustrated in FIG. **3** is 296.5 mW, whereas the sum total of power consumption in the circuit according to the first embodiment is 181 mW, and thus the power consumption is significantly reduced.

[0062] FIG. **10** is a circuit diagram illustrating configurations of a local signal generation circuit (PLL-LO) and a test signal generation circuit (PLL-TEST) in a receiver circuit according to a second embodiment.

[0063] The receiver circuit according to the second embodiment is used as a receiver circuit of a wireless device like that illustrated in FIG. **2**. The receiver circuit according to the second embodiment has the same configuration as that of the first embodiment except that the reference frequency divider circuit **45** divides a frequency f_{ref} of an original reference signal Ref output by the reference signal source **20**.

[0064] As described above, a frequency-divided signal output by the frequency divider circuit **32** of the PLL-LO **30** has a frequency which is equal to the frequency f_{ref} of the original reference signal Ref output by the reference signal source **20**, and, when a feedback loop is stabilized, their phases also match each other. Hence, the original reference signal Ref may be used in place of a frequency-divided signal.

[0065] The receiver circuit according to the second embodiment exhibits an effect similar to that in the first embodiment.

[0066] FIG. **11** is a circuit diagram illustrating configurations of a local signal generation circuit (PLL-LO) and a test signal generation circuit (PLL-TEST) in a receiver circuit according to a third embodiment.

[0067] The receiver circuit according to the third embodiment has the same configuration as the receiver circuit according to the first embodiment except that an initialization circuit is provided at an output of the filter **44** of the test signal generation circuit (PLL-TEST) **40**.

[0068] In the first and second embodiments, a frequency of a test signal is able to be offset with respect to a frequency of a local signal, that is, an absolute value of a frequency difference between the local signal and the test signal has to be

f_{offset}. For this reason, the test signal may be stabilized at both a frequency on a high-frequency side and a frequency on a low-frequency side with respect to the frequency of the local signal. In other words, which side an output frequency of the test signal is stabilized on depends on a circuit initial state, and thus there is uncertainty.

[0069] In the third embodiment, an output from the filter **44**, that is, a control voltage for the VCO **41** is set at a level on one potential side by the initialization circuit, and its state is changed to a stable state, thereby resulting in stabilization in one of low-frequency and high-frequency states.

[0070] In FIG. **11**, the initialization circuit connects a signal line connecting the output of the filter **44** to an input of the VCO **41** to a high-potential power line via a resistor RS and a switch SW. When a predetermined time period has elapsed since the start of operation, the switch SW is put into an open state. Thus, in an initial state, a control voltage is set at a level on a high-potential side, an oscillation frequency of the VCO **41** is an upper limit frequency, feedback control results in a frequency f_{RX} of a test signal in a stable state represented by $f_{RX}=f_{LO}+f_{offset}$, and the frequency of the test signal is located on a high-frequency side with respect to a frequency of a local signal.

[0071] In an example illustrated in FIG. **11**, although the initialization circuit is constituted by the resistor RS and the switch SW, if the resistance of the resistor RS is increased, the switch SW does not have to be provided. Subsequently, a feedback loop moves toward stabilization, and, since the feedback loop moves toward stabilization from the high-frequency side, stability is achieved at a frequency offset to the high-frequency side with respect to the frequency of the local signal.

[0072] Additionally, in FIG. **11**, if the signal line connecting the output of the filter **44** to the input of the VCO **41** is connected to a low-potential power line via the resistor RS and the switch SW, a frequency of a test signal is located on a low-frequency side with respect to a frequency of a local signal.

[0073] Furthermore, to enable switching between a high-frequency side and a low-frequency side on which a frequency of a test signal is set with respect to a frequency of a local signal, the signal line is connected to both a high-potential power line and a low-potential power line via two sets of the resistor RS and the switch SW.

[0074] All examples and conditional language recited herein are intended for pedagogical purposes to aid the reader in understanding the invention and the concepts contributed by the inventor to furthering the art, and are to be construed as being without limitation to such specifically recited examples and conditions, nor does the organization of such examples in the specification relate to a showing of the superiority and inferiority of the invention. Although the embodiments of the present invention have been described in detail, it should be understood that the various changes, substitutions, and alterations could be made hereto without departing from the spirit and scope of the invention.

What is claimed is:

1. A receiver circuit comprising:

a local signal generation circuit that generates a local signal; and

a test signal generation circuit that generates a test signal having a frequency close to a frequency of the local signal,

wherein the test signal generation circuit includes

an oscillator that generates the test signal,

a mixer that mixes the local signal with an output of the oscillator to generate a low-frequency signal which is a difference signal between the local signal and the output of the oscillator,

a phase detector that detects a phase difference between the low-frequency signal output by the mixer and a reference signal, and

a filter that extracts a low-frequency component from an output of the phase detector, and controls an oscillation frequency of the oscillator by using an output of the filter.

2. The receiver circuit according to claim **1**,

wherein the local signal generation circuit performs feedback control in accordance with a phase comparison result between a local frequency-divided signal obtained by dividing the frequency of the local signal and an original reference signal, and

wherein the reference signal is a signal obtained by dividing a frequency of the local frequency-divided signal further.

3. The receiver circuit according to claim **1**,

wherein the local signal generation circuit performs feedback control in accordance with a phase comparison result between a local frequency-divided signal obtained by dividing the frequency of the local signal and an original reference signal, and

wherein the reference signal is a signal obtained by dividing a frequency of the original reference signal.

4. The receiver circuit according to claim **1**,

wherein the test signal generation circuit includes an initialization circuit that initializes the frequency of the test signal output by the oscillator to one of a low frequency and a high frequency with respect to the frequency of the local signal.

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