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Katsukura et al.

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(54) **CONTROLLER OF POWER CONVERSION DEVICE**

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(57) **ABSTRACT**

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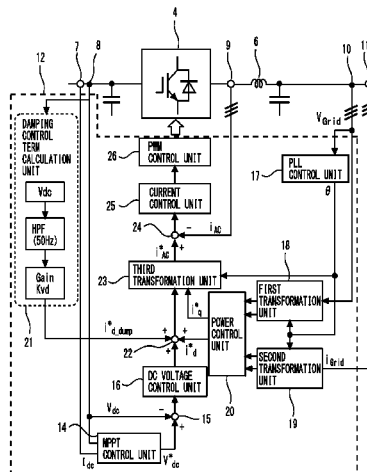
A controller of a power conversion device including a power converter connected between a direct current (DC) power supply and an alternating current (AC) power supply, includes: a damping control term calculation unit configured to calculate a value of pulsation of a DC voltage applied between the DC power supply and the power converter, or pulsation of a DC current flowing between the DC power supply and the power converter; and a current control unit configured to output, to the power converter, a command value for adjusting the power of the power converter so that a pulsation component corresponding to the pulsation value calculated by the damping control term calculation unit is reduced in accordance with a command value based on the value calculated by the damping control term calculation unit. The power conversion device can reduce resonance without including a damping resistor.

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H02M 1/00 (2006.01)
(Continued)

(52) **U.S. Cl.**
CPC **H02M 1/12** (2013.01); **H02M 1/0009** (2021.05); **H02M 1/14** (2013.01); **H02M 7/48** (2013.01)

(58) **Field of Classification Search**
CPC H02M 1/12; H02M 1/0009; H02M 7/48
See application file for complete search history.

1 Claim, 10 Drawing Sheets



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FIG. 1

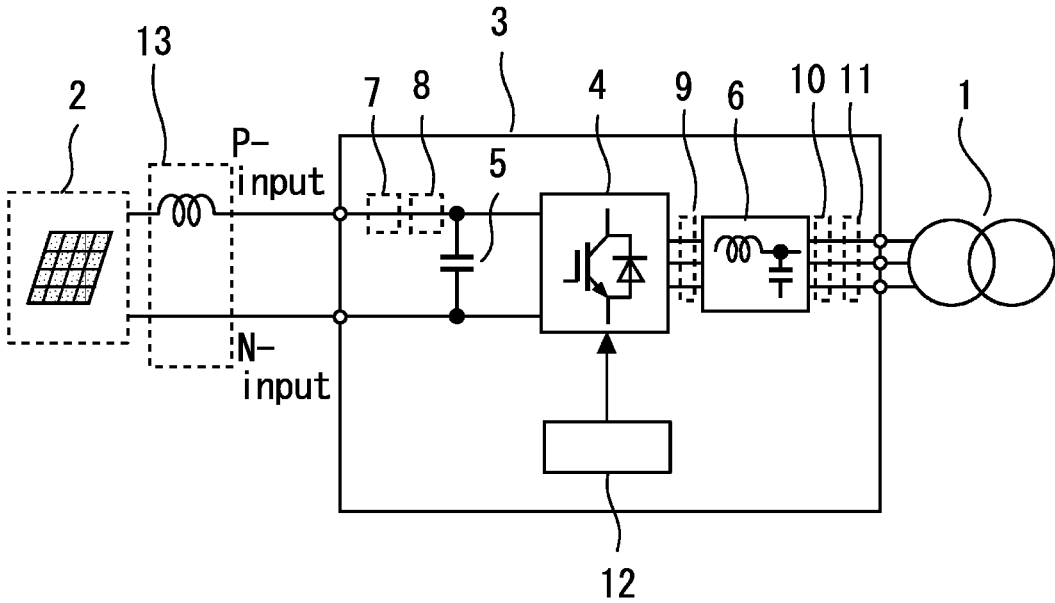


FIG. 2

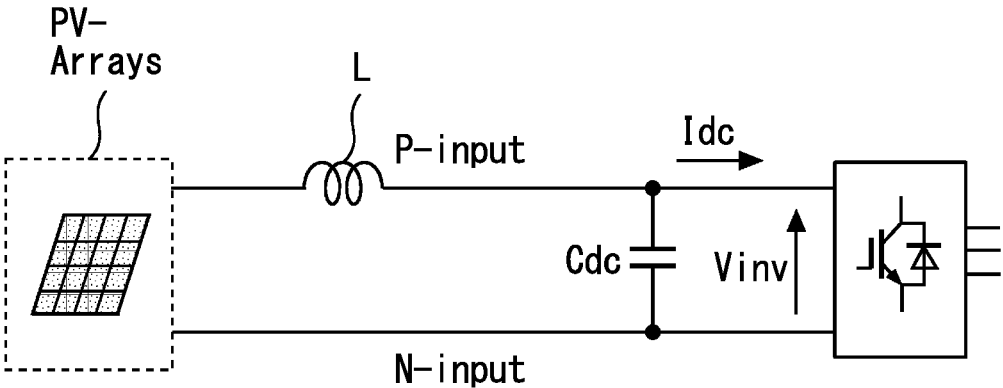


FIG. 3

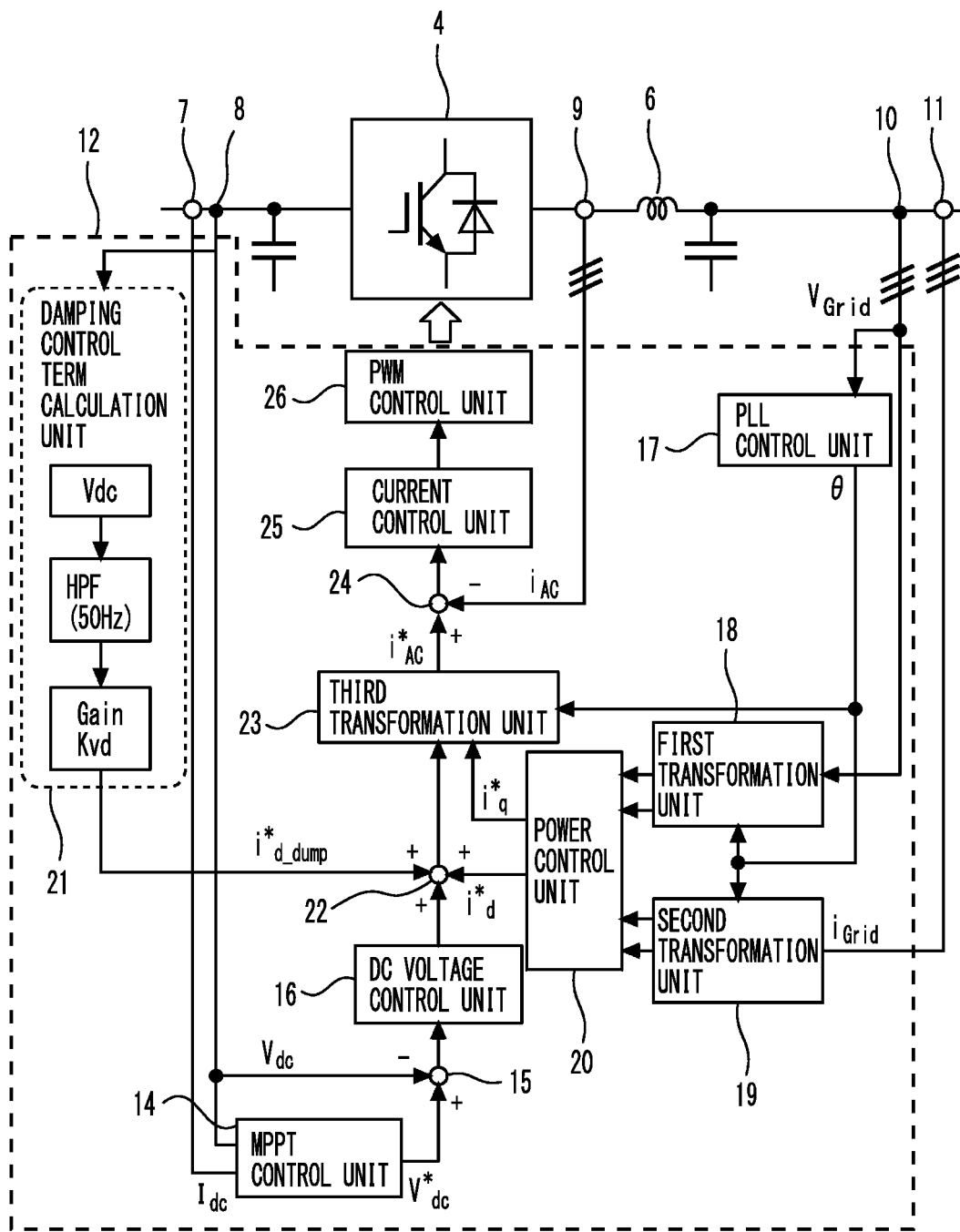


FIG. 4

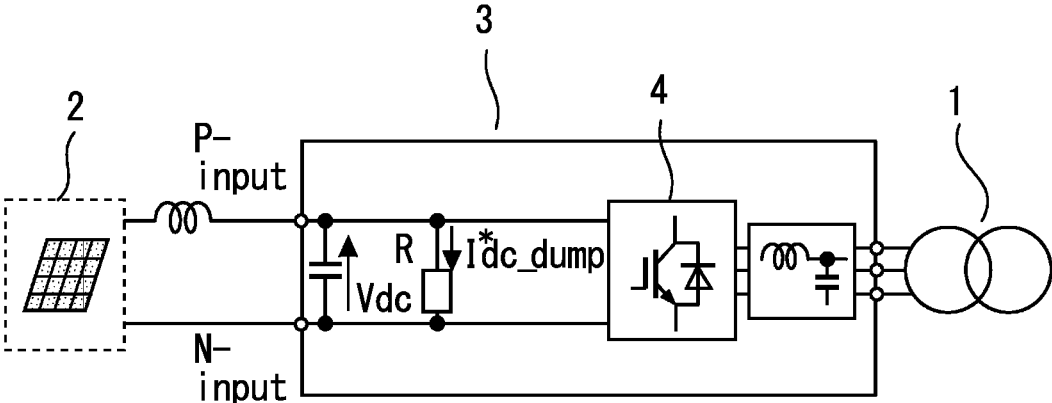


FIG. 5

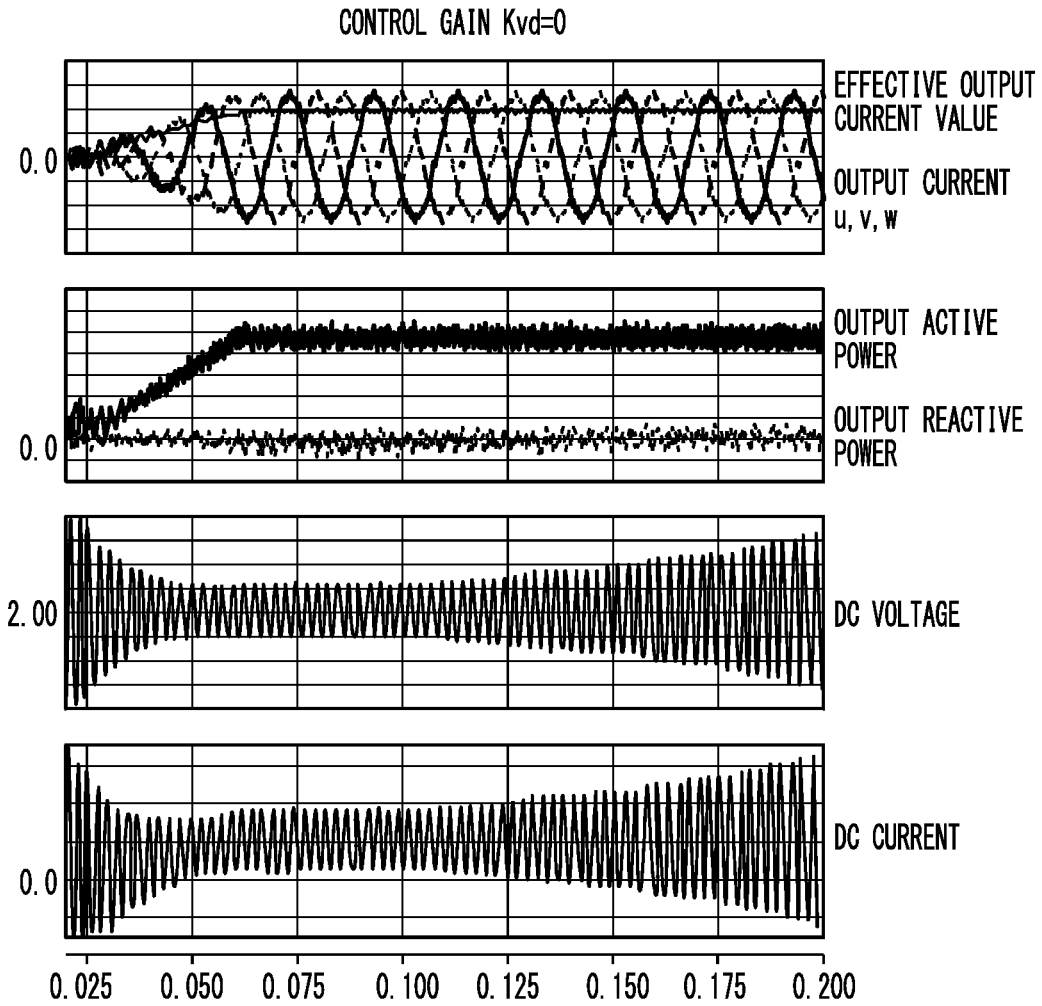


FIG. 6

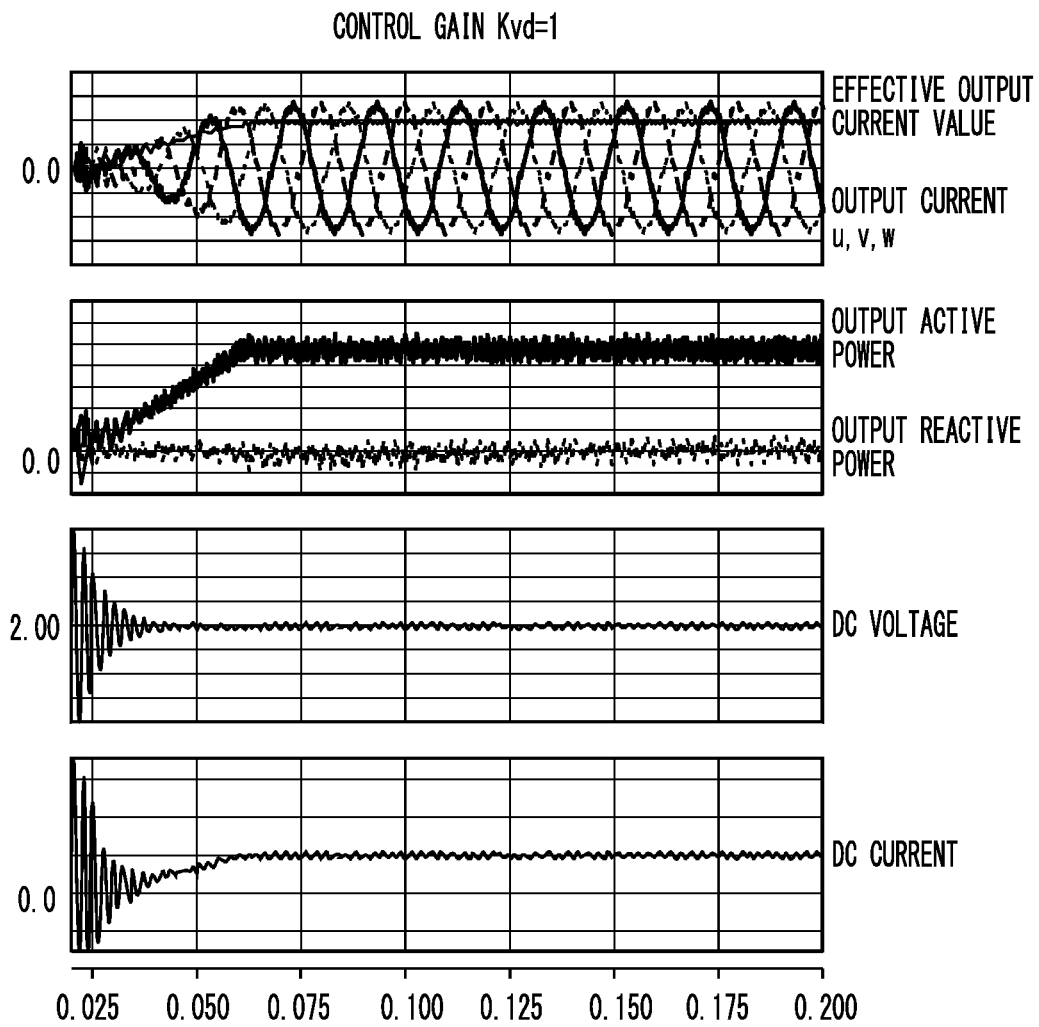


FIG. 7

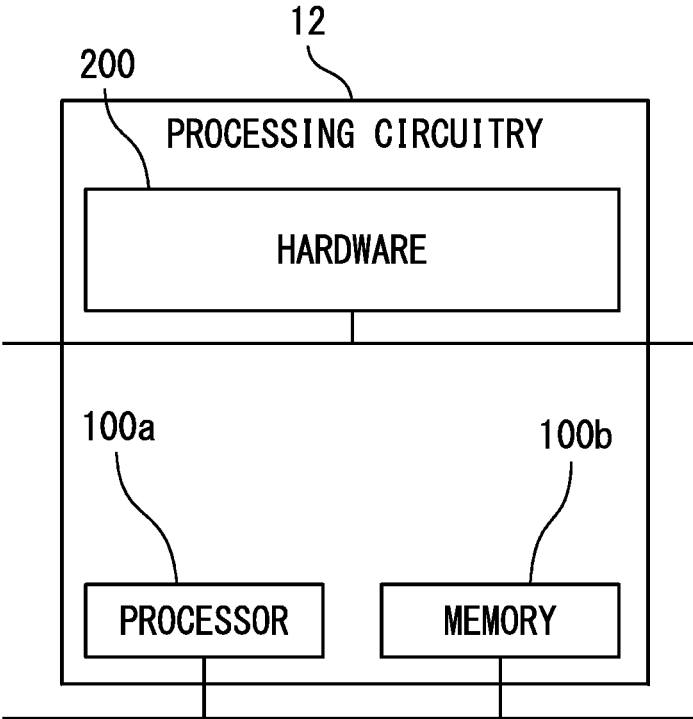


FIG. 8

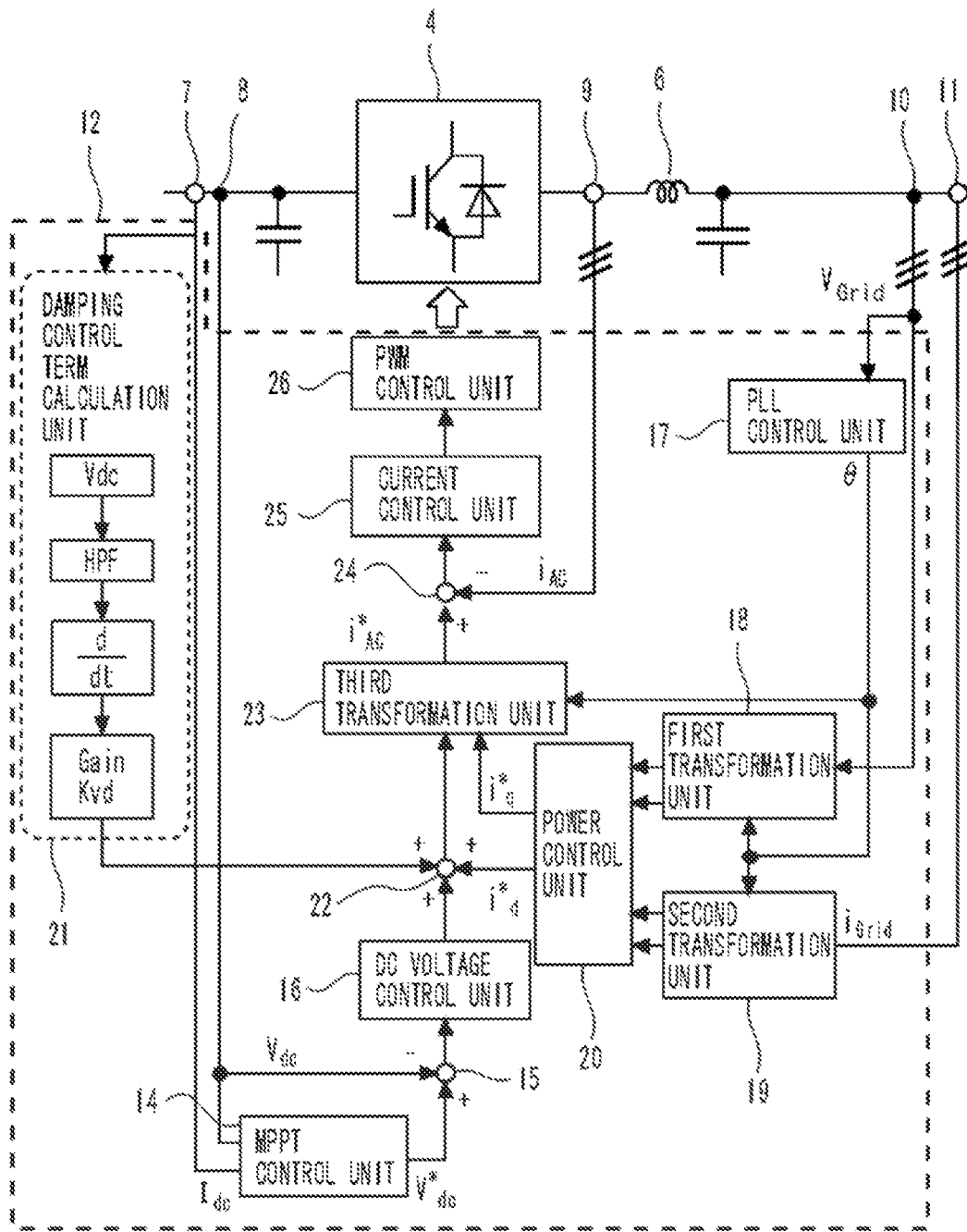


FIG. 9

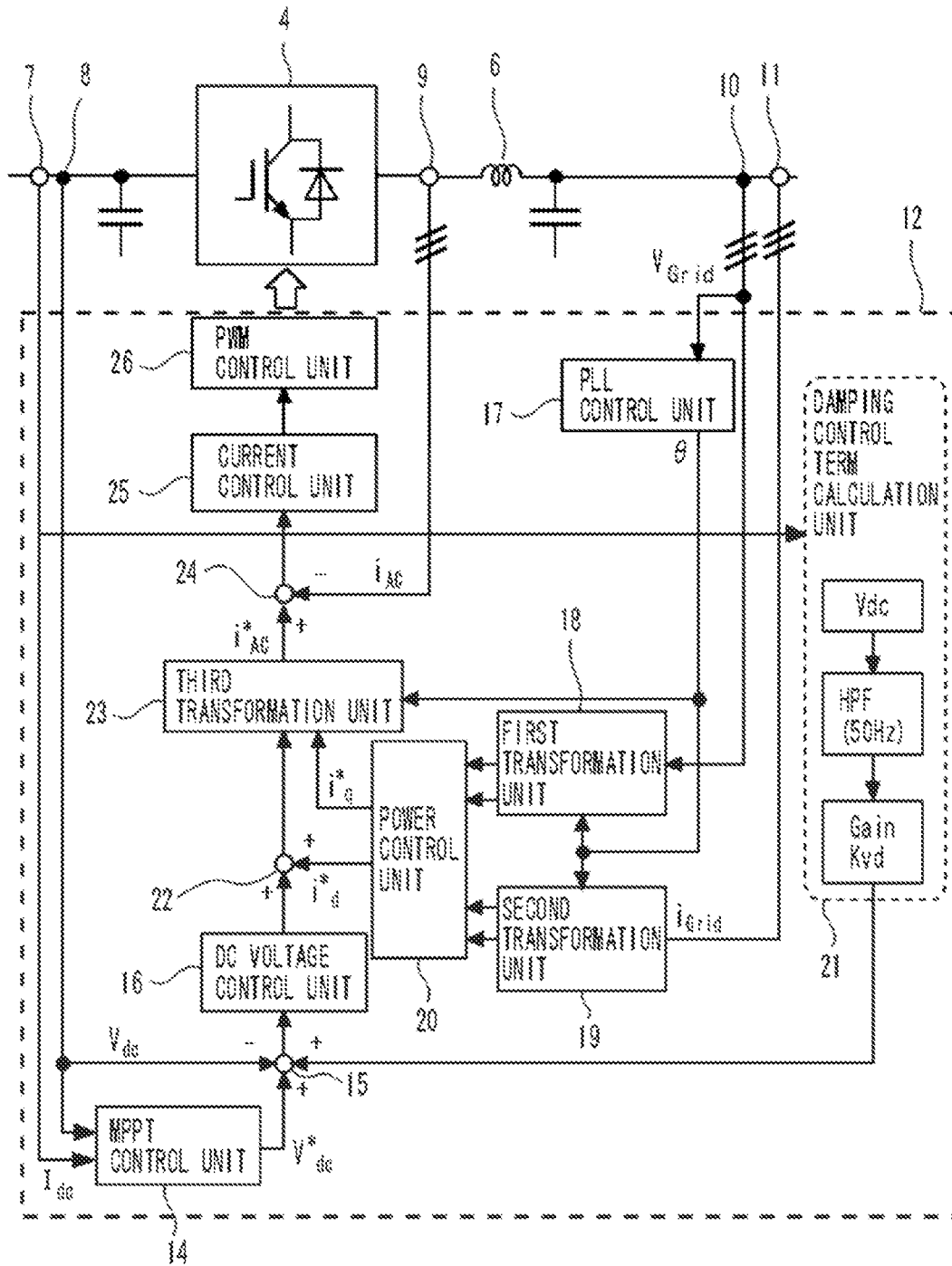
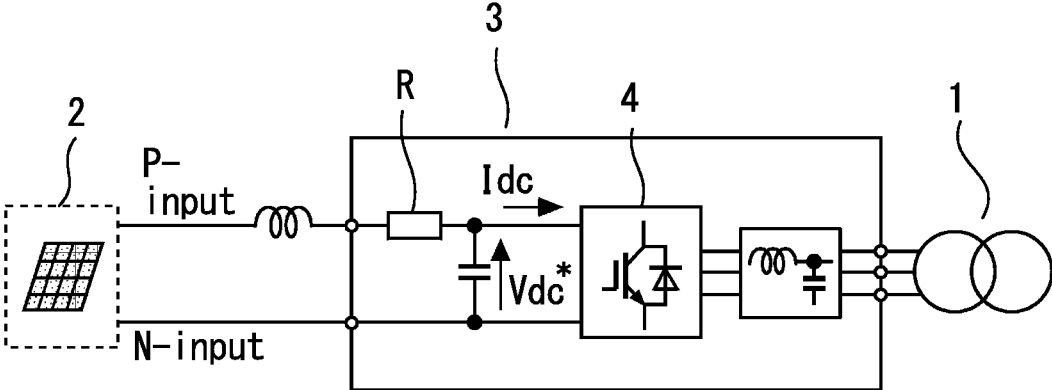


FIG. 10



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**CONTROLLER OF POWER CONVERSION
DEVICE**

FIELD

The present disclosure relates to a controller of a power conversion device.

BACKGROUND

PTL 1 discloses a power conversion device. The power conversion device reduces resonance that occurs in a circuit.

CITATION LIST

Patent Literature

[PTL 1] JP 2020-048361 A

SUMMARY

Technical Problem

However, the power conversion device described in PTL 1 includes a damping resistor in the circuit. Hence a large loss occurs due to the damping resistor.

The present disclosure has been made in order to solve the problem described above. An object of the present disclosure is to provide a controller of a power conversion device that can reduce resonance without including a damping resistor.

Solution to Problem

A controller of a power conversion device according to the present disclosure, the power conversion device including a power converter connected between a direct current (DC) power supply and an alternating current (AC) power supply, includes: a damping control term calculation unit configured to calculate a value of pulsation of a DC voltage applied between the DC power supply and the power converter, or pulsation of a DC current flowing between the DC power supply and the power converter; and a current control unit configured to output, to the power converter, a command value for adjusting the power of the power converter so that a pulsation component corresponding to the pulsation value calculated by the damping control term calculation unit is reduced in accordance with a command value based on the value calculated by the damping control term calculation unit.

Advantageous Effects of Invention

According to the present disclosure, it is possible to control the power converter by using detected pulsation. It is thus possible to reduce resonance without providing a damping resistor.

BRIEF DESCRIPTION OF DRAWINGS

FIG. 1 is a block diagram of a power system to which a controller of a power conversion device in a first embodiment is applied.

FIG. 2 is a diagram for explaining resonance on the DC side of a power conversion system to which the controller of the power conversion device in the first embodiment is applied.

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FIG. 3 is a block diagram of the controller of the power conversion device in the first embodiment.

FIG. 4 is a conceptual diagram in a case where a damping resistor is provided in parallel in a DC circuit of the power conversion device to which the controller of the power conversion device in the first embodiment is applied.

FIG. 5 is a diagram showing simulation results of the controller of the power conversion device in the first embodiment.

FIG. 6 is a diagram showing simulation results of the controller of the power conversion device in the first embodiment.

FIG. 7 is a hardware block diagram of the controller of the power conversion device in the first embodiment.

FIG. 8 is a block diagram of a controller of a power conversion device in a second embodiment.

FIG. 9 is a block diagram of a controller of a power conversion device in a third embodiment.

FIG. 10 is a conceptual diagram in a case where a damping resistor is provided in series in a DC circuit of the power conversion device to which the controller of the power conversion device in the third embodiment is applied.

DESCRIPTION OF EMBODIMENTS

Embodiments will be described in accordance with the accompanying drawings. In the drawings, the same or corresponding parts are denoted by the same reference numerals. The repetitive descriptions of the parts will be simplified or omitted as appropriate.

First Embodiment

FIG. 1 is a block diagram of a power system to which a controller of a power conversion device in a first embodiment is applied.

The power system of FIG. 1 includes an AC power supply 1, a DC power supply 2, and a power conversion device 3.

The AC power supply 1 is operated by an electric power company or the like. For example, the AC power supply 1 is an electric power system. The DC power supply 2 is provided outdoors. For example, the DC power supply 2 is a solar cell. The power conversion device 3 is connected between the AC power supply 1 and the DC power supply 2.

The power conversion device 3 includes a power converter 4, a capacitor 5, a filter 6, a first current detector 7, a first voltage detector 8, a second current detector 9, a second voltage detector 10, a third current detector 11, and a controller 12.

The power conversion device 3 and the DC power supply 2 are connected through a DC cable 13.

The power converter 4 is provided so as to convert a DC voltage into an AC voltage.

The capacitor 5 is provided between the DC power supply 2 and the power converter 4. The capacitor 5 is provided so as to smooth the DC voltage.

The filter 6 is provided between the power converter 4 and the AC power supply 1. The filter 6 is provided so as to reduce the harmonics of the AC current.

The first current detector 7 is provided on the input side of the capacitor 5. The first current detector 7 is provided so as to detect a value I_{dc} of the current that is input to the capacitor 5.

The first voltage detector 8 is provided on the input side of the capacitor 5. The first voltage detector 8 is provided so as to detect a value V_{dc} of the voltage that is input to the capacitor 5.

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The second current detector **9** is provided on the output side of the power converter **4**. The second current detector **9** is provided so as to detect a value i_{AC} of the current flowing on the output side of the power converter **4**.

The second voltage detector **10** is provided on the input side of the AC power supply **1**. The second voltage detector **10** is provided so as to detect a value V_{Grid} of the voltage that is input to the AC power supply **1**.

The third current detector **11** is provided on the input side of the AC power supply **1**. The third current detector **11** is provided so as to detect a value i_{Grid} of the current that is input to the AC power supply **1**.

The controller **12** is connected to the power converter **4**. The controller **12** receives the information of the detected value Idc from the first current detector **7**. The controller **12** receives the information of the detected value Vdc from the first voltage detector **8**. The controller **12** receives the information of the detected value i_{AC} from the second current detector **9**. The controller **12** receives the information of the detected values V_{Grid} from the second voltage detector **10**. The controller **12** receives the information of the detected value i_{Grid} from the third current detector **11**. The controller **12** controls the power converter **4** on the basis of the information of the detected value Vdc, the detected value i_{AC} , the detected value V_{Grid} , and the detected value i_{Grid} . For example, the controller **12** adjusts the power of the power converter **4** so that the pulsation component of the DC voltage is reduced.

Next, resonance on the DC side will be described with reference to FIG. **2**.

FIG. **2** is a diagram for explaining resonance on the DC side of the power conversion system to which the controller of the power conversion device in the first embodiment is applied.

In FIG. **2**, Cdc is the capacitance of the capacitor **5**. L represents the parasitic inductance of the DC cable **13**. Vinv is a DC voltage applied to the power converter **4**. Idc represents a DC current flowing through the power converter **4**.

In general, Idc includes pulsation associated with power conversion. Depending on the magnitude of the inductance L, a resonance frequency with the capacitance Cdc becomes close to a pulsation frequency of Idc, and resonance occurs. In this case, the DC voltage and the DC current vibrate.

Next, a control method in which the controller **12** adjusts the electric power will be described with reference to FIG. **3**.

FIG. **3** is a block diagram of the controller of the power conversion device in the first embodiment.

As shown in FIG. **3**, the controller **12** includes a maximum power point tracking (MPPT) control unit **14**, a first subtraction unit **15**, a DC voltage control unit **16**, a phase-locked loop (PLL) control unit **17**, a first transformation unit **18**, a second transformation unit **19**, a power control unit **20**, the damping control term calculation unit **21**, a first addition unit **22**, a third transformation unit **23**, a second subtraction unit **24**, a current control unit **25**, and a pulse-width modulation (PWM) control unit **26**.

The MPPT control unit **14** receives the input of the information of the detected value Idc from the first current detector **7**. The MPPT control unit **14** receives the input of the information of the detected value Vdc from the first voltage detector **8**. The MPPT control unit **14** performs MPPT control on the basis of the detected value Idc and the detected value Vdc. The MPPT control unit **14** calculates a DC voltage command value V*dc on the basis of the

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detected value Idc and the detected value Vdc. The MPPT control unit **14** outputs the information of the DC voltage command value V*dc.

The first subtraction unit **15** receives the input of the information of the DC voltage command value V*dc from the MPPT control unit **14**. The first subtraction unit **15** receives the input of the information of the detected value Vdc from the first voltage detector **8**. The first subtraction unit **15** calculates a value obtained by subtracting the detected value Vdc from the DC voltage command value V*dc. The first subtraction unit **15** outputs the information of the value obtained by subtracting the detected value Vdc from the DC voltage command value V*dc.

The DC voltage control unit **16** receives the input of the information of the output value of the first subtraction unit **15**. The DC voltage control unit **16** calculates a d-axis current command value on the basis of the input value. The DC voltage control unit **16** outputs the information of the d-axis current command value.

The PLL control unit **17** receives the input of the information of the detected value V_{Grid} of the second voltage detector **10**. The PLL control unit **17** performs PLL control on the basis of the detected value V_{Grid} . The PLL control unit **17** outputs information of a reference phase θ synchronized with the detected value V_{Grid} .

The first transformation unit **18** receives the input of the information of the detected value V_{Grid} of the second voltage detector **10**. The first transformation unit **18** receives the input of the information of the reference phase θ from the PLL control unit **17**. The first transformation unit **18** transforms the detected value V_{Grid} into a d-axis voltage value and a q-axis voltage value by d-q transformation. Note that the q-axis voltage component is set to 0 as the reference phase of the d-q transformation. The first transformation unit **18** outputs the information of the d-axis voltage value and the information of the q-axis voltage value.

The second transformation unit **19** receives the input of the information of the detected value i_{Grid} from the third current detector **11**. The second transformation unit **19** receives the input of the information of the reference phase θ from the PLL control unit **17**. The second transformation unit **19** transforms the detected value i_{Grid} into a d-axis current value and a q-axis current value by the d-q transformation. Note that the q-axis voltage component is set to 0 as the reference phase of the d-q transformation. The second transformation unit **19** outputs the information of the d-axis current value and the information of the q-axis current value.

The power control unit **20** receives the input of the information of the d-axis voltage value and the information of the q-axis voltage value from the first transformation unit **18**. The power control unit **20** receives the input of information of a d-axis current value i^*d and a q-axis current value i^*q from the second transformation unit **19**. The power control unit **20** outputs the information of the d-axis current value i^*_d and the information of the q-axis current value i^*_q .

The damping control term calculation unit **21** receives the input of the information of the detected value Vdc from the first voltage detector **8**. The damping control term calculation unit **21** calculates a voltage pulsation Δv of the capacitor by applying a high-pass filter to the detected value Vdc. The damping control term calculation unit **21** calculates a damping control term $i^*_{d_dump}$ by multiplying the voltage pulsa-

tion value Δv by a preset control gain K_{vd} . The damping control term calculation unit 21 outputs the information of the value of the damping control term.

The first addition unit 22 receives the input of the information of the d-axis current command value from the DC voltage control unit 16. The first addition unit 22 receives the input of the information of the d-axis current value i_d^* from the power control unit 20. The first addition unit 22 receives the input of the information of the value of the damping control term from the damping control term calculation unit 21. The first addition unit 22 adds the d-axis current value i_d^* and the value of the damping control term to the d-axis current command value. The first addition unit 22 outputs the information of the value obtained by the addition.

The third transformation unit 23 receives the input of the information of the reference phase θ from the PLL control unit 17. The third transformation unit 23 receives the input of the information of the i_q^* of the q-axis current value from the power control unit 20. The third transformation unit 23 receives the input of the information of the calculated value from the first addition unit 22. The third transformation unit 23 performs inverse d-q transformation on the input value to calculate each phase current command value i_{AC}^* . The third transformation unit 23 outputs the information of each phase current command value i_{AC}^* .

The second subtraction unit 24 receives the input of the information of the detected value i_{AC} from the second current detector 9. The second subtraction unit 24 receives the input of the information of each phase current command value i_{AC}^* from the third transformation unit 23. The second subtraction unit 24 subtracts the value of the detected value i_{AC} from the value of the detected value i_{AC}^* . The second subtraction unit 24 outputs the information of the value obtained by the subtraction.

The current control unit 25 receives the input of the information of the calculated value from the second subtraction unit 24. The current control unit 25 calculates a voltage command value on the basis of the input value. The current control unit 25 outputs the information of the voltage command value.

The PWM control unit 26 receives the input of the information of the voltage command value from the current control unit 25. The PWM control unit 26 performs PWM control on the power converter 4 on the basis of the voltage command value. For example, the PWM control unit 26 outputs, to the power converter 4, a gate signal for performing the PWM control on the power converter 4 on the basis of the voltage command value.

Next, the concept of the damping control term will be described with reference to FIG. 4.

FIG. 4 is a conceptual diagram in a case where a damping resistor is provided in parallel in a DC circuit of the power conversion device in the first embodiment is applied.

By using the damping control term $i_{d_dump}^*$ described in FIG. 3, the current $i_{dc_dump}^*$ shown in Equation (1) below is added to the DC side of the power converter 4.

$$I_{dc_dump}^* = v_d \times i_{d_dump}^* / V_{dc} \quad (1)$$

In Equation (1), v_d is the d-axis voltage of the AC voltage.

When $i_{d_dump}^* = K_{vd} \times \Delta V_{dc}$ is substituted into Equation (1), Equation (2) below is obtained.

$$I_{dc_dump}^* = v_d \times K_{vd} / V_{dc} \times \Delta V_{dc} \quad (2)$$

In Equation (2), ΔV_{dc} is the voltage pulsation of the capacitor.

Here, v_d is the d-axis voltage of the AC voltage and V_{dc} is the DC voltage, and can thus be considered to be almost constant. When $1/R = v_d \times K_{vd} / V_{dc}$, Equation (3) below is obtained.

$$I_{dc_dump}^* = 1/R \times \Delta V_{dc} \quad (3)$$

In regard to the pulsation component, the damping control shown in FIG. 3 is equivalent to providing the damping resistor in parallel in the DC circuit of the power conversion device as shown in FIG. 4. Therefore, the pulsation-reducing effect is obtained as in the case where the damping resistor is provided.

Next, simulation results of the switching of the DC voltage damping control will be described with reference to FIGS. 5 and 6.

FIGS. 5 and 6 are diagrams showing the simulation results of the controller of the power conversion device in the first embodiment.

FIG. 5 shows simulation results when the control gain K_{vd} is 0. The top graph is a graph showing an effective output current value and output currents of a U-phase, a V-phase, and a W-phase. The second graph from the top is a graph showing output active power and output reactive power. The third graph from the top is a graph showing a DC voltage. The bottom graph is a graph showing a DC current.

In FIG. 5, when the output current, the output active power, and the output reactive power are each output as shown in the top graph and the second graph from the top, pulsation occur in the DC voltage and the DC current as shown in the third graph from the top and the bottom graph.

FIG. 6 shows simulation results when the control gain K_{vd} is 1. The top graph is a graph showing an effective output current value and output currents of a U-phase, a V-phase, and a W-phase. The second graph from the top is a graph showing output active power and output reactive power. The third graph from the top is a graph showing a DC voltage. The bottom graph is a graph showing a DC current.

In FIG. 6, as shown in the top graph and the second graph from the top, the output current, the output active power, and the output reactive power are each output as in FIG. 5. As shown in the third graph from the top and the bottom graph, the pulsation is reduced in the DC voltage and the DC current.

Next, with reference to FIG. 7, an example of the controller 12 will be described.

FIG. 7 is a hardware block diagram of the controller of the power conversion device in the first embodiment.

Each function of the controller 12 can be realized by processing circuitry. For example, the processing circuitry includes at least one processor 100a and at least one memory 100b. For example, the processing circuitry includes at least one dedicated hardware 200.

When the processing circuitry includes at least one processor 100a and at least one memory 100b, each function of the controller 12 is realized by software, firmware, or a combination of the software and the firmware. At least one of the software and the firmware is described as a program. At least one of the software and the firmware is stored into at least one memory 100b. At least one processor 100a reads out and executes the program stored in at least one memory 100b, thereby realizing each function of the controller 12. At least one processor 100a is also referred to as a central processing unit, a processing unit, an arithmetic unit, a microprocessor, a microcomputer, or a digital signal processor (DSP). For example, at least one memory 100b may be a non-volatile or volatile semiconductor memory, such as random-access memory (RAM), read-only memory (ROM),

flash memory, erasable programmable ROM (EPROM), or electrically erasable programmable ROM (EEPROM), a magnetic disk, a flexible disk, an optical disk, a compact disk, a mini-disk, a digital versatile disc (DVD), or the like.

When the processing circuitry includes at least one dedicated hardware **200**, the processing circuitry is realized by, for example, a single circuit, a composite circuit, a programmed processor, a parallel programmed processor, an application-specific integrated circuit (ASIC), a field-programmable gate array (FPGA), or a combination thereof. For example, the functions of the controller **12** are each realized by the processing circuitry. For example, the functions of the controller **12** are collectively realized by the processing circuitry.

Some of the functions of the controller **12** may be realized by the dedicated hardware **200**, and the others may be realized by the software or the firmware. For example, some functions of the controller **12** may be realized by the processing circuitry as the dedicated hardware **200**, and the other functions of the controller **12** may be realized by at least one processor **100a** reading and executing the program stored in at least one memory **100b**.

In this manner, the processing circuitry realizes each function of the controller **12** by the hardware **200**, the software, the firmware, or a combination thereof.

According to the first embodiment described above, the controller **12** adjusts the power of the power converter **4** so that the pulsation component of the DC voltage is reduced. It is thus possible to reduce resonance without providing a damping resistor.

The controller **12** calculates a d-axis current command value by using the voltage pulsation of the capacitor **5** and controls the power converter **4**. Therefore, the pulsation can be reduced as in the case where the damping resistor is provided in parallel on the DC side of the power conversion device **3**.

Specifically, an amount proportional to a DC voltage Δv is added to the power of the power converter **4**. Thus, a DC current Δi added on the DC side of the power converter **4** is substantially proportional to Δv . Therefore, it is possible to obtain a damping effect on a high-frequency component, the effect being similar to that in the case where the damping resistor is provided in parallel on the DC side of the power converter **4**.

When the resonance having occurred between the capacitor **5** and the inductance L is large, depending on the magnitude of the inductance on the DC side, the power conversion device **3** may detect a DC overvoltage and come to a protective stop. In contrast, according to the first embodiment, the pulsation of the DC voltage is reduced, whereby the occurrence of the protective stop can be prevented.

In the power system, also, when a system disturbance such as an instantaneous voltage drop or an instantaneous power failure occurs, a Fault Ride Through function is required to continue the operation of the power converter **4**. When a sudden change occurs in the phase and amplitude of the system voltage, the output power or the DC voltage of the power converter **4** changes suddenly. As a result, the power conversion device **3** may detect an overvoltage and come to a protective stop. In contrast, according to the first embodiment, the pulsation of the DC voltage is reduced, whereby the occurrence of the protective stop can be prevented.

When harmonics are included in the system voltage and the power converter **4** outputs a fundamental current, the power which is the product of the voltage and the current has

pulsation of a frequency component which is the sum and difference of the frequency of the harmonics of the system voltage and the fundamental frequency of the output current. Therefore, the DC voltage may pulsate. As a result, the ripple current of the capacitor **5** in the power conversion device **3** increases, which may cause a loss of a margin for the ripple current rating or an increase in temperature. In contrast, according to the first embodiment, such phenomena can be prevented by reducing the pulsation of the DC voltage.

It has been described in FIG. **2** that the resonance occurs between the parasitic inductance of the DC cable **13** and the capacitor **5**, but a DC reactor may be provided between the power converter **4** and the DC power supply in order to remove the switching ripples of the power converter **4**. In this case, resonance may occur between the DC reactor and the capacitor **5**. In contrast, according to the first embodiment, the damping control by the controller **12** can reduce the pulsation of the DC voltage.

In the first embodiment, the example of the case where the DC power supply is the solar cell has been shown. However, also in the case of a DC power supply except for the solar cell, the pulsation of the DC voltage can be reduced by a controller similar to the controller **12**. In this case as well, a similar reduction in pulsation can be realized by adding, to the d-axis current command value or the AC power command value, a value obtained by multiplying the DC voltage pulsation component, obtained by applying a high-pass filter to the measured DC voltage value, by a control gain.

Second Embodiment

FIG. **8** is a block diagram of a controller of a power conversion device in a second embodiment. Note that the same or corresponding parts as those of the first embodiment are denoted by the same reference numerals. The descriptions of the parts will be omitted.

As shown in FIG. **8**, the damping control term calculation unit **21** receives the input of the information of the detected value I_{dc} from the first current detector **7**. The damping control term calculation unit **21** calculates a pulsation component $\Delta i1$ by applying a high-pass filter to the detected value I_{dc} . The damping control term calculation unit **21** differentiates $\Delta i1$ with time. The damping control term calculation unit **21** calculates a damping control term by multiplying the value, obtained by differentiating $\Delta i1$ with time, by a preset control gain K_{vd} . The damping control term calculation unit **21** outputs the information of the damping control term.

According to the second embodiment described above, the controller **12** adjusts the power of the power converter **4** so that the pulsation component of the DC current is reduced. It is thus possible to reduce resonance without providing a damping resistor.

The controller **12** controls the power converter **4** on the basis of the command value of the AC current calculated using the value obtained by differentiating the pulsation component value of the DC current with time. Hence the pulsation can be reduced as in a case where the damping resistor is provided in series on the DC side of the power conversion device **3**.

Specifically, an amount proportional to the DC current $\Delta i1$ is added to the power of the power converter **4**. Thus, a DC current $\Delta i2$ added on the side closer to the power converter **4** than the capacitor **5** is substantially proportional to $\Delta i1$. By charging the capacitor **5** with $\Delta i2$, the voltage pulsation Δv of the capacitor **5** is substantially proportional to the integral

of Δi_2 . As a result, Δv is substantially proportional to Δi_1 . Therefore, it is possible to obtain a damping effect on a high-frequency component, the effect being similar to that in the case where the damping resistor is provided in series on the DC side of the power conversion device 3.

Third Embodiment

FIG. 9 is a block diagram of the controller 12 of the power conversion device 3 in a third embodiment. Note that the same or corresponding parts as those of the first embodiment are denoted by the same reference numerals. The descriptions of the parts will be omitted.

As shown in FIG. 9, the damping control term calculation unit 21 receives the input of the information of the detected value I_{dc} from the first current detector 7. The damping control term calculation unit 21 calculates a pulsation component Δi_1 by applying a high-pass filter to the detected value I_{dc} . The damping control term calculation unit 21 calculates a damping control term by multiplying Δi_1 by a preset control gain K_{id} .

The first subtraction unit 15 receives the input of the information of the DC voltage command value V^*_{dc} from the MPPT control unit 14. The first subtraction unit 15 receives the input of the information of the detected value V_{dc} from the first voltage detector 8. The first subtraction unit 15 receives the input of the information of the damping control term from the damping control term calculation unit 21. The first subtraction unit 15 calculates a value obtained by subtracting the detected value V_{dc} from a value obtained by adding the DC voltage command value V^*_{dc} and the damping control term. The first subtraction unit 15 outputs information of a value obtained by subtracting the detected value V_{dc} from the value obtained by adding the DC voltage command value V^*_{dc} and the damping control term.

Next, the concept of the damping control term will be described with reference to FIG. 10.

FIG. 10 is a conceptual diagram in a case where the damping resistor is provided in series in the DC circuit of the power conversion device to which the controller of the power conversion device in the third embodiment is applied.

In the conceptual diagram of FIG. 10, Equation (4) below holds. The damping control term calculation unit 21 (not shown in FIG. 10) calculates a damping control term on the basis of Equation (4).

$$V_{dc}^* = K_{id} \times \Delta I_{dc} \tag{4}$$

In Equation (4), V_{dc}^* is a voltage. K_{id} is a control gain. ΔI_{dc} is a current pulsation.

According to the third embodiment described above, the controller 12 controls the power converter 4 on the basis of the command value of the DC voltage calculated using the pulsation component value of the DC current. It is thus possible to reduce resonance without providing a damping resistor.

INDUSTRIAL APPLICABILITY

As described above, the controller of the power conversion device of the present disclosure can be used for a power system.

REFERENCE SIGNS LIST

- 1 AC power supply
- 2 DC power supply
- 3 Power conversion device
- 4 Power converter
- 5 Capacitor
- 6 Filter
- 7 First current detector
- 8 First voltage detector
- 9 Second current detector
- 10 Second voltage detector
- 11 Third current detector
- 12 Controller
- 13 DC cable
- 14 MPPT control unit
- 15 First subtraction unit
- 16 DC voltage control unit
- 17 PLL control unit
- 18 First transformation unit
- 19 Second transformation unit
- 20 Power control unit
- 21 Damping control term calculation unit
- 22 First addition unit
- 23 Third transformation unit
- 24 Second subtraction unit
- 25 Current control unit
- 26 PWM control unit
- 100a Processor
- 100b Memory
- 200 Hardware
- R Resistor

The invention claimed is:

1. A controller of a power conversion device, the power conversion device including a power converter connected between a direct current (DC) power supply and an alternating current (AC) power supply, the controller comprising:

- a damping control term calculation unit configured to calculate a value of pulsation of a DC voltage applied between the DC power supply and the power converter, or pulsation of a DC current flowing between the DC power supply and the power converter; and
- a current control unit configured to output, to the power converter, a command value for adjusting power of the power converter on a basis of a command value of AC current, calculated using a value obtained by differentiating a pulsation component value of the DC current with time, so that the pulsation component corresponding to the pulsation value calculated by the damping control term calculation unit is reduced in accordance with a command value based on the value calculated by the damping control term calculation unit.

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