

### (54) THERMOSENSITIVE RECORDING MATERIAL

- Company, Philadelphia, PA (US) (56) References Cited
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- **Example 19 Second Particle PATENT PATENT DOCUMENTS**<br>
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- (\*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days. patent is extended or adjusted under 33 Primary Examiner — Bruce H Hess<br>U.S.C. 154(b) by 0 days. (74) Attorney, Agent, or Firm — Reid S. Willis
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- (21) Appl. No.: **15/366,102**<br>(22) Filed: **Dec. 1, 2016** (22) Filed: Dec. 1, 2016

### (65) **Prior Publication Data**

US 2017/0158887 A1 Jun. 8, 2017

### Related U.S. Application Data

- (60) Provisional application No.  $62/263,161$ , filed on Dec. 4, 2015.
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(52) U.S. Cl.<br>CPC ............... *C09D 7/1291* (2013.01); *B41M 5/44*  $(2013.01);$   $C09D$   $7/1275$   $(2013.01);$   $C09D$ 7/1283 (2013.01); C09D 125/14 (2013.01);  $B41M$  2205/04 (2013.01);  $B41M$  2205/38 (2013.01)

# (12) United States Patent (10) Patent No.: US 9,932,487 B2<br>Einsla et al. (45) Date of Patent: Apr. 3, 2018

### $(45)$  Date of Patent: Apr. 3, 2018

Field of Classification Search CPC . B41M 5/44; B41M 2205/04; B41M 2205/38 USPC . 503 / 207 MATERIAL CPC . B41M 5/44; B41M 2205/04; B41M 2205<br>(71) Applicants: Dow Global Technologies LLC,<br>Midland, MI (US); Rohm and Haas<br>Midland , MI (US): Rohm and Haas





### ( 57 ) ABSTRACT

The present invention relates to a thermosensitive recording material comprising paper , an undercoat layer disposed on the paper, and a thermosensitive recording layer disposed on the undercoat layer, wherein the undercoat layer comprises a binder and first and second hollow sphere polymer par ticles , wherein the first hollow sphere polymer particles have a diameter in the range of from  $1.2 \mu m$  to  $1.8 \mu m$ ; the second hollow sphere polymer particles have a diameter in the range of from  $0.25 \mu m$  to  $1.0 \mu m$ ; the number ratio of the second to the first hollow sphere polymer particles is in the range of from 1:1 to 20:1; the diameter of the second hollow sphere polymer particles is in the range of from 15 to 65% of the diameter of the first hollow sphere polymer particles; the dry bulk density of the first hollow sphere polymer particles is in the range of 0.25 to 0.5 g/mL; and the dry bulk density of the second hollow sphere polymer particles is in the range of 0.30 to 0.90  $g/mL$ .

### 9 Claims, No Drawings

The present invention relates to a thermosensitive record-<br>in the dry bulk density of the second hollow sphere polymer<br>ing material comprising an undercoat layer disposed on particles is in the range of 0.30 to 0.90 g/mL.

The use of undercoats for thermosensitive recording  $\frac{10}{\text{s}}$  showing improved strength and improved optical densitive recording material applications. materials is known to prevent undesirable absorption of ink into the paper and to provide thermal insulation for the into the paper and to provide thermal insulation for the DETAILED DESCRIPTION OF THE paper. Consequently, coated paper produces sharper brighter MVENTION

15 images and has better reflectivity than uncoated paper.<br>
U.S. Pat. No. 6,531,183 discloses a coating composition<br>
comprising binder and hollow pigment particles for improv-<br>
in a first and spect, the present invention is a comprise second pigment particles that may be solid or neutralized acid cores, wherein "vacuolated" and may be the same or different size as the  $20\alpha$ ) the first core-shell polymer r "vacuolated" and may be the same or different size as the 20 a) the first core-shell polymer particles have a diameter in first particles.<br>first particles.

st particles.<br>U.S. Pat. No. 6,780,820, discloses a variety of undercoats b) the second core-shell polymer particulars including those containing, inorganic pigments used in the range of from  $0.25 \mu m$  to  $1.0 \mu m$ ;<br>above critical pigment volume concentration coatings, fine c) the number ratio of the second to the first core-shell above critical pigment volume concentration coatings, fine c) the number ratio of the second to the first core organic single voided particles, or multivoided particles. 25 polymer particles is in the range of from 1:1 to

derived from a composition comprising a binder and a in the range of from 15 to 65% of the diameter of the first<br>bimodal distribution of first and second hollow polymeric core-shell polymer particles; bimodal distribution of first and second hollow polymeric core-shell polymer particles;<br>pigments with acid-free hydrophilic cores and with volume e) the dry bulk density of the first core-shell polymer pigments with acid-free hydrophilic cores and with volume e) the dry bulk density of the first core-shell mean diameters generally in the range of 300 to 1.100 nm, 30 particles is in the range of 0.25 to 0.5 g/mL; and

position technology to find a material suitable for use as an particles is in the range of 0.30 to 0.90 g/mL.<br>undercoat that provides a balance of strength of the paper The binder is the film-forming component of the coati

position comprising an aqueous dispersion of a binder and 40 first and second core-shell polymer particles having aqueous first and second core-shell polymer particles having aqueous typically in the range of 2 to 50, more preferably to 30 meutralized acid cores, wherein weight percent, based on the weight of the composition.

b) the second core-shell polymer particles have a diameter in 45 the range of from  $0.25 \mu m$  to  $1.0 \mu m$ ;

in the range of from 15 to 65% of the diameter of the first 50 preferably from 1.3  $\mu$ m, and most preferably from 1.4  $\mu$ m to core-shell polymer particles;<br>1.8  $\mu$ m, preferably to 1.7  $\mu$ m, and more preferably to 1.6

particles is in the range of 0.30 to 0.90 g/mL.<br>
In a second aspect, the present invention is thermosensi-<br>
in a second aspect, the present invention is thermosensi-<br>
in a second aspect, the present invention is thermosens disposed on the undercoat layer, wherein the undercoat layer with particles sizes from 500 nm to 1  $\mu$ m are, by definition, comprises a binder and a bimodal distribution of first and 60 the diameter that is measured by L

range of from 0.25 to 1.0 µm;<br>
c) the number ratio of the second to the first hollow sphere Particle diameters for the second core-shell polymer par-

polymer particles is in the range of from 1:1 to 20:1; ticles with particle sizes from 250 nm to less than 500 nm is,

THERMOSENSITIVE RECORDING d) the diameter of the second core-shell polymer particles is<br>MATERIAL in the range of from 15 to 65% of the diameter of the first in the range of from 15 to 65% of the diameter of the first core-shell polymer particles;

BACKGROUND OF THE INVENTION e) the dry bulk density of the first hollow sphere polymer

particles is in the range of 0.25 to 0.5 g/mL; and f) the dry bulk density of the second hollow sphere polymer

the undercoat layer.<br>The use of undercoats for thermosensitive recording <sup>10</sup> showing improved strength and improved optical density for

first and second core-shell polymer particles having aqueous

b) the second core-shell polymer particles have a diameter in the range of from  $0.25 \mu m$  to  $1.0 \mu m$ ;

organic single voided particles, or multivoided particles. 25 polymer particles is in the range of from 1:1 to 20:1;<br>U.S. Pat. No. 8,334,047 discloses the use of an undercoat d) the diameter of the second core-shell polyme

mean diameters generally in the range of 300 to 1,100 nm. 30 particles is in the range of 0.25 to 0.5 g/mL; and<br>It would be an advance in the art of undercoating com-<br>f) the dry bulk density of the second core-shell polyme

polyvinyl acetates, (poly)vinyl-acrylics, (poly)styrene-<br>SUMMARY OF THE INVENTION acetates acrylics, (poly)styrene-butadiene, (poly)vinyl acetate/ethyl-<br>ene, (poly)vinyl-acrylics, polyurethanes, polyacrylamides, In a first aspect, the present invention is a coating com-<br>sition comprising an aqueous dispersion of a binder and 40 the binder for the composition of the present invention is

a) the first core-shell polymer particles have a diameter in The composition further comprises first and second core-<br>the range of from 1.0  $\mu$ m to 1.8  $\mu$ m; shell polymer particles having aqueous neutralized acid shell polymer particles having aqueous neutralized acid cores. These particles are known as hollow sphere particles the range of from  $0.25 \mu m$  to  $1.0 \mu m$ ; or opaque polymers and can be prepared by methods known c) the number ratio of the second to the first core-shell in the art. (See, for example, U.S. Pat. No. 6.020.435).

polymer particles is in the range of from 1:1 to 20:1;<br>d) the diameter of the second core-shell polymer particles is<br>the range of from 1.0  $\mu$ m, preferably from 1.2  $\mu$ m, more the range of from 1.0  $\mu$ m, preferably from 1.2  $\mu$ m, more preferably from 1.3  $\mu$ m, and most preferably from 1.4  $\mu$ m to e) the dry bulk density of the first core-shell polymer The second core-shell polymer particles have a diameter in particles is in the range of 0.25  $\mu$ m,  $\mu$  or  $\mu$  the range of from 0.25  $\mu$ m, preferably from 0.3  $\$ particles is in the range of 0.25 to 0.5 g/mL; and the range of from 0.25 µm, preferably from 0.3 µm, more f) the dry bulk density of the second core-shell polymer preferably from 0.35 µm, and most preferably from 0.4 µm,

second hollow sphere polymer particles, wherein using a  $100 \times$  oil immersion lens with a  $1.63$  numerical a) the first hollow sphere particles have a diameter in the aperture; each diameter reading is made by on screen a) the first hollow sphere particles have a diameter in the aperture; each diameter reading is made by on screen range of from  $1.0 \text{ }\mu\text{m}$  to  $1.8 \text{ }\mu\text{m}$ ; range of from 1.0  $\mu$ m to 1.8  $\mu$ m; reading of the edge-to-edge distance of the greatest distance b) the second hollow sphere particles have a diameter in the through the center of the particles and is averaged over at through the center of the particles and is averaged over at least 10 particles.

terized by a dry bulk density in the range of from 0.25, polymer particles is in the range of from 1:1, preferably from preferably from 0.30, more preferably from 0.35 g/mL to  $\,$  s  $\,$  2:1, more preferably from 3:1, an preferably from 0.30, more preferably from 0.35 g/mL to 5 2:1, more preferably from 3:1, and most preferably from 4:1, 0.5, preferably to 0.45, and more preferably to 0.40 g/mL. to 20:1, preferably to 15:1, and more prefer An example of a commercial product suitable for use as an wherein the diameter of the second hollow sphere polymer aqueous dispersion of first core-shell polymer particles is particles is in the range of from 15, preferabl aqueous dispersion of first core-shell polymer particles is particles is in the range of from 15, preferably from 20, more ROPAQUE<sup>TM</sup> TH-2000 Opaque Polymer (a Trademark of preferably from 25, most preferably from 27 per The Dow Chemical Company or its Affiliates). Dry bulk 10 preferably to 40, more preferably to 33, and most preferably density is measured in accordance with the procedure dis-<br>closed in U.S. Pat. No. 6,020,435, Column 16,

acterized by a dry bulk density in the range of from 0.30, 15 preferably from 0.30, more preferably from 0.35 g/mL to preferably from 0.40, more preferably from 0.50, and most 0.5, preferably to 0.45, and more preferably preferably from 0.55 g/mL, to 0.90, preferably to 0.80, more The second hollow sphere polymer particles are further preferably to 0.75, and most preferably to 0.65 g/mL. An characterized by a dry bulk density in the range example of a commercial product suitable for use as an preferably from 0.40, more preferably from 0.50, and most aqueous dispersion of second core-shell polymer particles is 20 preferably from 0.55  $\alpha$ /mL, to 0.90, prefe aqueous dispersion of second core-shell polymer particles is 20 preferably from 0.55 g/mL, to 0.90, preferably to 0.80, ROPAQUE<sup>TM</sup> ULTRA E Opaque Polymer. preferably to 0.75, and most preferably to 0.65 g/mL.

The number ratio of the second to the first core-shell The undercoat layer can be applied to the paper by any of polymer particles is in the range of from 1:1, preferably from a variety of means such as roll applicator, we 2:1, more preferably from 3:1, and most preferably from 4:1, curtain coater, or jet methods. The undercoat layer may be to  $20:1$ , preferably to  $15:1$ , more preferably to  $12:1$ ; and  $25$  smoothed by any of a variety of

from 25, most preferably from 27 percent, to 65, preferably g/m<sup>2</sup>, to 40, more preferably to 33, and most preferably to 30  $\frac{9}{m^2}$ . percent of the diameter of the first core-shell polymer A thermosensitive recording layer, which typically comparticles. By way of example, if the first core-shell polymer prises a leuco dye (see U.S. Pat. No. 4,929,590), particles. By way of example, if the first core-shell polymer prises a leuco dye (see U.S. Pat. No. 4,929,590), is then particles have a diameter of 1.5  $\mu$ m and the second core-shell applied over the undercoat layer, typ particles have a diameter of 1.5 µm and the second core-shell applied over the undercoat layer, typically at a thickness in polymer particles have a diameter of 425 nm, the diameter the range of from 1  $g/m^2$  to 20  $g/m^2$ of the second core-shell polymer particles is  $0.425/1.5$  or  $35 \text{ g/m}^2$ . The thermosensitive recording layer may also com-<br>28.3% of the diameter of the first core-shell polymer par-<br>prise a variety of other additives in

and second core-shell polymer concentration, when the composition is applied as a film, is typically in the range of 40 EXAMPLES from 50 to 98%, preferably to 95%. Preferably, the PVC of the film is above critical. It has been discovered that under-<br>coats with surprising strength can be prepared at above-<br>Pigment Formulation coats with surprising strength can be prepared at above-<br>critical PVCs.

other inorganic or polymeric pigments such as calcium  $\mu$ m diameter, 151.8 g, 31.9 g dry weight, dry bulk density carbonate, calcined kaolin, TiO<sub>2</sub>, ZnO, Al(OH)<sub>2</sub>, BaSO<sub>2</sub>, 0.36 g/mL, void fraction 65%) was added to a carbonate, calcined kaolin,  $TiO_2$ , ZnO, Al(OH)<sub>3</sub>, BaSO<sub>4</sub>, 0.36 g/mL, void fraction 65%) was added to a vessel with and SiO<sub>2</sub>, but may be practiced in the absence of ancillary stirring followed by addition of a slurry pigments. The composition may also include other additives ULTRA E Opaque Polymer (0.4 µm diameter, 3.07 g, 0.95 such as defoamers, crosslinking agents, surface active 50 g dry weight, dry bulk density 0.58 g/mL, void frac such as defoamers, crosslinking agents, surface active  $50 \text{ g}$  dry weight, dry bulk density 0.58 g/mL, void fraction agents and thermofusible materials, but may be practiced in  $45\%$ ), followed by addition of RHOPLEX<sup>T</sup> agents, and thermofusible materials, but may be practiced in the absence of ancillary additives.

as an undercoat (intermediate first layer) for thermosensitive 1.5% volume fraction) then water (1.2 g) to form an aqueous<br>recording layer disposed on paper. Accordingly, in a second 55 suspension having a solids content o material comprising paper, an undercoat layer disposed on 85% (with TH-2000 accounting for 83.4% and ULTRA E the paper, and a thermosensitive recording layer disposed on accounting for 1.6%) and the number ratio of TH2000 the paper, and a thermosensitive recording layer disposed on accounting for  $1.6\%$  the undercoat laver, wherein the undercoat laver comprises ULTRA E was  $\sim 1.1$ . the undercoat layer, wherein the undercoat layer comprises ULTRA E was  $\sim$  1:1.<br>a binder and first and second hollow sphere polymer part - 60 The number of particles per gram of dry pigment is<br>ticles, wherein the first h ticles, wherein the first hollow sphere polymer particles have calculated by first calculating the volume (V) of a single a diameter in the range of from 1.0 um, preferably from 1.2 particle and then converting volume to m a diameter in the range of from 1.0 µm, preferably from 1.2 particle and then converting volume to mass using the <br>um, more preferably from 1.3 µm, and most preferably from known dry bulk density (d) of the pigment particl um, more preferably from 1.3 um, and most preferably from known dry bulk density (d) of  $1.4 \text{ um}$ , to  $1.8 \text{ um}$ , preferably to  $1.7 \text{ um}$ , and more preferably the mass of a single particle: 1.4  $\mu$ m, to 1.8  $\mu$ m, preferably to 1.7  $\mu$ m, and more preferably to 1.6  $\mu$ m; wherein the second hollow sphere polymer 65 to 1.6  $\mu$ m; wherein the second hollow sphere polymer 65  $v=4/3\pi r^3$ ably from 0.3  $\mu$ m, more preferably from 0.35  $\mu$ m, and most m=Vxd

by definition, that diameter that is measured using a preferably to 0.4  $\mu$ m, to 1  $\mu$ m, preferably to 0.8  $\mu$ m, more BI90Plus particle size analyzer. 90Plus particle size analyzer.<br>The first core-shell polymer particles are further charac-<br>the number ratio of the second to the first hollow sphere

to Column 17, lines 1-7.<br>The first hollow sphere polymer particles are further char-<br>The second core-shell polymer particles are further char-<br>characterized by a dry bulk density in the range of from 0.25,

most preferably to 10:1. <br>The diameter of the second core-shell polymer particles is and a variety of method of methods including a blade smooth rod, a grooved rod, or a wire wound<br>The diameter of the second core-shell pol The diameter of the second core-shell polymer particles is rod. The final dried coat weight of the undercoat layer is in the range of from 15, preferably from 20, more preferably typically in the range of from 1, more pref typically in the range of from 1, more preferably from 2  $g/m^2$ , to 25, more preferably to 10, and most preferably to

the range of from 1 g/m<sup>2</sup> to 20 g/m<sup>2</sup>, more preferably to 10 g/m<sup>2</sup>. The thermosensitive recording layer may also comticles. crosslinking agents, surface active agents, and thermofusible<br>The total pigment volume concentration (PVC) of the first materials.

The composition of the present invention may include 45 A slurry of ROPAQUETM TH-2000 Opaque Polymer (1.5 aer inorganic or polymeric pigments such as calcium  $\mu$ m diameter, 151.8 g, 31.9 g dry weight, dry bulk density the absence of ancillary additives.<br>The coating composition of the present invention is useful fraction), then polyvinyl alcohol (13.45 g, 1.95 g dry weight, PVC of the dried coating prepared from the formulation was 85% (with TH-2000 accounting for 83.4% and ULTRA E

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The number of particles per gram is simply 1/m. Using TABLE 2 this approach, the number ratio of ULTRA E and TH-2000 were calculated as follows:

 $5.15\times10^{13}$  particles/g ULTRA E $\times$ 0.95 g ULTRA E=4.9 $\times10^{13}$ particles of ULTRA E

 $1.57\times10^{12}$  particles/g TH-2000 $\times31.9$  g TH-2000=5.0 $\times10^{13}$  particles TH-2000

## ULTRA E: TH-2000~1:1  $^{10}$

A series of formulations were made varying the pigment amounts as shown in Table 1. For Examples 2-11 and C2, the total PVC of the dry coating was 87.5% with the binder and the polyvinyl alcohol remaining the same accounting for the remaining 12.5%. Water additions were adjusted to maintain  $15$ a solids content of  $\sim$  25%. ULTRA E # fraction refers to the number fraction of ULTRA E with respect to TH-2000.<br>Volume fraction refers to the volume fraction of ULTRA E with respect to TH-2000. C1-C3 refer to comparative

Preparation of Thermal Print La The undercoated paper samp			ULTRA E Number Fraction and Volume Fraction with Respect to TH-2000		
$g/m2$ thermal imaging material developer using substantially the	25	Volume fraction	Ratio of ULTRA E to TH-2000	ULTRA E #fraction	$Ex. \#$
the undercoat.		$\Omega$	0:1	0	C1
<b>Optical Density Measurements</b>		0.02	1:1	0.5	
The coated papers were printer-	30	0.04	2:1	0.67	2
F1405-98(2013); an Atlantek Pa		0.05	3:1	0.75	
		0.07	4:1	0.8	4
used. The conditions for printing		0.09	5:1	0.83	
printer were as follows: 50		0.10	6:1	0.86	6
sequence dot pulse duration up t		0.12	7:1	0.88	
$35$ The printhead resistance was $\theta$		0.13	8:1	0.89	8
		0.15	9:1	0.9	9
voltage of 21.5 V. The printed the		0.16	10:1	0.91	10
of the coated paper was measu		0.65	100:1	0.99	11
X-Rite 428 handheld spectroder		0.95	1000:1	0.999	C <sub>2</sub>
Table 3 illustrates the effect of					C <sub>3</sub>

The samples were coated on paper as follows: A  $9" \times 12"$  <sup>45</sup> sheet of paper (weight 72  $g/m^2$ ) was placed on a drawdown machine and secured with a clip on the top. A strip of scotch tape was applied across the top of the paper to be coated to prevent the subsequently applied coating from leaching  $\frac{50}{2}$ through the paper. A wire wound rod was laid across the top of the paper above the tape, and a bead of coating was laid across the paper on the tape using a pipette. The rod was moved down the paper to coat the paper evenly to form an undercoat layer (weight  $\sim$  4 to 4.5 g/m<sup>2</sup>). The coated sheets<br>were placed on a piece of cardboard and dried for 1 min at 55 where placed on a piece of cardboard and dried for 1 min at  $\frac{55}{200}$ . The data show that a balance of IGT-VVP strength and  $\frac{1}{200}$  C, then represent from the oriental and dried for 1 min at  $\frac{1}{200}$  C, then rep  $80^{\circ}$  C., then removed from the oven and allowed to equili-<br>here for 2 h in a contralled toware time and humidity recontraction to a range of from about 0.67 to about 0.91. brate for 2 h in a controlled temperature and humidity room<br>
Freparation of Non-Hollow Polystyrene Beads<br>
Freparation of Non-Hollow Polystyrene Beads (CTR) set to 22° C. and 50% relative humidity.<br>Three batches of aqueous dispersions of non-hollow poly-

the test are reported in terms of viscosity-velocity-product<br>
(IGT-VVP), which is a measure of coating strength. Table 2 A 4-necked round bottom flask equipped with a mechani-(IGT-VVP), which is a measure of coating strength. Table 2 shows the relationship between the number fraction of small





with respect to TH-2000. C1  $\epsilon$  refer to comparative The results demonstrate that the bimodal formulation examples 1-3. TABLE 1<br>
occurring over the ULTRA E number fraction range of 0.80<br>
to 0.95.<br>
The undercoated paper samples were coated with ~3.5<br>
The undercoated paper samples were coated with ~3.5

 $g/m<sup>2</sup>$  thermal imaging material containing leuco dye and a developer using substantially the procedure used to prepare the undercoat.

<sup>0</sup> The coated papers were printed in accordance with ASTM F1405-98(2013); an Atlantek Paper Tester Model 200 was used. The conditions for printing using an Atlantek thermal<br>printer were as follows: 50% checkerboard pattern, sequence dot pulse duration up to 0.8 ms, Tcycle = 5.000 ms. The printhead resistance was 629 ohms with an applied voltage of 21.5 V. The printed thermal paper optical density of the coated paper was measured at 0.4 mJ/dot using an X-Rite 428 handheld spectrodensitometer.

Table 3 illustrates the effect of number fraction of small opaque polymers (ULTRA E) to OD print optical density.

	$40$ opaque polymers (ULTRA E) to OD print optical density.			
The formulations were used to form undercoats as described in the following section.		<b>TABLE 3</b>		
Preparation of an Undercoat		Print Optical Density as a Function of ULTRA E Number Fraction		
The samples were coated on paper as follows: A $9" \times 12"$ <sup>45</sup> sheet of paper (weight $72 \text{ g/m}^2$ ) was placed on a drawdown	Ex. #	ULTRA E #fraction	Ratio of ULTRA E to TH-2000	OD
machine and secured with a clip on the top. A strip of scotch tape was applied across the top of the paper to be coated to	C <sub>1</sub>	0 0.50	1:1	1.01 1.03
prevent the subsequently applied coating from leaching		0.67	2:1	1.20
through the paper. A wire wound rod was laid across the top of the paper above the tape, and a bead of coating was laid	10	083 0.91	5:1 10:1	1.07 1.10
across the paper on the tape using a pipette. The rod was moved down the negate coat the negative worlds to form on	11 C <sub>3</sub>	0.99	100:1	1.01 0.93

The bads with different diameters were prepared to<br>Coating strength was measured with an IGT printability demonstrate the effect of particle size ratios on coating Coating strength was measured with an IGT printability demonstrate the effect of particle size ratios on coating tester in accordance with ASTM T-499 su-64. The results of strength as follows.

shows the relationship between the number fraction of small 65 cal stirrer and reflux condenser was charged with DI water opaque polymers (ULTRA E) and the coating strength, as  $(1535 \text{ g})$  and heated to 92° C. To this fl opaque polymers (ULTRA E) and the coating strength, as  $(1535 \text{ g})$  and heated to 92° C. To this flask was added ammonium persulfate (4 g in 90 g water) and a seed latex ammonium persulfate  $(4 g in 90 g water)$  and a seed latex

(104.5 g, 41% solids, 60 nm). A monomer emulsion con-<br>taining DI water (815 g), sodium dodecylbenzene sulfonate the range of from 0.25 to 1 µm; taining DI water (815 g), sodium dodecylbenzene sulfonate (25.5 g, 22.5% solids), styrene (1256 g) and methacrylic acid (38.87 g) was added over 120 min. An ammonium polymer particles is in the range of from 1:1 to 20:1;<br>persulfate solution (2 g in 120 g water) wan concurrent with  $\frac{5}{4}$  the diameter of the second hollow sphere pol persulfate solution (2 g in 120 g water) wan concurrent with 5 d) the diameter of the second hollow sphere polymer<br>the monomer emulsion feed. During the course of the<br>reaction the temperature was maintained at 88° C. Foll over 15 min. The reaction was then cooled to 75° C. and a 10<br>solution of ferrous sulfate (32.4 g, 0.15% active was<br>charged). Residual monomers were reduced by feeding a<br>solution of t-butylhydroperoxide (0.80 g in 25 g wat isoascorbic acid (1.10 g in 25 g water). The resulting wherein the first hollow sphere polymer particles have a<br>diameter in the range of from 1.2 µm to 1.8 µm; and the dispersion had a solids content of  $32.4\%$  and a particle size 15 of 187 nm.

described for the preparation of the 200-nm beads except for particles is in the range of from 2:1 to 15:1; wherein the range the second bollow polymer particles in the range the seed latex (105.4 g, 45% solids, 100 nm). The resulting  $20^{\circ}$  diameter of the second hollow polymer particles in the range diameter of the first hollow sphere dispersion had a solids content of 31.8% and a particle size of 286 nm.<br>
of 200 nm Polystyrene Beads (DS3) 3. The thermosensitive recording material of claim 2

described for the preparation of the 200-nm beads except for 25 unameter in the range of from 1.5 um to 1.7 um; and the seed latex (133.7 a 32% solids 143 nm). The resulting second hollow sphere polymer particles have a d the seed latex (133.7 g, 32% solids, 143 nm). The resulting second hollow sphere polymer particles have a diameter in<br>the range of from 0.35 µm to 0.6 µm; wherein the number dispersion had a solids content of 31.7% and a particle size the range of from 0.55 um to 0.6 um; wherein the number of 407 nm.

coating strength, which can be measured using hollow or the range of from 25 to 33% of non-hollow spheres. Table 3 shows the effect of particle hollow sphere polymer particles. diameter of the second (smaller) polymer particles on IGT-<br>VVP. In each of these experiments, the first (larger) polymer<br>particles on IGT-<br>particles were 1.5 µm, the PVC was 87.5%, and the small 35<br>particles were 1.5 µm, particle number fraction was 0.91. Name refers to the name<br>of the dianomian of small notumer particles: OB 06 refers to the number of from 4:1 to 10:1; wherein the of the dispersion of small polymer particles; OP-96 refers to particles is in the range of from 4:1 to 10:1; wherein the polymer particles is in diameter of the second hollow sphere polymer particles is in ROPAQUETM OP-96 Opaque Polymer; AF-1055 refers to diameter of the second hollow sphere polymer particles is in<br>ROPAQUETM AF-1055 Opaque Polymer (a Trademark of the range of from 27 to 30% of the diameter of the first ROPAQUETM AF-1055 Opaque Polymer (a Trademark of the range of from 27 to 30% of the diameter of the first<br>The Dow Chaptical Company or its Affiliated Styrano 1.2, 40 hollow sphere polymer particles; and wherein the first The Dow Chemical Company or its Affiliates). Styrene  $1, 2, 40$  hollow sphere polymer particles have a diameter in the range and  $2$  all non-hollow sphere polymer particles have a diameter in the range and 3 all non-hollow sphere beads that were prepared as  $\frac{\text{mol}(\text{low sphere power})}{\text{of from 1.4 }\mu\text{m to 1.6 }\mu\text{m}}$ .

The Effect of Particle Size Ratio on Coating Strength							
Small Particle diameter (µm)	Name	Ratio	<b>IGT-VVP</b>				
	AF-1055	0.67	8				
0.5	OP-96	0.33	32				
0.42	<b>ULTRA E</b>	0.28	36				
0.41	PS1	0.27	29				
0.29	PS2	0.19	15				
0.19	PS3	0.13	12				

The results demonstrate that the strongest coatings are  $\frac{p}{2}$ . The thermosensitive recording material of claim 1 formed with small to large particle ratios around 0.28. The invention claimed is:

1. A thermosensitive recording material comprising paper, 60 range of from 1 to 25 g/m<sup>-</sup>, and the thickness of the an undercoat layer disposed on the paper, and a thermosenan undercoating layer disposed on the paper, and a dictionary and the expection of claim 1<br>stive recording layer disposed on the undercoatilayer,<br>wherein the dried coat weight of the undercoat layer is in the wherein the undercoat layer comprises a binder and first and second hollow sphere polymer particles, wherein:

a) the first hollow sphere particles have a diameter in the  $65$  range of from 1.0  $\mu$ m to 1.8  $\mu$ m;

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- c) the number ratio of the second to the first hollow sphere<br>polymer particles is in the range of from  $1:1$  to  $20:1$ ;
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second hollow sphere polymer particles have a diameter in the range of from  $0.3 \mu m$  to  $0.8 \mu m$ ; wherein the number Preparation of 300-nm Polystyrene Beads (PS2) the range of from 0.5 um to 0.6 um; wherein the number<br>The 200 mm heads were prepared substantially equal to the second to the first hollow sphere polymer The 300-nm beads were prepared substantially as ratio of the second to the first hollow sphere polymer particles is in the range of from 2:1 to 15:1; wherein the

Preparation of 400-nm Polystyrene Beads (PS3)<br>The thermosensitive recording material of claim 2<br>The 400-nm beads were prepared substantially as wherein the first hollow sphere polymer particles have a The 400-nm beads were prepared substantially as wherein the first hollow sphere polymer particles have a scribed for the preparetion of the 200 nm beads except for 25 diameter in the range of from 1.3 µm to 1.7 µm; and th of 407 nm.<br>
Particles list in the range of from 3:1 to 12:1; wherein the Particles in Particles in the first holder of the second hollow sphere polymer particles in Particle size ratios were found to have a notable effect on  $30<sup>o</sup>$  diameter of the second hollow sphere polymer particles in

diameter to the large particle diameter.<br>5. The thermosensitive recording material of claim 2<br>wherein the dry bulk density of the first hollow sphere TABLE 4<br>
<sup>45</sup> polymer particles is in the range of 0.30 to 0.45 g/mL; and<br>
e Size Ratio on Coating Strength<br>
particles is in the range of 0.40 to 0.80 g/mL.

> 6. The thermosensitive recording material of claim 3 wherein the dry bulk density of the first hollow sphere polymer particles is in the range of 0.35 to 0.40 g/mL; and the dry bulk density of the second hollow sphere polymer particles is in the range of 0.50 to 0.75  $g/m\bar{L}$ .<br>7. The thermosensitive recording material of claim 4

wherein the dry bulk density of the first hollow sphere  $_{55}$  polymer particles is in the range of 0.35 to 0.40 g/mL; and the dry bulk density of the second hollow sphere polymer particles is in the range of 0.55 to 0.65 g/mL.

wherein the dried coat weight of the undercoat layer is in the range of from 1 to 25  $g/m^2$ , and the thickness of the

range of from 2 to 6 g/m<sup>2</sup>, and the thickness of the recording layer is in the range of from 1 g/m<sup>2</sup> to 10 g/m<sup>2</sup>.