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Tsuchida et al.

(54) HERMETIC ROTARY COMPRESSOR

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(56) **References Cited**

U.S. PATENT DOCUMENTS

5,222,885 A *	6/1993	Cooksey	F04C 29/023
		_	418/94
5,533,875 A *	7/1996	Crum	F04C 23/008
			417/368

(Continued)

FOREIGN PATENT DOCUMENTS

JP	49-133204 U	11/1974	
JP	63-58872 U	4/1988	
	(Continued)		

OTHER PUBLICATIONS

International Search Report of the International Searching Authority dated Apr. 2, 2013 for the corresponding international application No. PCT/JP2012/083098 (and English translation).

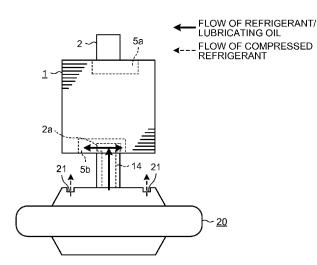
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(57) **ABSTRACT**

A rotor has at its two axis end portions an upper largediameter inner circumferential portion and a lower largediameter inner circumferential portion that have inner diameters larger than the inner diameter of the axially middle portion of the rotor and are offset in the radial direction. A crankshaft has a passageway, which is formed in the crankshaft and allows refrigerant to flow therethrough, and a gas venting hole, which provides communication between the passageway and at least one discharge opening formed in the outer circumferential surface of the crankshaft. The at least one discharge opening is formed at a position facing the inner circumferential surface of the lower large-diameter inner circumferential portion 5b on the compression unit side.

3 Claims, 6 Drawing Sheets



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See application file for complete search history.

(56)

References Cited

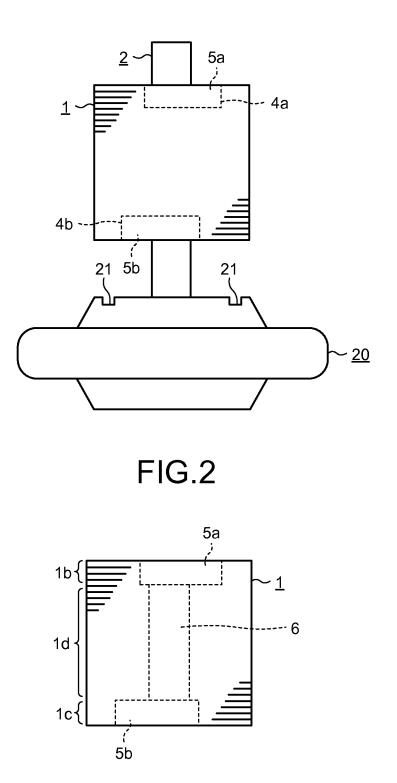
U.S. PATENT DOCUMENTS

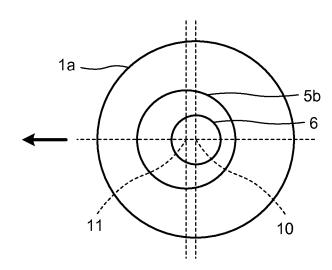
6,000,917	A *	12/1999	Smerud F04C 23/008
			417/366
6,305,914	B1 *	10/2001	Lifson F04C 29/0021
			417/410.5
2004/0042917	A1*	3/2004	Chang, II F04C 23/008
			417/410.5
2008/0078618	Al*	4/2008	Lee F04C 18/356
		_ /	184/6.2
2008/0175738	Al*	7/2008	Jung F04C 18/0215
			418/55.6
2008/0226483	Al*	9/2008	Iwanami F01C 21/10
		0/0000	418/97
2009/0041603	Al *	2/2009	Ginies F04C 18/0215
2012/0107151		5/2012	418/55.6
2012/0107151	A1*	5/2012	Yokoyama F04B 39/16
			417/366

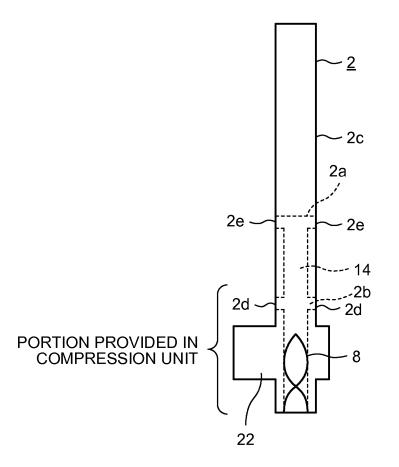
FOREIGN PATENT DOCUMENTS

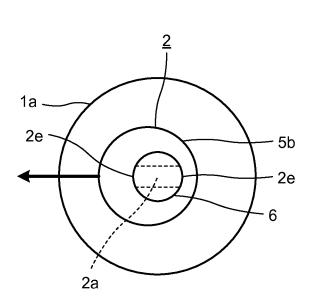
JP	01-152935 A	6/1989
JP	05-316672 A	11/1993
JP	2000-213483 A	8/2000
JP	2001-349284 A	12/2001
JP	2002-089476 A	3/2002

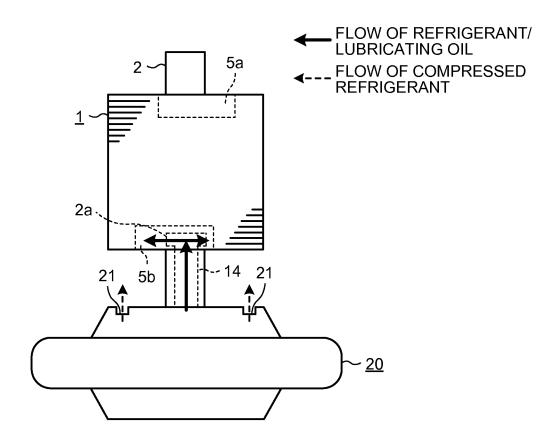
* cited by examiner

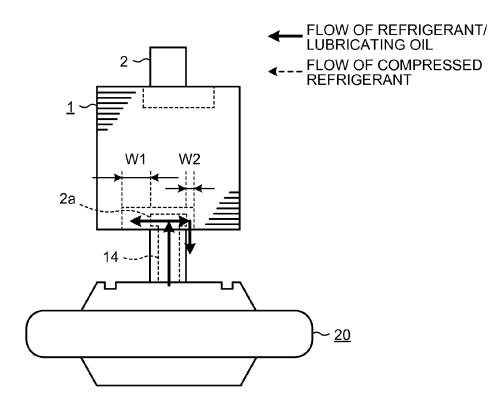


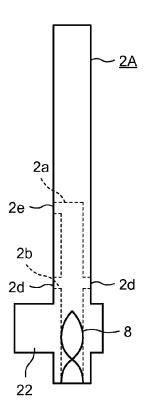




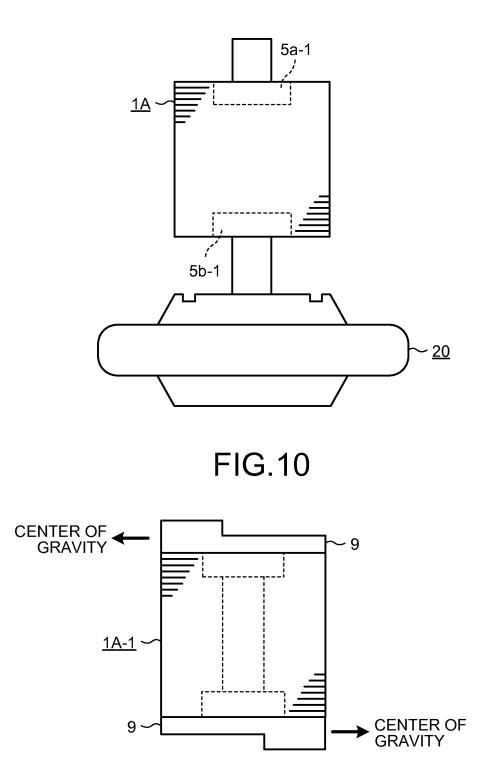












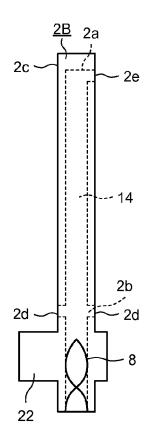
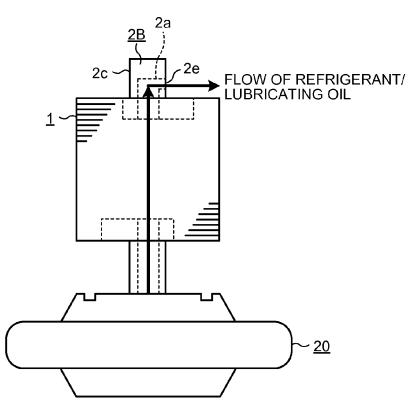


FIG.12



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HERMETIC ROTARY COMPRESSOR

CROSS REFERENCE TO RELATED APPLICATION

This application is a U.S. national stage application of International Patent Application No. PCT/JP2012/083098 filed on Dec. 20, 2012.

TECHNICAL FIELD

The present invention relates to a hermetic rotary compressor.

BACKGROUND

Hermetic rotary compressors include, as main components, a hermetic container, an electric motor provided in the hermetic container, and a compression unit arranged in the $_{20}$ hermetic container and driven by the electric motor to compress refrigerant gas. The electric motor includes a rotor firmly fixed on a crankshaft extending from a rocking scroll in the compression unit and a stator fixed to the hermetic container. Such a hermetic rotary compressor sucks the 25 refrigerant gas into the compression unit and compresses the refrigerant gas by rotating the rotor to rotate the crankshaft and thereby rotates the rocking scroll provided on the crankshaft. The compressed refrigerant gas is discharged into the hermetic container to pass through the gap between 30 the hermetic container and the stator and the gap between the rotor and the stator and is supplied through a discharge pipe to a refrigerator. Meanwhile, lubricating oil stored in the hermetic container is raised in a passageway in the crankshaft by the pressure-feeding action of an oil stirrer (twisted 35 plate) provided in the passageway during the rotation of the crankshaft and supplied as a sealing oil and a lubricating oil to sliding portions of the compression unit and the like.

A hermetic rotary compressor having such a configuration causes deformation in the crankshaft because the torque ⁴⁰ increases when the refrigerant is compressed and the torque decreases when the high pressure refrigerant is discharged. The deformation in the crankshaft results from the load that the crankshaft receives from the rocking scroll and is increased during the rotation at higher speeds and under ⁴⁵ higher loads. As a result, vibrations and noises are generated.

To mitigate such vibrations and noises, conventional hermetic rotary compressors typically include components called balance weights attached on the axial ends of the rotor. Here, the balance weights are desirably made of a ⁵⁰ material that has a high specific gravity and allows no magnetic flux from the rotor to pass therethrough (low magnetic permeability), and brass is typically used. The brass is, however, expensive and it is desirable not to use the brass to reduce costs. ⁵⁵

To dispense with the balance weights, a conventional rotor described in Patent Literature 1 has a through-opening, which is unbalanced with respect to the shaft hole as the center, in at least one axial end of the rotor. This configuration in the conventional technique described in Patent 60 trated in FIG. 1. Literature 1 allows the rotor to produce the effect of the balance weights. FIG. 2 is a side FIG. 3 is a pla FIG. 4 is a contract of the balance weights. FIG. 5 is a between a gas verified to the shaft hole as the center, in at least one axial end of the rotor. This configuration in the conventional technique described in Patent 60 trated in FIG. 1. FIG. 5 is a between a gas verified to the shaft hole as the balance weights.

Patent Literature

Patent Literature 1: Japanese Patent Application Laid-Open No. 10-152935

An unbalanced through-opening in the inner side of the rotor surface, as in the conventional technique described in Patent Literature 1, however, is less effective in cancelling the vibration (that is, the effect of cancelling the deforming ⁵ force of the crankshaft acting when the compression unit compresses the refrigerant) in comparison with the case when the balance weights are used, and thus requires larger force to cancel the vibration. As described above, the conventional technique is problematic in that it cannot ¹⁰ reduce costs and cannot produce the vibration mitigating effect at a similar level to the case with the balance weights.

SUMMARY

The present invention has been achieved in view of the above, and an object of the present invention is to provide a hermetic rotary compressor that provides the capability of reducing costs and mitigating vibration.

To solve the above described problems and achieve the object, a hermetic rotary compressor according to the present invention includes: a compression unit that compresses refrigerant gas; an electric motor that drives the compression unit; a hermetic container that accommodates the compression unit and the electric motor and contains the refrigerant; and a crankshaft that extends from the compression unit to the electric motor and is provided on a rotor in the electric motor. The rotor has two large-diameter inner circumferential portions formed at two axis end portions of the rotor, the large-diameter inner circumferential portions having inner diameters larger than an inner diameter of an axially middle portion of the rotor, the large-diameter inner circumferential portions having inner diameter centers offset with respect to a rotation axis line of the crankshaft in a radial direction, and the crankshaft has a first passageway and a second passageway, the first passageway being formed in the crankshaft and allowing the refrigerant to flow through the first passageway, the second passageway providing communication between the first passageway and at least one discharge opening that is formed in an outer circumferential surface of the crankshaft, the at least one discharge opening being formed at a position that faces an inner circumferential surface of one of the two large-diameter inner circumferential portions, the one large-diameter inner circumferential portion being on a side of the compression unit.

The present invention makes refrigerant raised from a compression unit during the rotation to jet out onto an inner circumferential surface of inner circumferential portions formed at both axially end portions of a rotor to thereby cancel a deforming force of a shaft and, thus, achieves an effect of reducing costs and mitigating vibration.

BRIEF DESCRIPTION OF DRAWINGS

FIG. **1** is a diagram of major components of a hermetic ⁵⁵ rotary compressor according to a first embodiment of the present invention.

FIG. 2 is a side view of a rotor illustrated in FIG. 1.

FIG. 3 is a plan view of the rotor illustrated in FIG. 1.

FIG. **4** is a configuration diagram of a crankshaft illustrated in FIG. **1**.

FIG. **5** is a diagram for explaining the relationship between a gas venting hole provided in the crankshaft and a large-diameter inner circumferential portion formed in the rotor.

FIG. 6 is a first diagram for explaining the operation of the hermetic rotary compressor according to the first embodiment of the present invention.

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FIG. **7** is a second diagram for explaining the operation of the hermetic rotary compressor according to the first embodiment of the present invention.

FIG. **8** is a diagram of an exemplary modification of the crankshaft according to the first embodiment of the present 5 invention.

FIG. 9 is a diagram illustrating the internal model of a typical compressor.

FIG. **10** is a diagram of a rotor configured such that the issue found with a rotor illustrated in FIG. **9** is solved.

FIG. **11** is a configuration diagram of a crankshaft included in a hermetic rotary compressor according to a second embodiment of the present invention.

FIG. **12** is a diagram for explaining the operation of the ¹⁵ hermetic rotary compressor according to the second embodiment of the present invention.

DETAILED DESCRIPTION

Exemplary embodiments of a hermetic rotary compressor according to the present invention will now be described in detail with reference to the drawings. The present invention is not limited to the embodiments.

First Embodiment

FIG. 1 is a diagram of major components of a hermetic rotary compressor according to a first embodiment of the present invention. FIG. 2 is a side view of a rotor illustrated 30 in FIG. 1. FIG. 3 is a plan view of the rotor illustrated in FIG. 1. FIG. 4 is a configuration diagram of a crankshaft illustrated in FIG. 1. FIG. 5 is a diagram for explaining the relationship between a gas venting hole provided in the crankshaft and a large-diameter inner circumferential por-35 tion formed in the rotor. FIG. 6 is a first diagram for explaining the operation of the hermetic rotary compressor according to the first embodiment of the present invention. FIG. 7 is a second diagram for explaining the operation of the hermetic rotary compressor according to the first 40 embodiment of the present invention.

In FIG. 1, a compression unit 20 and a rotor 1 are illustrated as major components of the hermetic rotary compressor. The compression unit 20 is provided in a hermetic container (not illustrated) containing lubricating oil 45 and compresses refrigerant gas. The rotor 1 is firmly fixed on a crankshaft 2 extending from the compression unit 20. The rotor 1 includes a permanent magnet and a laminated core and is arranged on the inner diameter side of an undepicted stator. The crankshaft 2 rotates together with the rotor 1, and 50 a rocking scroll 22 provided in the compression unit 20 is attached to the crankshaft 2 at its lower portion. The crankshaft 2 will be described in detail later.

With reference to FIG. 2, the rotor 1 has a small-diameter inner circumferential portion 6, an upper large-diameter 55 inner circumferential portion 5a, and a lower large-diameter inner circumferential portion 5b formed on the inner diameter side of the rotor 1. The small-diameter inner circumferential portion 6 is formed at an axially middle portion (axis middle portion 1d) of the rotor 1 and has an inner 60 diameter substantially identical with the outer diameter of the crankshaft 2. The upper large-diameter inner circumferential portion 5a is formed at an end (upper axis end portion 1b) of the rotor 1 on the opposite side to the compression unit 20. The lower large-diameter inner circumferential 65 portion 5b is formed at an end (lower axis end portion 1c) of the rotor 1 on the compression unit 20 side. 4

FIG. 3 is a view of the lower large-diameter inner circumferential portion 5b and the small-diameter inner circumferential portion 6, with the rotor 1 observed from the compression unit 20 side. In the illustrated example, the upper large-diameter inner circumferential portion 5a is omitted. In this manner, the upper large-diameter inner circumferential portion 5a and the lower large-diameter inner circumferential portion 5b have inner diameters larger than the inner diameter of the small-diameter inner circumferential portion 6, with their centers 11 offset with respect to a rotation axis line 10 in a radial direction, such that the weight balance of the rotor 1 achieves an imbalance.

With reference to FIG. 4, the crankshaft 2 has a passageway 14 for the refrigerant and the lubricating oil (hereinafter referred to as "refrigerant and the like"), extending upward from the lower end of the crankshaft 2. An oil stirrer 8 is provided in the passageway 14 at its lower portion to pressure-feed the lubricating oil, which is stored in the hermetic container at its lower portion, upward through the passageway 14. The crankshaft 2 also has an oil supply hole 2b and a gas venting hole 2a positioned above the oil supply hole 2b.

The oil supply hole 2*b* is formed above the rocking scroll 22 to provide communication between an outer circumferential surface 2*c* of the crankshaft 2 and the passageway 14, and has discharge openings 2*d*, which are on the outer circumferential surface 2*c* side, positioned inside the compression unit 20. When the crankshaft 2 rotates, the lubricating oil contained in the hermetic container is pressure-feed by the pressure-feeding action of the oil stirrer 8 upward from the lower end of the passageway 14. The lubricating oil is, then, discharged from the oil supply hole 2*b* positioned inside the compression unit 20 and other sliding portions. This maintains 35 the airtightness of each sliding portion and produces the lubricating action.

The gas venting hole 2a is formed such that it penetrates through the crankshaft 2 and communicates with the passageway 14. The gas venting hole 2a has discharge openings 2e in the outer circumferential surface 2c of the crankshaft 2. The discharge openings 2e are formed in such a manner to face an inner circumferential surface 4b of the lower large-diameter inner circumferential portion 5b of the rotor 1.

FIG. 5 is a view illustrating the relationship between the lower large-diameter inner circumferential portion 5*b* and the gas venting hole 2a, when the rotor 1 is viewed from the compression unit 20 side. As described above, the lower large-diameter inner circumferential portion 5*b* has the center 11 offset with respect to the rotation axis line 10 in the radial direction (see FIG. 3). The gas venting hole 2a has the discharge openings 2e in the outer circumferential surface 2c of the crankshaft 2 in the direction in which the lower large-diameter inner circumferential portion 5b is offset (the direction indicated by the arrow) and in the direction opposite to the arrow.

The operation of the hermetic rotary compressor according to the first embodiment will now be described with reference to FIG. **6**. FIG. **6** is a first diagram for explaining the operation of the hermetic rotary compressor according to the first embodiment of the present invention. The rotor **1** rotates to compress the refrigerant in the compression unit **20** via the crankshaft **2**. The compressed high pressure refrigerant is discharged from discharge pipes (not illustrated) provided in the upper surface of the compression unit. Meanwhile, the lubricating oil staying at a lower portion of the compression unit **20** is raised by the oil stirrer

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8 through the passageway 14 and discharged from the oil supply hole 2b. Thus, problems such as seizure due to friction of the compression unit 20 are prevented from occurring.

Meanwhile, the refrigerant and the like that passes 5 through the passageway 14 is discharged from the gas venting hole 2a. Here, when the refrigerant and the like that is pressure-fed through the passageway 14 is discharged from the discharge openings 2e of the gas venting hole 2a, a centrifugal force due to the rotation of the crankshaft 2 acts 10 on the refrigerant and the like. The discharge openings 2e of the gas venting hole 2a are formed at the positions facing the inner circumferential surface 4b of the lower large-diameter inner circumferential portion 5b of the rotor 1. Hence, the refrigerant and the like under the influence of the centrifugal 15 force collides with the inner circumferential surface 4b of the lower large-diameter inner circumferential portion 5b.

Since the rotor 1 according to the present embodiment has the inner circumferential portions (5a and 5b) formed at the axis end portions (1b and 1c) such that the weight balance 20achieves an imbalance, the deforming force of the crankshaft 2 acting when the compression unit 20 compresses the refrigerant can be cancelled. Thus, the vibrations and noises can be reduced.

In the rotor 1 according to the present embodiment, the 25 discharge openings 2e of the gas venting hole 2a are provided in the direction in which the lower large-diameter inner circumferential portion 5b is offset and in the opposite direction. Hence, as illustrated in FIG. 7, a clearance W1 between the inner circumferential surface 4b of the lower 30 large-diameter inner circumferential portion 5b and one of the discharge openings 2e is wider than a clearance W2 between the inner circumferential surface 4b of the lower large-diameter inner circumferential portion 5b and one of the other discharge openings 2e.

Because of this configuration, the refrigerant and the like discharged from the discharge opening 2e on the clearance W2 side hits the inner circumferential surface 4b of the lower large-diameter inner circumferential portion 5b before falling toward the compression unit 20, while the refrigerant 40 1 includes a through-opening, which is unbalanced with and the like discharged from the discharge opening 2e on the clearance W1 side does not hit the inner circumferential surface 4b of the lower large-diameter inner circumferential portion 5b. Thus, as the refrigerant and the like under the influence of the centrifugal force of the crankshaft 2 hits the 45 inner circumferential surface 4b of the lower large-diameter inner circumferential portion 5b, its jetting force acts as a force to decenter the crankshaft 2. As a result, a further mitigating effect on the vibrations and noises can be expected.

When the rotor 1 rotates at high speeds, the lubricating oil discharged from the discharge opening 2e at the clearance W1 side hits the inner circumferential surface 4b of the lower large-diameter inner circumferential portion 5b before falling toward the compression unit 20. If the lubricating oil 55 scatters beyond the inner circumferential surface 4b to the outer circumferential side without hitting the inner circumferential surface 4b of the lower large-diameter inner circumferential portion 5b, discharge holes 21 formed in the upper portion of the compression unit 20 may be blocked by 60 the lubricating oil. If the discharge holes 21 are blocked by the lubricating oil, the refrigerant, which is compressed to have high pressure, may be discharged from the discharge holes 21 with difficulty; thus, degradation in performance of the compressor may result. In the rotor 1 according to the 65 present embodiment, the discharge openings 2e of the gas venting hole 2a face the inner circumferential surface 4b of

the lower large-diameter inner circumferential portion 5b of the rotor 1. This provides the capability of preventing the lubricating oil discharged from the gas venting hole 2a from scattering beyond the inner circumferential surface 4b of the lower large-diameter inner circumferential portion 5b to the outer circumferential side. Hence, even in a case where the discharge holes 21 of the compression unit 20 are provided at the positions as illustrated in FIG. 7 (on the radially outer side of the inner circumferential surface 4b of the lower large-diameter inner circumferential portion 5b), there is no potential for the discharge holes 21 to be blocked by the lubricating oil.

FIG. 9 is a diagram illustrating the internal model of an ordinary compressor. In a rotor 1A configured as illustrated in FIG. 9, the inner diameters of an upper large-diameter inner circumferential portion 5a-1 and a lower large-diameter inner circumferential portion 5b-1 are not offset in the radial direction. A compressor having such a configuration experiences torque fluctuations because the torque increases when the refrigerant is compressed and the torque decreases when the high pressure refrigerant is discharged and, as a result, the vibrations and noises are generated.

FIG. 10 is a diagram of a rotor 1A-1 configured such that the problems shown by the rotor illustrated in FIG. 9 are solved. To mitigate the vibrations and noises, components called balance weights 9 are typically attached to the axial ends of the rotor 1A-1, as illustrated in FIG. 10. The balance weights 9 are formed to have unbalanced centers of gravity and attached in orientations to cancel deformation in a crankshaft caused when refrigerant is compressed. This cancels the deformation in the crankshaft caused when the refrigerant is compressed, so that the vibrations and noises can be mitigated. Here, the balance weights are desirably made of a material that has a high specific gravity and allows 35 no magnetic flux from the rotor to pass therethrough (low magnetic permeability), and brass is typically used. The brass is, however, expensive and it is desirable not to use the brass to reduce costs.

The conventional technique described in Patent Literature respect to the shaft hole as the center, in at least one axial end. This through-opening is provided in an orientation to cancel deformation in a crankshaft caused when the refrigerant is compressed. With such a configuration, a similar effect to the case with the balance weights 9 can be expected. The configuration of the conventional technique, however, is problematic in that its effect of cancelling the vibration is small and it cannot reduce costs and produce the vibration mitigating effect at a similar level to the case with the 50 balance weights.

In the hermetic rotary compressor according to the present embodiment, the upper large-diameter inner circumferential portion 5a and the lower large-diameter inner circumferential portion 5b have the inner diameters larger than the inner diameter of the small-diameter portion inner circumferential portion 6, with their centers 11 offset with respect to the rotation axis line 10 in the radial direction. Additionally, the gas venting hole 2a is formed such that it communicates with the passageway 14 in the crankshaft 2. The discharge openings 2e of the gas venting hole 2a are provided at the positions facing the inner circumferential surface 4b of the lower large-diameter inner circumferential portion 5b of the rotor 1, in the direction in which the lower large-diameter inner circumferential portion 5b is offset and in the direction opposite to the offset. Thus, as the refrigerant and the like under the influence of the centrifugal force of the crankshaft 2 hits the inner circumferential surface 4b (particularly, the

surface on the clearance W2 side illustrated in FIG. 7) of the lower large-diameter inner circumferential portion 5b, its jetting force acts as a force to decenter the crankshaft 2. As a result, the vibration mitigating effect at a similar level to the case with the balance weights 9 can be obtained without 5 the balance weights 9.

FIG. 8 is a diagram of an exemplary modification of the crankshaft according to the first embodiment of the present invention. In FIG. 8, the exemplary modification of the crankshaft according to the present embodiment is illus- 10 trated. A crankshaft 2A illustrated in FIG. 8 has a gas venting hole 2a having one discharge opening 2e. In other words, the gas venting hole 2a illustrated in FIG. 8 is formed such that it communicates with a passageway 14 but does not penetrate through the crankshaft 2A. The discharge opening $2e_{15}$ is provided at a position facing the inner circumferential surface 4b of the lower large-diameter inner circumferential portion 5b of the rotor 1 in the direction opposite to the direction in which the lower large-diameter inner circumferential portion 5b is offset. That is, the discharge opening 202e is provided at the clearance W2 side illustrated in FIG. 7. In the case of such a configuration, since the refrigerant and the like under influence of the centrifugal force of the crankshaft 2A is discharged from the one discharge opening 2e, its jetting force is increased in comparison with the case 25 with the two discharge openings 2e and the force to decenter the crankshaft 2A can be further increased.

As described above, a hermetic rotary compressor according to the present embodiment includes: a compression unit 20 that compresses refrigerant gas; an electric motor that 30 drives the compression unit 20; a hermetic container that accommodates the compression unit 20 and the electric motor and contains the refrigerant; and a crankshaft 2 that extends from the compression unit 20 to the electric motor and is provided on a rotor 1 in the electric motor. The rotor 35 1 has two large-diameter inner circumferential portions (5a and 5b) formed at its two axis end portions (1b and 1c), the large-diameter inner circumferential portions (5a and 5b) have inner diameters larger than an inner diameter of an axially middle portion (1d) of the rotor 1 and have inner 40 diameter centers 11 offset with respect to a rotation axis line 10 of the crankshaft 2 in a radial direction. The crankshaft 2 has a first passageway (14), which is formed in the crankshaft 2 and allows the refrigerant to flow therethrough, and a second passageway (2a), which provides communi- 45 cation between the first passageway and discharge openings 2e formed in an outer circumferential surface 2c of the crankshaft 2. The discharge openings 2e are formed at positions facing an inner circumferential surface 4b of one large-diameter inner circumferential portion (5b) of the two 50 large-diameter inner circumferential portions (5a and 5b), the one large-diameter inner circumferential portion (5b) is on the compression unit 20 side. This configuration enables the jetting force of the refrigerant discharged from the discharge openings 2e to act as a force to decenter the 55 crankshaft 2. As a result, the vibration mitigating effect at a similar level to the case with the balance weights 9 can be obtained without the balance weights 9; thus, costs can be reduced and the vibrations and noises can be mitigated.

Additionally, in the hermetic rotary compressor according $_{60}$ to the present embodiment, the second passageway (2*a*) is in communication with the first passageway (14) and penetrates through the crankshaft 2 in the radial direction, with the discharge openings 2*e* provided in the direction in which the one large-diameter inner circumferential portion (5*b*) is $_{65}$ offset and in the opposite direction. With such a configuration, the jetting force of the refrigerant discharged from the

discharge openings 2e can be used as a force to cancel the deforming force of the crankshaft 2 in the most effective manner.

Second Embodiment

FIG. 11 is a configuration diagram of a crankshaft included in a hermetic rotary compressor according to a second embodiment of the present invention. FIG. 12 is a diagram for explaining the operation of the hermetic rotary compressor according to the second embodiment of the present invention. The difference from the first embodiment is a crankshaft 2B included instead of the crankshaft 2 or 2A. The crankshaft 2B has a gas venting hole 2a and an oil supply hole 2b formed therein similarly as in the first embodiment, but a discharge opening 2e of the gas venting hole 2a is positioned above the upper end surface of the rotor 1. As illustrated in FIG. 12, the gas venting hole 2a does not penetrate through the crankshaft 2B and the discharge opening 2e is provided in the direction opposite to the direction in which a lower large-diameter inner circumferential portion 5b is offset.

The operation of the hermetic rotary compressor according to the second embodiment will now be described. When the refrigerant and the like flowing through the passageway 14 is discharged from the discharge opening 2e of the gas venting hole 2a, a centrifugal force due to the rotation of the crankshaft 2B acts on the refrigerant and the like. As described above, the discharge opening 2e of the gas venting hole 2a is positioned above the upper end surface of the rotor 1. Hence, the decentering force due to the jetting of the refrigerant and the like discharged from the discharge opening 2e is generated at a position relatively far away from a compression unit 20. Thus, a vibration mitigating effect of the hermetic rotary compressor according to the second embodiment can be expected to be larger than that of the first embodiment.

If the discharge opening 2e of the gas venting hole 2a is formed at a position facing the inner circumferential surface of an upper large-diameter inner circumferential portion 5a, the lubricating oil would be accumulated in an inner circumferential portion of the rotor 1. Thus, the discharge opening 2e of the gas venting hole 2a according to the present embodiment is positioned above the upper end surface of the rotor 1. Additionally, an end plate may be provided on the rotor 1 such that it covers the opening of the upper large-diameter inner circumferential portion 5a to prevent the collecting of the lubricating oil discharged from the gas venting hole 2a in the upper large-diameter inner circumferential portion 5a.

The hermetic rotary compressor according to the embodiments of the present invention is presented as examples of the present invention; it is possible to combine the hermetic rotary compressor with yet another publicly known technique, and it is of course also possible to configure the hermetic rotary compressor with a modification, such as a partial omission, without departing from the spirit of the present invention.

INDUSTRIAL APPLICABILITY

As described above, the present invention can be applied to hermetic rotary compressors and is particularly useful in reducing costs and mitigating vibration. The invention claimed is:

1. A hermetic rotary compressor, comprising:

- an electric motor that drives a compression unit configured to compress refrigerant gas;
- a hermetic container that accommodates the compression ⁵ unit and the electric motor and contains the refrigerant gas; and
- a crankshaft that extends from the compression unit to the electric motor and is provided on a rotor in the electric motor, wherein¹⁰
- the rotor has two large-diameter inner circumferential portions formed at two axis end portions of the rotor, the large-diameter inner circumferential portions include an upper large-diameter inner circumferential portion and a lower large-diameter inner circumferential portion having inner diameters larger than an inner diameter of an axially middle portion of the rotor, the large-diameter inner circumferential portions have inner diameter centers offset with respect to a rotation axis line of the crankshaft in a radial direction, 20
- the crankshaft has a first passageway and a second passageway, the first passageway being formed in the crankshaft and allowing the refrigerant gas to flow through the first passageway, the second passageway providing communication between the first passageway ²⁵ and at least one discharge opening that is formed in an outer circumferential surface of the crankshaft,
- the at least one discharge opening jets out the refrigerant gas onto an inner circumferential surface of one of the two large-diameter inner circumferential portions and ³⁰ is formed at a position that faces the inner circumferential surface of the one of the two large-diameter inner circumferential portions,
- the one of the two large-diameter inner circumferential portions is the lower large-diameter inner circumferen-³ tial portion provided on a side of the compression unit,
- the second passageway is in communication with the first passageway and penetrates through the crankshaft in the radial direction, and
- the at least one discharge opening comprises two open-⁴⁰ ings that are provided in a direction in which the one large-diameter inner circumferential portion is offset and in a direction opposite to the direction in which the one large-diameter inner circumferential portion is offset.⁴⁵
- 2. A hermetic rotary compressor, comprising:
- an electric motor that drives a compression unit configured to compress refrigerant gas;
- a hermetic container that accommodates the compression unit and the electric motor and contains the refrigerant ⁵⁰ gas; and
- a crankshaft that extends from the compression unit to the electric motor and is provided on a rotor in the electric motor, wherein
- the rotor has two large-diameter inner circumferential ⁵⁵ portions formed at two axis end portions of the rotor, the large-diameter inner circumferential portions include an upper large-diameter inner circumferential portion and a lower large-diameter inner circumferential portion having inner diameters larger than an inner

diameter of an axially middle portion of the rotor, the large-diameter inner circumferential portions have inner diameter centers offset with respect to a rotation axis line of the crankshaft in a radial direction,

- the crankshaft has a first passageway and a second passageway, the first passageway being formed in the crankshaft and allowing the refrigerant gas to flow through the first passageway, the second passageway providing communication between the first passageway and at least one discharge opening that is formed in an outer circumferential surface of the crankshaft,
- the at least one discharge opening jets out the refrigerant gas onto an inner circumferential surface of one of the two large-diameter inner circumferential portions and is formed at a position that faces the inner circumferential surface of the one of the two large-diameter inner circumferential portions,
- the one of the two large-diameter inner circumferential portions is the lower large-diameter inner circumferential portion provided on a side of the compression unit, and
- the at least one discharge opening comprises one opening that is provided in a direction opposite to a direction in which the one large-diameter inner circumferential portion is offset.

3. A hermetic rotary compressor, comprising:

- an electric motor that drives a compression unit configured to compress refrigerant gas;
- a hermetic container that accommodates the compression unit and the electric motor and contains the refrigerant gas; and
- a crankshaft that extends from the compression unit to the electric motor and is provided on a rotor in the electric motor, wherein
- the rotor has two large-diameter inner circumferential portions formed at two axis end portions of the rotor, the large-diameter inner circumferential portions include an upper large-diameter inner circumferential portion and a lower large-diameter inner circumferential portion having inner diameters larger than an inner diameter of an axially middle portion of the rotor, the large-diameter inner circumferential portions have inner diameter centers offset with respect to a rotation axis line of the crankshaft in a radial direction,
- the crankshaft has a first passageway and a second passageway, the first passageway being formed in the crankshaft and allowing the refrigerant gas to flow through the first passageway, the second passageway providing communication between the first passageway and at least one discharge opening that is formed in an outer circumferential surface of the crankshaft,
- the at least one discharge opening is formed above an upper end surface of the rotor on an opposite side of the rotor from the compression unit, and
- the at least one discharge opening is provided in a direction opposite to a direction in which one of the large-diameter inner circumferential portions as the lower large-diameter inner circumferential portion provided on a side of the compression unit is offset.

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