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# Chee et al.

# (54) RADIO FREQUENCY FRONT END SYSTEM WITH AN INTEGRATED TRANSMIT/RECEIVE SWITCH

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H04B 1/48	(2006.01)
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# (57) **ABSTRACT**

A Radio Frequency (RF) front end system and method are disclosed. The RF front end system comprises an antenna, a matching network coupled to the antenna, a power amplifier (PA) coupled to the matching network via a port on a transmit path, a low noise amplifier (LNA) coupled to the matching network via the port on a receive path and at least one transmit/receive switch (T/R SW) coupled between the port and at least one of the PA and LNA.

#### 18 Claims, 9 Drawing Sheets



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Figure 1 Prior Art



Figure 2 Prior Art







Figure 4



Figure 5



Figure 6



Figure 7



Figure 8



Figure 9

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# **RADIO FREQUENCY FRONT END SYSTEM** WITH AN INTEGRATED **TRANSMIT/RECEIVE SWITCH**

### CROSS-REFERENCE TO RELATED APPLICATION

Under 35 U.S.C. §120 the present application is a continuation of U.S. Pat. Ser. No. 13/204,544, filed Aug. 5, 2011, entitled "RADIO FREQUENCY FRONT END SYS-TEM WITH AN INTEGRATED TRANSMIT/RECEIVE SWITCH" which is incorporated herein by reference.

## FIELD OF THE INVENTION

The present invention relates to a Radio Frequency (RF) front end system, and more particularly, to a RF front end system utilized in a transceiver system.

#### BACKGROUND

Some conventional transceivers do not isolate transmitters from receivers to allow for independent optimization of the transmitters and receivers. Other conventional transceiv- 25 ers integrate Radio Frequency (RF) front end components off-chip to isolate transmitters from receivers which increases the cost and size of the RF front end systems. Accordingly, what is desired is to provide a system and method that overcomes the above issues. The present inven-30 tion addresses such a need.

# SUMMARY OF THE INVENTION

A Radio Frequency (RF) front end system and method are 35 disclosed. The RF front end system comprises an antenna, a matching network coupled to the antenna, a power amplifier (PA) coupled to the matching network via a port on a transmit path, a low noise amplifier (LNA) coupled to the matching network via the port on a receive path and at least 40 one transmit/receive switch (T/R SW) coupled between the port and at least one of the PA and LNA.

# BRIEF DESCRIPTION OF THE DRAWINGS

The accompanying drawings illustrate several embodiments of the invention and, together with the description, serve to explain the principles of the invention. One of ordinary skill in the art will recognize that the particular embodiments illustrated in the drawings are merely exem- 50 plary, and are not intended to limit the scope of the present invention.

FIG. 1 illustrates a conventional time division duplexing (TDD) transceiver front end system.

FIG. 2 illustrates an existing transmit/receive switch (T/R 55 SW) implementation.

FIG. 3 illustrates another existing T/R SW implementation.

FIG. 4 illustrates a proposed T/R SW implementation in accordance with an embodiment.

FIG. 5 illustrates a proposed T/R SW implementation with a TX SW integrated with an output stage of the PA in accordance with an embodiment.

FIG. 6 illustrates an output stage of the PA in accordance with an embodiment.

FIG. 7 illustrates a common-gate LNA in accordance with an embodiment.

FIG. 8 illustrates a cross-coupled common-gate LNA in accordance with an embodiment.

FIG. 9 illustrates an integrated T/R SW in accordance with an embodiment.

# DETAILED DESCRIPTION OF PREFERRED **EMBODIMENTS**

The present invention relates to a Radio Frequency (RF) front end system, and more particularly, to a RF front end system utilized in a transceiver system. The following description is presented to enable one of ordinary skill in the art to make and use the invention and is provided in the context of a patent application and its requirements. Various modifications to the preferred embodiment and the generic principles and features described herein will be readily apparent to those skilled in the art. Thus, the present invention is not intended to be limited to the embodiments  $_{20}$  shown but is to be accorded the widest scope consistent with the principles and features described herein.

A Radio Frequency (RF) front end system and method are disclosed. The RF front end system comprises an antenna, a matching network coupled to the antenna, a power amplifier (PA) coupled to the matching network via a port on a transmit path, a low noise amplifier (LNA) coupled to the matching network via the port on a receive path and at least one transmit/receive switch (T/R SW) coupled between the port and at least one of the PA and LNA. In so doing, a more robust integrated T/R SW solution is achieved and the cost, size and package pin count of the RF front end is further reduced. To describe the features of the present invention in more detail, refer now to the following description in conjunction with the accompanying Figures.

In a conventional time division duplexing (TDD) transceiver front end system, a T/R SW is used to share the antenna between a transmitter and receiver. FIG. 1 illustrates a conventional TDD transceiver front end system 100 that includes an antenna 102, a T/R SW 104, a transmitter (TX) 106, and a receiver (RX) 108. However, in this conventional TDD transceiver front end system 100, the transmitter 106 and the receiver 108 may not be optimized with the antenna impedance.

To address this problem, FIG. 2 illustrates an existing transceiver front end system 200 that includes an antenna 202, a T/R SW 204, a PA matching network 206, a LNA matching network 208, a power amplifier (PA) 210 and a low noise amplifier (LNA) 212 that are all integrated as off-chip components. During receive, the transmit switch (TX SW) 214 is open and the receive switch (RX SW) 216 is closed which connects the antenna 202 to the receive path (RX path) 220 and isolates the transmit path (TX path) 218 from the RX path 220. During transmit, the TX SW 214 is closed and the RX SW 216 is open which connects the antenna 202 to the TX path 218 and isolates the RX 220 path from the TX path 218.

Thus, in this transceiver front end system 200, the T/R SW 204 allows the antenna 202 to be shared between the TX path 218 and RX path 220 while providing isolation between 60 them. With the TX path 218 isolated from the RX path 220, the PA matching network 206 and the LNA matching network 208 can each be optimized independently for the PA 210 and the LNA 212 respectively. However, in this transceiver front end system 200, the RF front end components, including the T/R SW 204, PA 210 and LNA 212, are integrated off-chip which increases the cost and size of the RF front end.

To address this problem and reduce the cost and size of the RF front end, FIG. 3 illustrates another existing transceiver front end system 300 that includes an antenna 302, a T/R SW **304**, a PA matching network **306**, a LNA matching network 308, a PA 310, a LNA 312, a TX path 314 and a RX path 316. In this transceiver front end system 300, the RF front end components, including the T/R SW 304, PA 310 and LNA 312, are integrated on-chip. In this transceiver front end system 300, the PA 310 and the LNA 312 have their own matching networks **306** and **308** that interact with 10 each other. The PA 310 and its matching network 306 loads the RX path 316 during receive and the LNA 312 and its matching network 308 loads the TX path 314 during transmit. However, in this transceiver front end system 300, it is difficult to achieve a robust matching network that is opti-15 mized for both the PA 310 and the LNA 312 without significant performance degradation.

The present invention addresses these drawbacks. FIG. 4 illustrates a transceiver front end system 400 that includes a PA 402, LNA 404 and T/R SW 406 integrated on-chip and 20 an antenna 408 and matching network 410 integrated offchip. In the transceiver front end system 400, the PA 402 and LNA 404 are combined together at a port 412 and share the same matching network 410. In order to share the same matching network 410 and package pin, the PA 402 and 25 LNA 404 are designed with similar optimal impedance. In another embodiment, the port 412 is a single RF port. In the transceiver front end system 400, the T/R SW 406 isolates the TX path 414 from the RX path 416 to minimize the loading on each other. 30

It is understood that the transceiver front end system 400 may result in switch loss in the TX path 414. FIG. 5 illustrates another transceiver front end system 500 that includes a PA 502, LNA 504 and T/R SW 506 integrated on-chip and an antenna 508 and matching networking 510 35 integrated off-chip. In the transceiver front end system 500, the PA 502 and LNA 504 are combined together at a port 512 and share the same matching network 510. In order to share the same matching network 510 and package pin, the PA 502 and LNA 504 are designed with similar optimal impedance. 40 In another embodiment, the port 512 is a single RF port. In the transceiver front end system 500, the switch loss in the TX path 514 is eliminated by integrating the TX SW with the output stage of the PA 502.

FIG. 6 illustrates one implementation of such output stage 45 of the PA 600. The output stage of the PA 600 includes an integrated circuit (IC) power supply pin Vdd 602, input devices Mpa1 604 and Mpa2 606, voltages Vpa\_n 608 and Vpa\_p 610 corresponding to the input devices Mpa1 604 and Mpa2 606, cascode devices Mpa3 612 and Mpa4 614, 50 voltages Vcas\_pa 616 and Vcas\_pa 618 corresponding to the cascode devices Mpa3 612 and Mpa4 614, and differential output signals Voutp\_pa 620 and Voutn\_pa 622.

In the output stage of the PA 600, the IC power supply pin Vdd 602 is differentially coupled to the input devices Mpa1 55 604 and Mpa2 606 and to the cascode devices Mpa3 612 and Mpa4 614. In the output stage of the PA 600, input device Mpa1 604 is in series with cascode device Mpa3 612 and input device Mpa2 606 is in series with cascode device Mpa4 614. Furthermore, input device Mpal 604 and cascade 60 device Mpa3 612 provide differential output signal Voutn\_pa 622 and input device Mpa2 606 and cascade device Mpa4 614 provide differential output signal Voutpa 620.

The input devices Mpa1 604 and Mpa2 606 can be made of a variety of materials including but not limited to thin 65 oxide devices to provide a large transconductance. The cascode devices Mpa3 612 and Mpa4 614 can also be made 4

of a variety of materials including but not limited to thick oxide devices to provide isolation between the input and output and prevent devices breakdown due to the large output swing. The cascode devices Mpa3 612 and Mpa4 614 also function as the TX SW to isolate the TX path from the RX path when Vcas\_pa is pulled low. The output stage of the PA 600 illustrates a differential version of the PA. In another embodiment, the output stage of the PA 600 can be applied to a single-ended version of the PA.

As previously mentioned, the PA and LNA in FIGS. 4 and 5 are designed with similar optimal impedance to allow the PA and LNA to share the same matching network. However, a common source inductive degenerated LNA typically has a much higher optimal impedance than the optimal impedance of a PA. Thus, in one embodiment, the present invention utilizes a common-gate LNA because the common-gate LNA has a similar optimal impedance as the PA.

FIG. 7 illustrates a common-gate LNA 700 that includes an IC power supply pin Vdd 702, input devices Mlna1 704 and Mlna2 706, voltages Vg 708 and Vg 710 corresponding to the input devices Mal 704 and Mlna2 706, cascode devices Mlna3 712 and Mlna4 714, voltages Vcas 716 and Vcas 718 corresponding to the cascode devices Mlna3 712 and Mina 714, input signals Vlna\_n 720 and Vlna\_p 722, and differential output signals Voutp\_lna 724 and Voutn\_lna 726.

In the common-gate LNA 700, the IC power supply pin Vdd 702 is differentially coupled to the input devices Mlna1 704 and Mlna2 706 and to the cascode devices Mlna3 712 and Mlan4 714. In the common-gate LNA 700, input device Mlna1 704 is in series with cascode device Mlna3 712 and input device Mlna2 706 is in series with cascode device Mlna4 714. Furthermore, input device Mlna1 704 and cascade device Mlna3 712 provide differential output signal Voutn\_lna 726 and input device Mlna2 706 and cascade device Mlna4 714 provide differential output signal Voutp\_lna 724.

In the common-gate LNA 700, the input impedance is inversely proportional to the transconductance of the input devices Mlna1 704 and Mlna2 706. The transconductance of the input devices Mlna1 704 and Mlna2 706 can be set to a variety of settings including but not limited to a common RF port impedance. Additionally, the cascode devices Mlna3 712 and Mlna4 714 are used to isolate the input from the output. The common-gate LNA 700 illustrates a differential version of the LNA. In another embodiment, the common-gate LNA 700 can be applied to a single-ended version of the LNA.

One of ordinary skill in the art readily recognizes that other implementations of a LNA that includes a similar optimal impedance to a PA may be utilized and that would be within the spirit and scope of the present invention. FIG. 8 illustrates another implementation of the LNA as a crosscoupled common-gate LNA 800 that includes an IC power supply pin Vdd 802, input devices Mlna1 804 and Mlna2 806, voltages Vg 808 and Vg 810 corresponding to the input devices Mlna1 804 and Mlna2 806, cascode devices Mlna3 812 and Mlna4 814, voltages Vcas 816 and Vcas 818 corresponding to the cascode devices Mlna3 812 and Mina 814, input signals Vlna\_n 820 and Vlna\_p 822, and differential output signals Voutn\_lna 824 and Voutp\_lna 826.

In the cross-coupled gate LNA **800**, the IC power supply pin Vdd **802** is differentially coupled to the input devices Mlna**1 804** and Mlna**2 806** and to the cascode devices Mlna**3 812** and Mlan**4 814**. In the cross-coupled gate LNA **800**, input device Mlna**1 804** is in series with cascode device Mlna**3 812** and input device Mlna**2 806** is in series with cascode device Mlna4 814. Furthermore, input device Mlna1 804 and cascode device Mlna3 812 provide differential output signal Voutn\_lna 824 and input device Mlna2 806 and cascode device Mlna4 814 provide differential output signal Voutp\_lna 826.

In the cross-coupled common-gate LNA 800, the input signal Vlna\_p 822 is fed to the gate of Mlna1 804 and the source of Mlna2 806 and the input signal Vlna\_n 820 is fed to the gate of Mlna2 806 and the source of Mlna1 804. The cross-coupled common-gate LNA 800 illustrates a differen- 10 tial version of the LNA. In another embodiment, the crosscoupled common-gate LNA 800 can be applied to a singleended version of the LNA.

In another embodiment, a common source LNA with feedback implementation is utilized. The feedback reduces 15 the optimal input impedance of a common source LNA to a level that is similar to the optimal impedance of the PA.

One of ordinary skill in the art readily recognizes that the present invention may utilize various implementations of an integrated transmit/receive switch (T/R SW) and that would 20 be within the spirit and scope of the present invention. FIG. 9 illustrates an integrated transmit/receive switch (T/R SW) 900 that includes series transistors Msw1 902 and Msw2 904, shunt transistors Msw3 906, Msw4 908 and Msw5 910, input signals Vinp 912 and Vinn 914 and output signals 25 Voutp 916 and Voutn 918. Shunt transistor Msw3 906 shunts the differential mode signal whereas shunt transistors Msw4 908 and Msw5 910 shunt both the common mode and differential mode signals.

When integrated T/R SW 900 is on, shunt transistors 30 Msw3-5 906-910 are off and series transistors Msw1-2 902-904 are on to allow the input signals Vinp 912 and Vinn 914 to pass through the integrated T/R SW 900 to the output with minimal loss. When integrated T/R SW 900 is off, shunt transistors Msw 1-2 902-904 are off and shunt transistors 35 Msw 3-5 906-910 are all on. The high series impedance and low shunt impedance attenuate the large signal of the PA and isolate the input of the LNA from the output of the PA. The integrated T/R SW 900 illustrates a differential version of the T/R SW. In another embodiment, a single-ended version 40 of the T/R SW can be implemented.

One of ordinary skill in the art readily recognizes that the integrated T/R SW 900 can be implemented in a variety of other ways including but not limited to omitting the shunt transistor Msw3 906, omitting the shunt transistors Msw4 45 908 and Msw5 910, using a field-effect transistor (FET) or using a transmission gate and that would be within the spirit and scope of the present invention.

As above described, by isolating the TX path from the RX path, integrating the RF front end components on-chip and 50 is a cross-coupled common-gate LNA. creating a matching network that is optimized for both the PA and the LNA, the present invention achieves a more robust integrated T/R SW solution. Thus, the cost, size and package pin count of the RF front end system is reduced by the present invention.

Although the present invention has been described in accordance with the embodiments shown, one of ordinary skill in the art will readily recognize that there could be variations to the embodiments and those variations would be within the spirit and scope of the present invention. Accord- 60 ingly, many modifications may be made by one of ordinary skill in the art without departing from the spirit and scope of the appended claims.

What is claimed is:

1. A Radio Frequency (RF) front end system comprising: 65 end, the method comprising: a power amplifier (PA) configured to couple to a matching network via a port on a transmit (TX) path;

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- a low noise amplifier (LNA) configured to couple to the matching network via the port on a receive (RX) path, wherein the PA and the LNA are combined together at the port: and
- a transmit/receive switch (T/R SW) coupled in series between the port and the LNA, and a non-switchable direct connection formed between the PA and the port: and
- wherein an output stage of the PA is configured to perform switching functionality.
- 2. The RF front end system of claim 1, wherein the port is a single RF port.

3. The RF front end system of claim 1, wherein the output stage of the PA includes a power supply pin Vdd differentially coupled to first and second input devices and to first and second cascade devices, wherein the first input device is in series with the first cascade device and the second input device is in series with the second cascade device, wherein the first input device and first cascade device provide a first differential output signal and the second input device and second cascade device provide a second differential output signal.

4. The RF front end system of claim 3, wherein the first and second input devices are thin oxide devices and the first and second cascade devices are thick oxide devices.

5. The RF front end system of claim 1, wherein the output stage of the PA is single-ended.

6. The RF front end system of claim 1, wherein the LNA is a common-gate LNA.

7. The RF front end system of claim 6, wherein the common-gate LNA includes a power supply pin Vdd differentially coupled to first and second input devices and first and second cascade devices, wherein the first input device is in series with the first cascade device and the second input device is in series with the second cascade device, wherein the first input device and first cascade device provide a first differential output signal and the second input device and second cascade device provide a second differential output signal.

8. The RF front end system of claim 7, wherein an input impedance of the common-gate LNA is inversely proportional to a transconductance of the first and second input devices.

9. The RF front end system of claim 8, wherein the input impedance is a common RF port impedance.

10. The RF front end system of claim 6, wherein the common-gate LNA is single-ended.

11. The RF front end system of claim 1, wherein the LNA

12. The RF front end system of claim 1, wherein the LNA is a common source LNA with feedback implementation.

13. The RF front end system of claim 1, wherein the at least one T/R SW includes first and second series transistors, 55 first, second and third shunt transistors, first and second input signals, and first and second output signals.

14. The RF front end system of claim 1, wherein the at least one T/R SW is single-ended.

15. The RF front end system of claim 1, wherein the at least one T/R SW is implemented using a field-effect transistor (FET) or a transmission gate.

16. The RF front end system of claim 1, wherein the at least one T/R SW is a plurality of transmit-receive switches.

17. A method for creating a Radio Frequency (RF) front

coupling a power amplifier (PA) to a matching network via a port on a transmit (TX) path;

coupling a low noise amplifier (LNA) to the matching network via the port on a receive (RX) path, wherein the PA and the LNA are combined together at the port; coupling a transmit/receive switch (T/R SW) in series

between the port and the LNA, and providing a nonswitchable direct connection between the PA and the port; and

combining the PA and the LNA together at the port, wherein an output stage of the PA is configured to 10 perform switching functionality.

18. The method of claim 17, further comprising integrating an antenna and the matching network off-chip.

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