



US009646242B2

(12) **United States Patent**
Hofer et al.

(10) **Patent No.:** **US 9,646,242 B2**
(45) **Date of Patent:** **May 9, 2017**

(54) **BOOSTER ANTENNA, CONTACTLESS CHIP ARRANGEMENT, ANTENNA STRUCTURE AND CHIP ARRANGEMENT**

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(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.

(21) Appl. No.: **14/192,895**

(22) Filed: **Feb. 28, 2014**

(65) **Prior Publication Data**

US 2014/0246503 A1 Sep. 4, 2014

(30) **Foreign Application Priority Data**

Mar. 1, 2013 (DE) 10 2013 102 051

(51) **Int. Cl.**

- G06K 19/077** (2006.01)
- H01Q 7/00** (2006.01)
- H01Q 1/22** (2006.01)
- H01Q 1/38** (2006.01)
- H01Q 9/20** (2006.01)
- H01Q 9/42** (2006.01)
- H01Q 21/30** (2006.01)

(52) **U.S. Cl.**

CPC . **G06K 19/07794** (2013.01); **G06K 19/07767** (2013.01); **H01Q 1/2225** (2013.01); **H01Q 1/38** (2013.01); **H01Q 7/00** (2013.01); **H01Q 9/20** (2013.01); **H01Q 9/42** (2013.01); **H01Q 21/30** (2013.01)

(58) **Field of Classification Search**

CPC G06K 19/07767; G06K 19/07794
USPC 235/492
See application file for complete search history.

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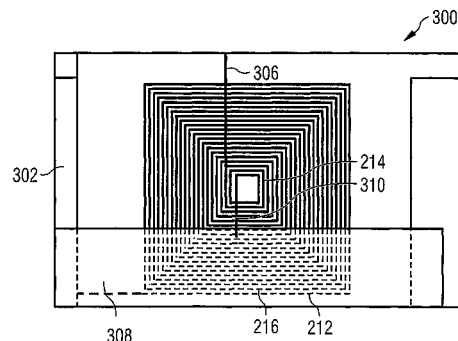
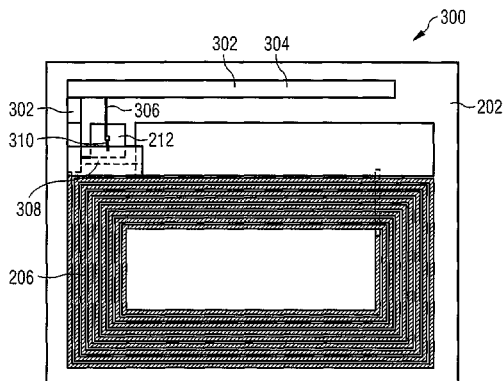
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(57) **ABSTRACT**

In various embodiments, a booster antenna for a chip arrangement is provided. The booster antenna includes: a first circuit, which forms a first resonant circuit; a second circuit, which forms a second resonant circuit, wherein the first circuit is electrically conductively connected to the second circuit; and a third circuit, which forms a third resonant circuit, wherein the third circuit is electrically conductively connected to the second circuit.

19 Claims, 10 Drawing Sheets



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FIG 1

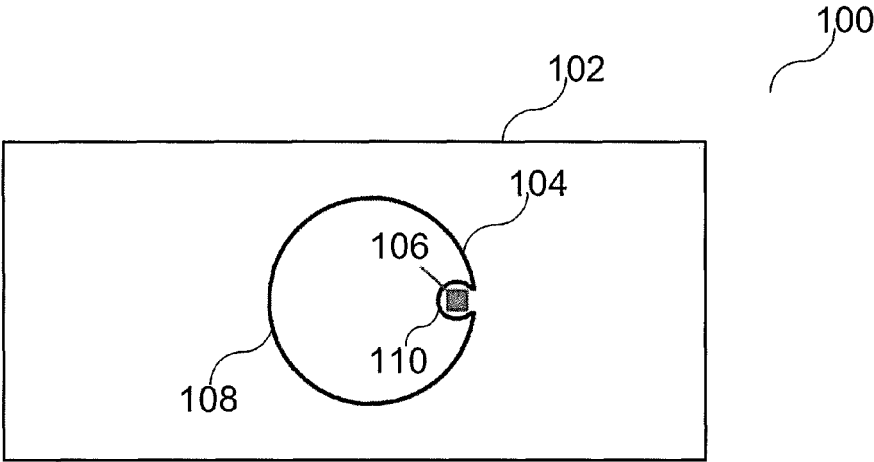


FIG 2

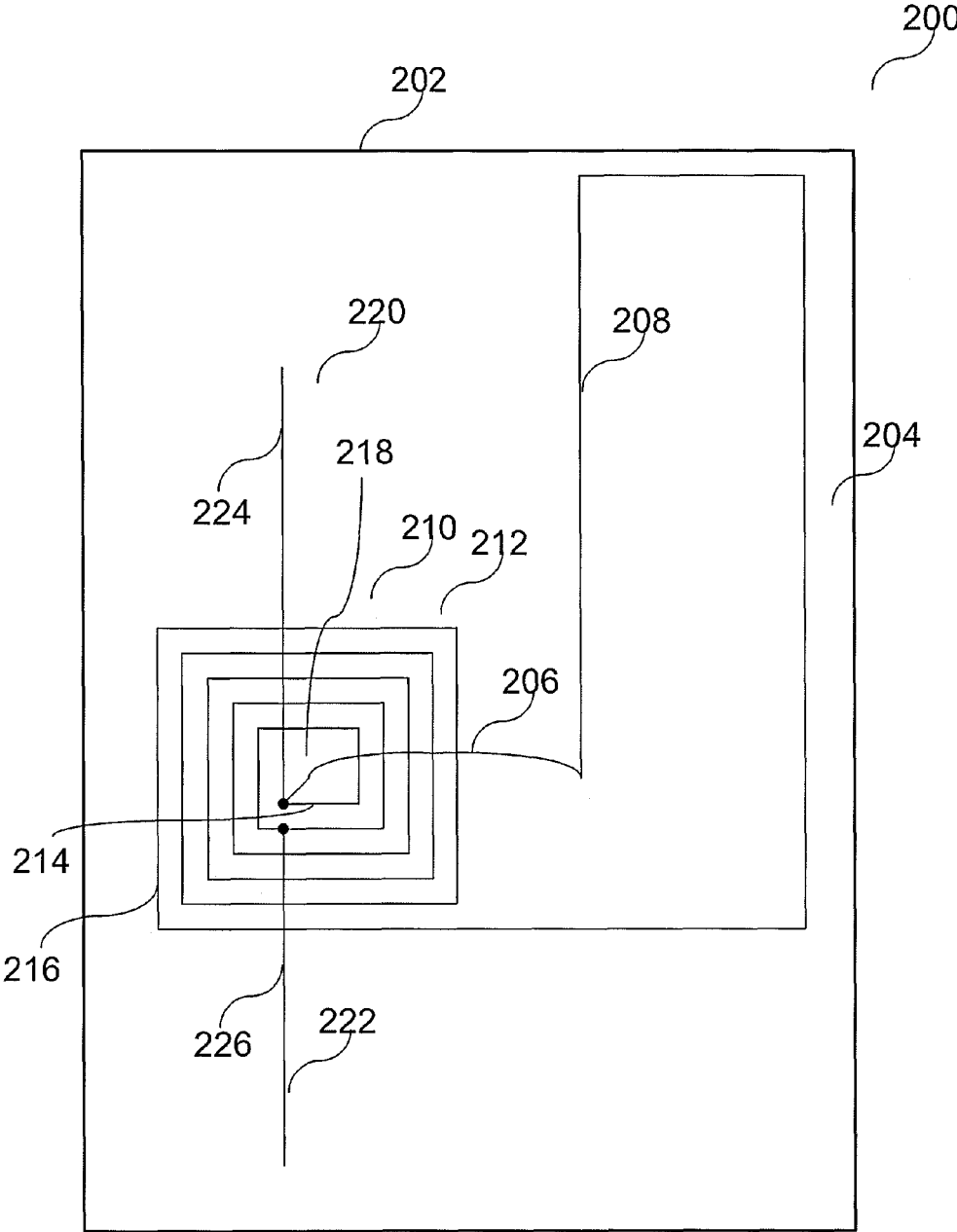


FIG 3

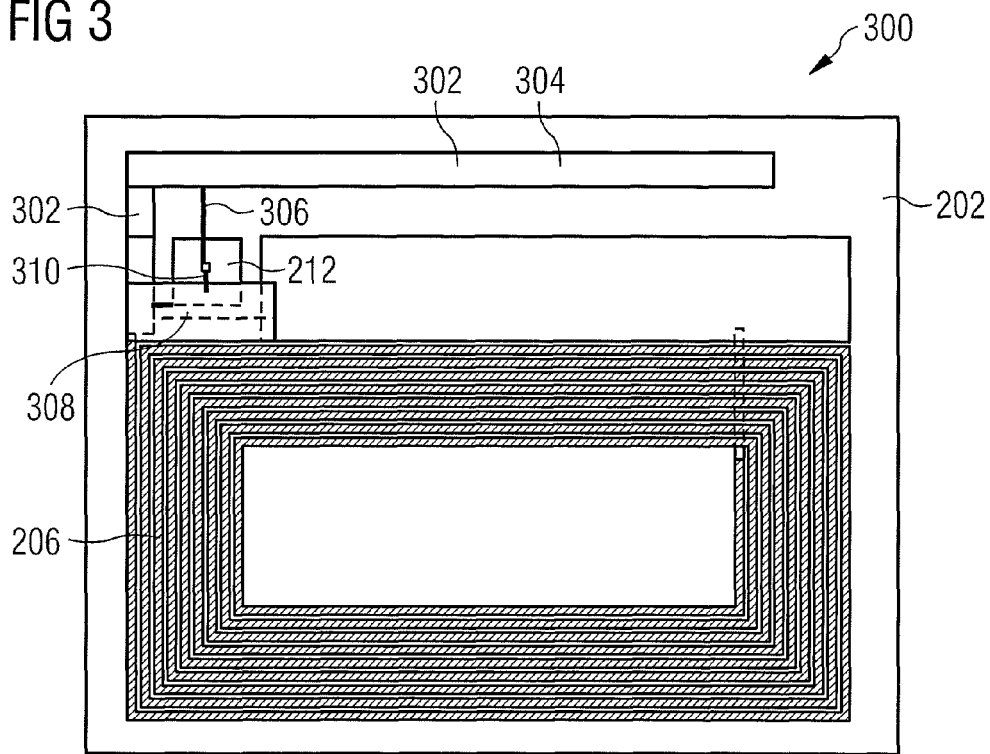


FIG 4

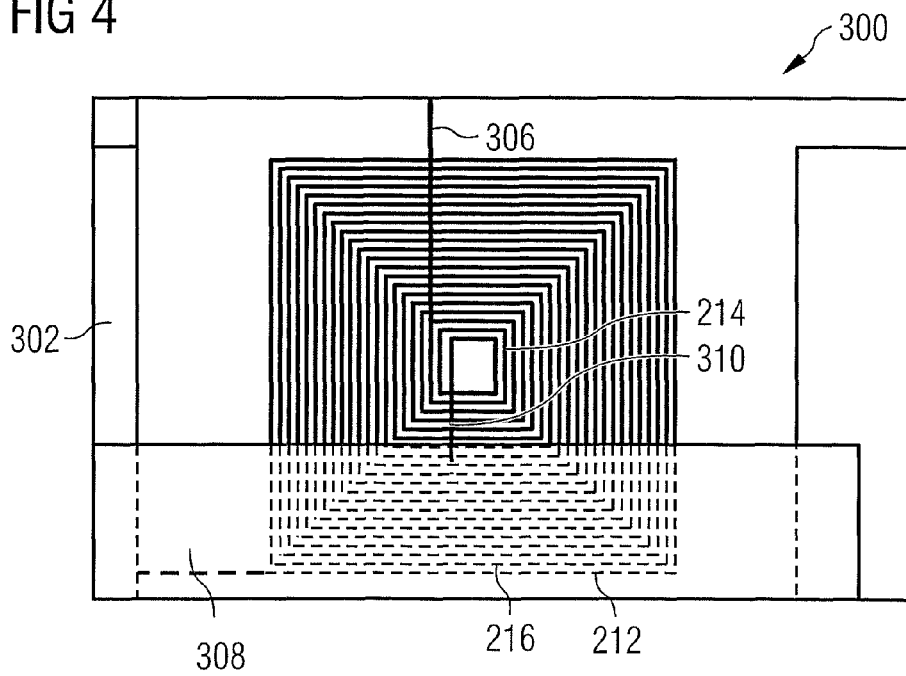


FIG 5

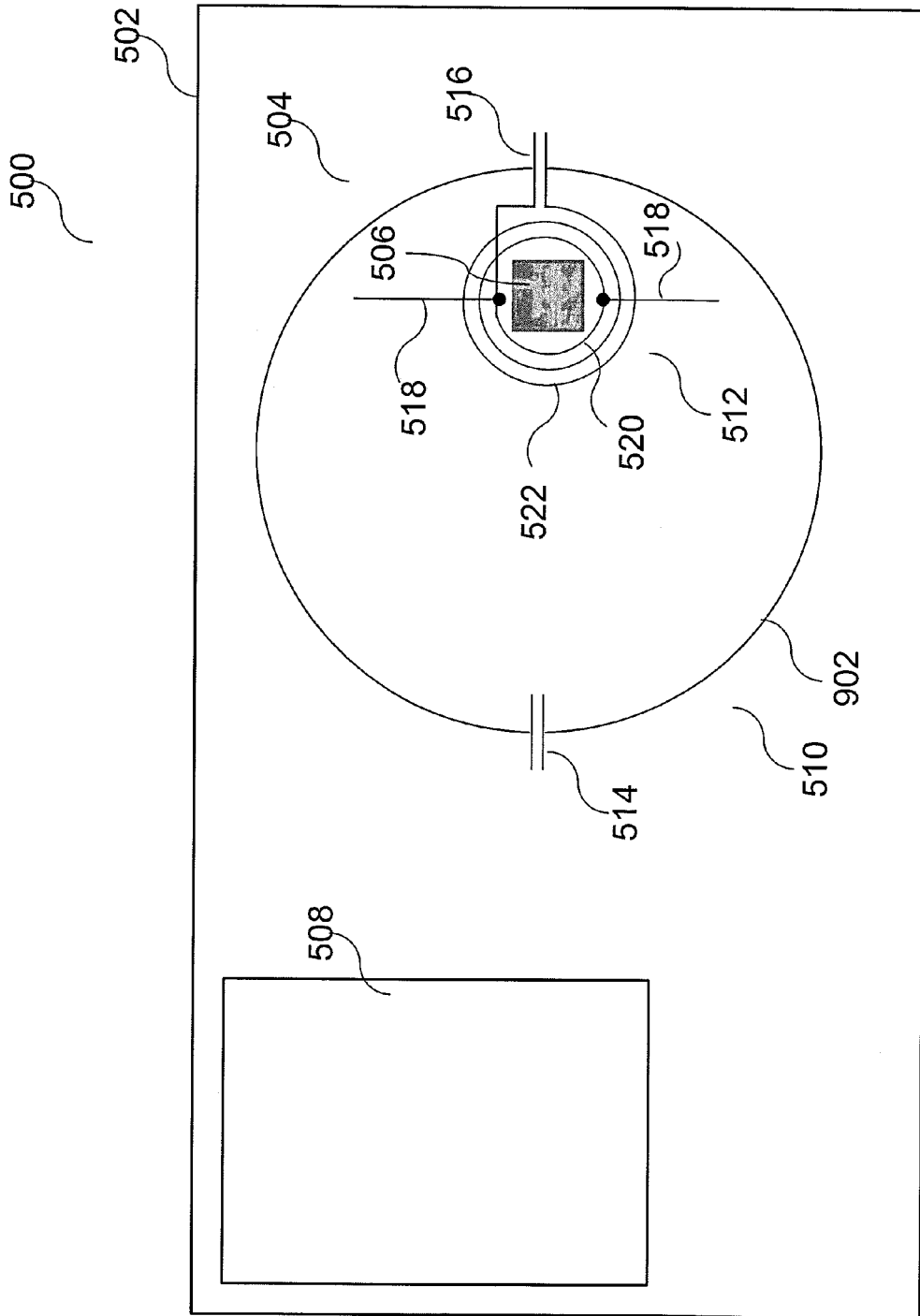


FIG 6

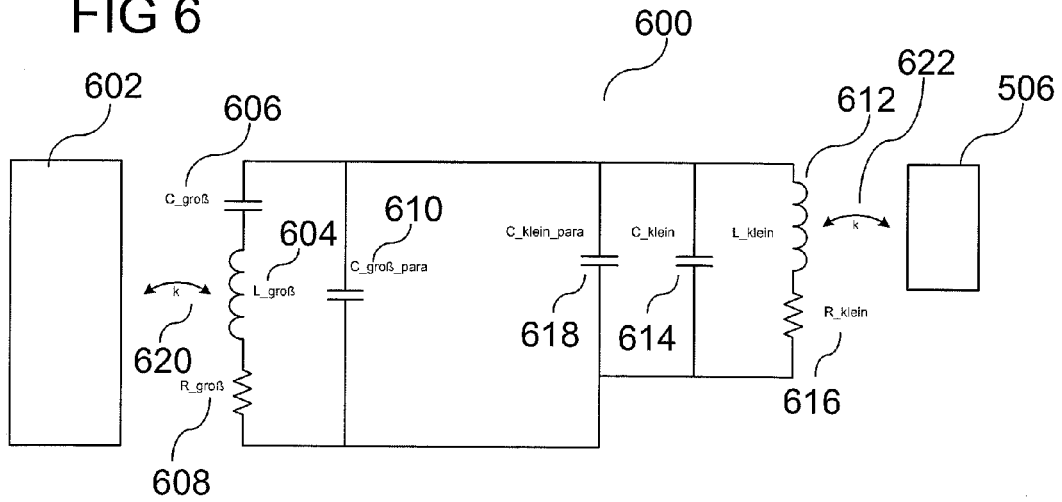


FIG 7

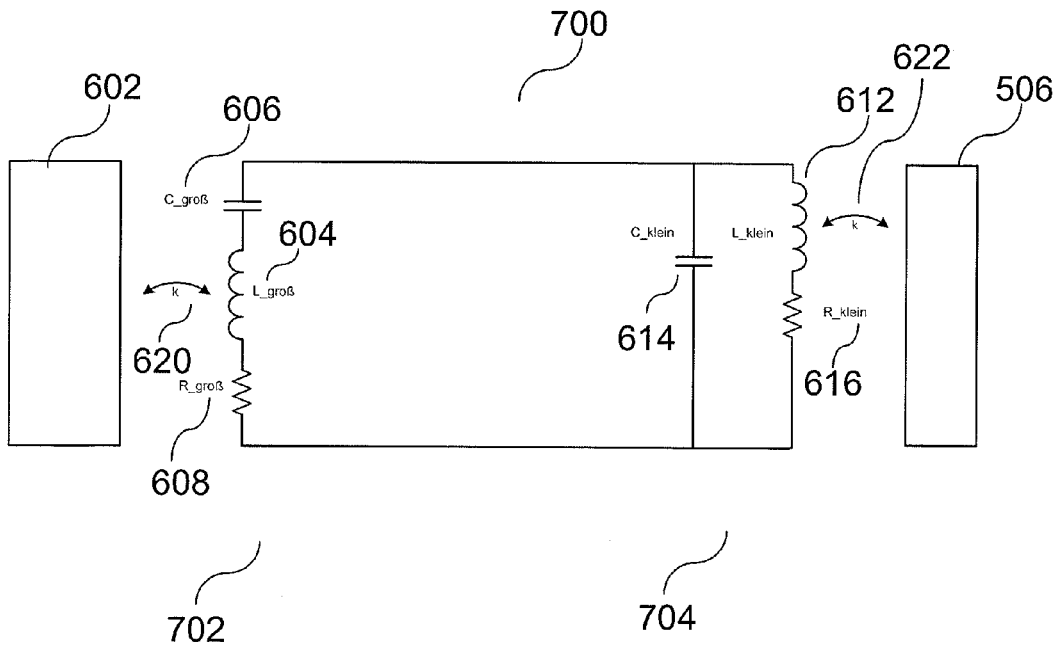


FIG 8A

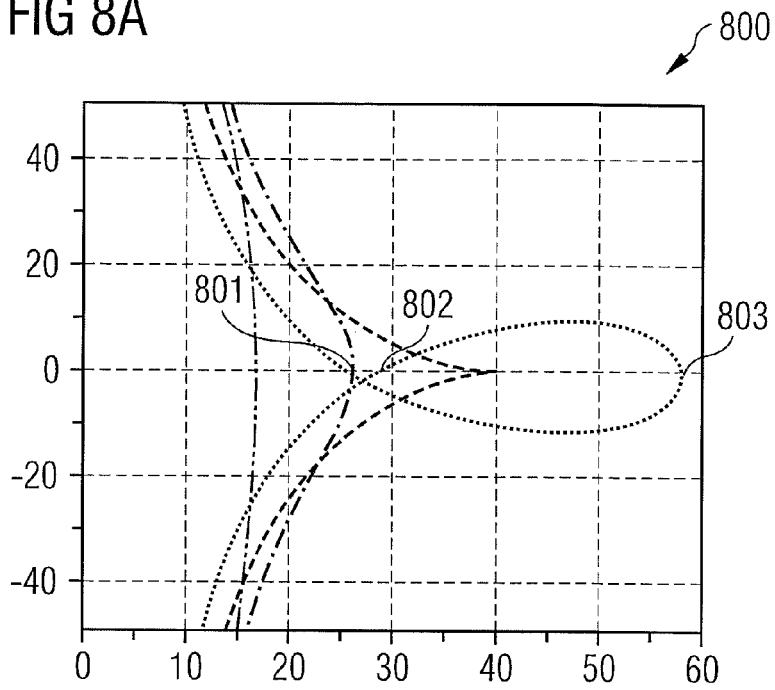


FIG 8B

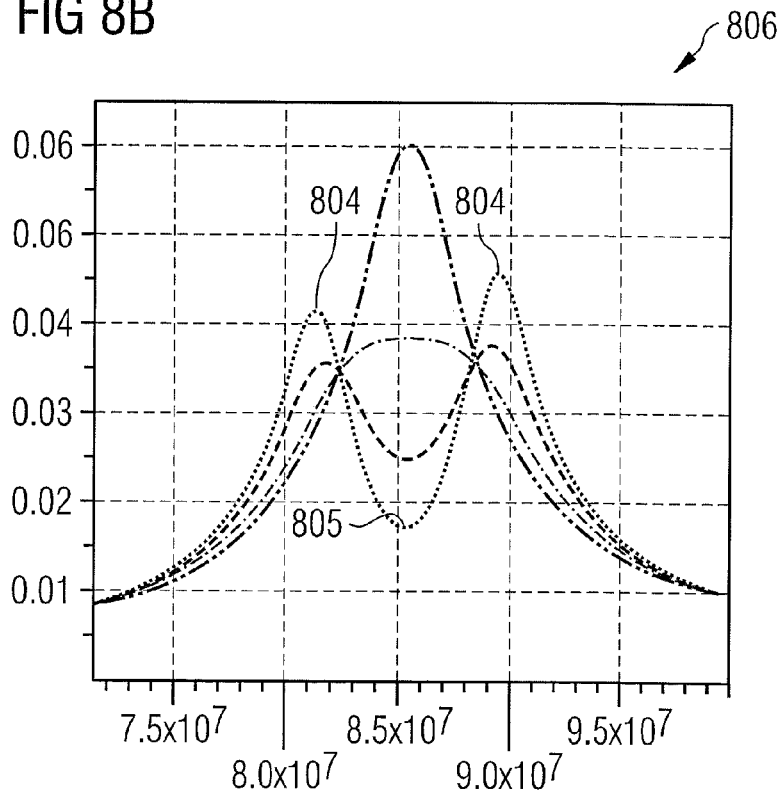


FIG 9

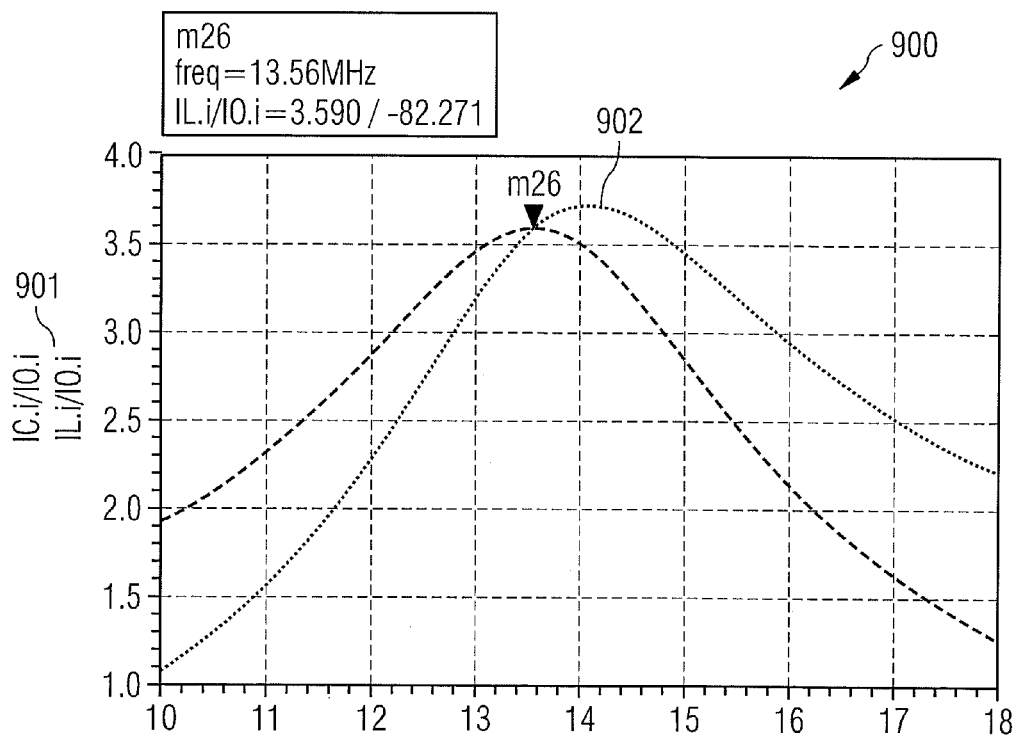


FIG 10

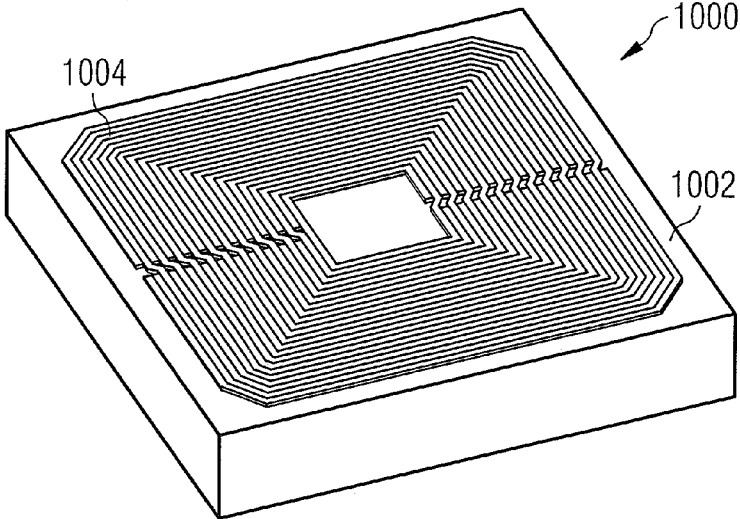
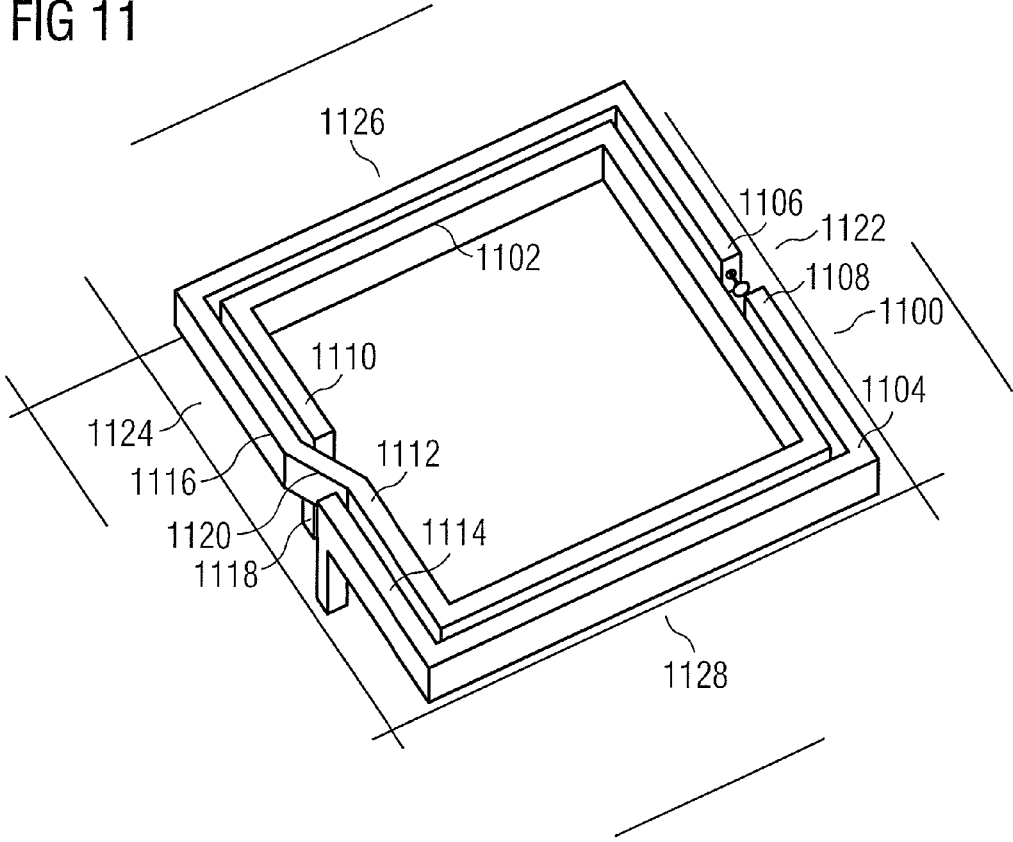


FIG 11



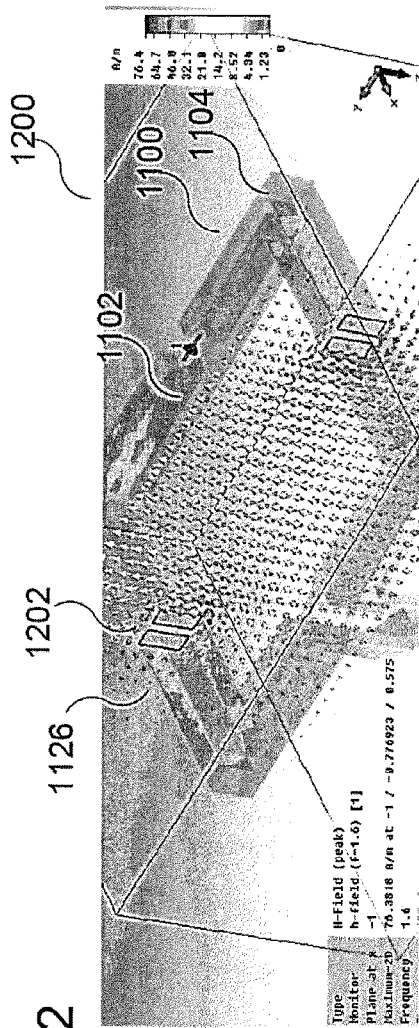


FIG 12

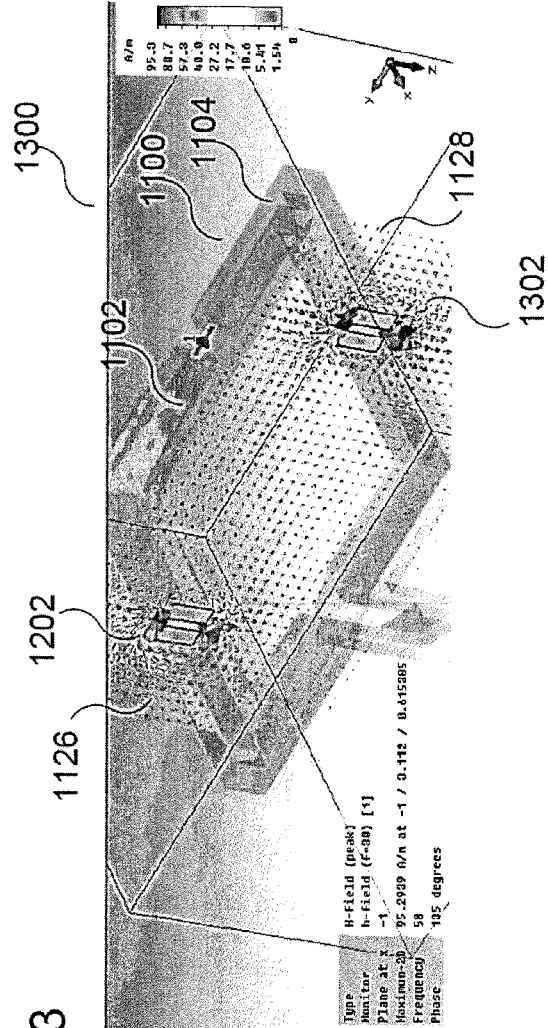


FIG 13

FIG 14

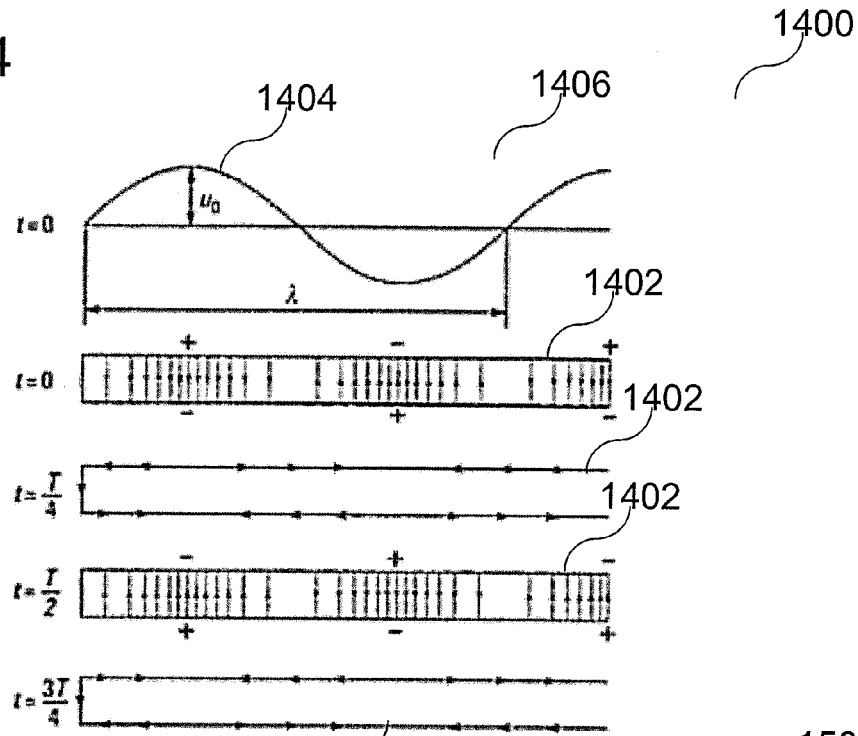
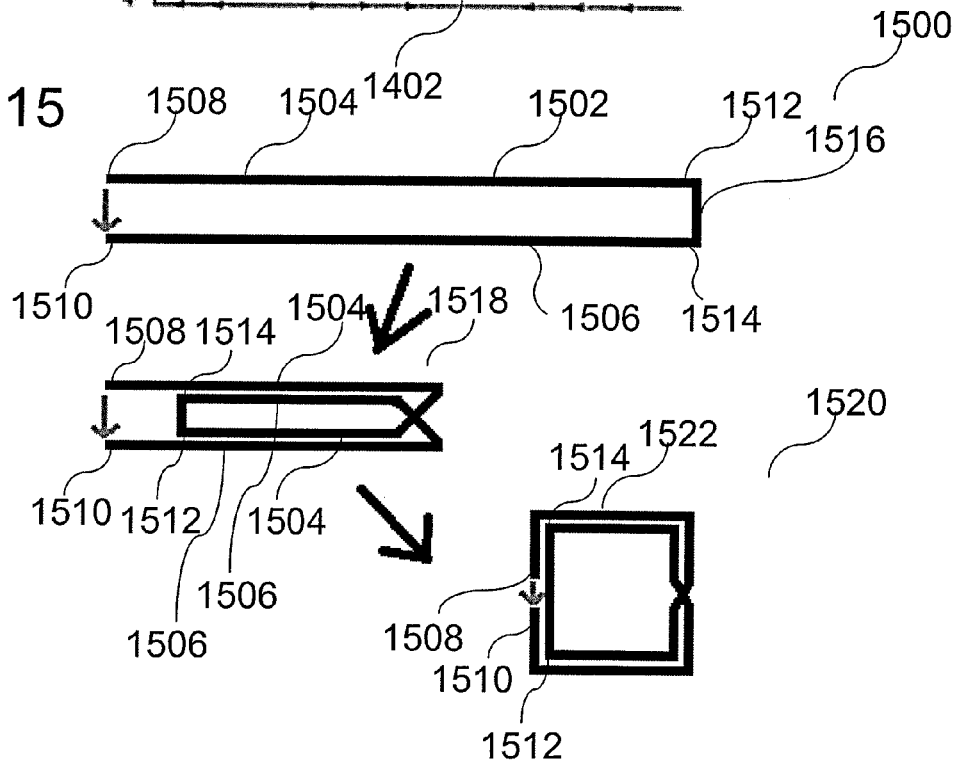


FIG 15



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BOOSTER ANTENNA, CONTACTLESS CHIP ARRANGEMENT, ANTENNA STRUCTURE AND CHIP ARRANGEMENT

CROSS-REFERENCE TO RELATED APPLICATION

This application claims priority to German Patent Application Serial No. 10 2013 102 051.8, which was filed Mar. 1, 2013, and is incorporated herein by reference in its entirety.

TECHNICAL FIELD

Various embodiments relate generally to a booster antenna, a contactless chip arrangement, an antenna structure and a chip arrangement.

BACKGROUND

In a conventional smart card which is in widespread use, for example, in the electronic payment transactions sector, the communication between the chip located on the smart card and a read device is contact-based, i.e. via smart card contacts exposed towards the outside of the smart card.

For this purpose, however, for use the smart card always needs to be inserted into a corresponding read device, which a user may find objectionable. A development which solves this problem provides so-called dual-interface smart cards, in which the chip, in addition to the conventional contact-based interface, can also communicate by means of a contactless interface. The contactless interface on the smart card can have a smart card antenna, which is contained in the smart card and is connected to the chip. The smart card antenna and the chip can be arranged together on a smart card module, in which case such a miniaturized form of the smart card antenna can then be referred to as a smart card module antenna. The joint arrangement of the coil and the chip on a smart card module is also referred to as CoM (coil on module). Irrespective of the type of smart card antenna, a galvanic connection is formed between said smart card antenna and the smart card module or the chip.

In an electronic payment system, for example, a functional distance of up to 4 cm between the chip and the read unit is required. However, meeting this setpoint input can prove to be problematic since, under certain circumstances, it is not possible for a sufficiently large smart card module antenna for enabling wireless communication at the required distance to be arranged on the small area which is available on the smart card module. In order to improve the performance of the contactless communication, in addition a so-called amplifier antenna (also referred to as booster antenna) can be built into a smart card and inductively coupled to the smart card module or the smart card module antenna arranged on the smart card module. Likewise, such a booster antenna can be inductively coupled to the CoM of a purely contactless smart card for improving the performance of the contactless communication. The booster antenna can be provided on a separate layer and contained in the smart card. The separate layer which contains the booster antenna can be or can have been laminated into the smart card during manufacture of the smart card, for example. The possible read or write distance between a write or read device and the smart card module is substantially increased by the booster antenna.

FIG. 1 shows a contactless smart card **100** with a smart card body **102**, a booster antenna **104** integrated (for

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example laminated) therein and a contactless smart card module arrangement (for example also referred to as coil on module, CoM) **106**, wherein the booster antenna **104** partially surrounds the contactless smart card module arrangement **106**.

The booster antenna **104** is formed by a large ring-shaped conductor loop **108**, wherein a small part of the conductor loop is formed to give a small conductor loop **110** which partially surrounds the contactless smart card module arrangement **106**, for example a coil on module **106**, which is arranged within a peripheral region of the large conductor loop **108**.

Furthermore, there are several approaches and embodiments for so-called comprehensive UHF-HF antennas. The dimensions and outline dimensions of said antennas generally correspond to conventional RFID (radiofrequency identification) labels, such as in accordance with a smart card, for example, and are generally realized by means of a combination of a dipole and HF coil.

SUMMARY

In various embodiments, a booster antenna for a chip arrangement is provided. The booster antenna includes: a first circuit, which forms a first resonant circuit; a second circuit, which forms a second resonant circuit, wherein the first circuit is electrically conductively connected to the second circuit; and a third circuit, which forms a third resonant circuit, wherein the third circuit is electrically conductively connected to the second circuit.

BRIEF DESCRIPTION OF THE DRAWINGS

In the drawings, like reference characters generally refer to the same parts throughout the different views. The drawings are not necessarily to scale, emphasis instead generally being placed upon illustrating the principles of the invention. In the following description, various embodiments of the invention are described with reference to the following drawings, in which:

FIG. 1 shows a conventional contactless smart card including a smart card body, a booster antenna integrated therein, and a contactless smart card module arrangement;

FIG. 2 shows a booster antenna in accordance with various embodiments;

FIG. 3 shows a booster antenna in accordance with various embodiments;

FIG. 4 shows an enlarged detail of the top left region of the booster antenna shown in FIG. 3;

FIG. 5 shows a smart card with a booster antenna in accordance with various embodiments;

FIG. 6 shows a real equivalent circuit diagram of the booster antenna shown in FIG. 5;

FIG. 7 shows a simplified equivalent circuit diagram of the booster antenna shown in FIG. 5;

FIGS. 8A and 8B show the associated locus curves and the profile of the absolute value (in an absolute value graph) of the circuit illustrated in FIG. 7;

FIG. 9 shows the ratio of the currents which flow in the second circuit to the current which is induced in the first circuit, given a corresponding Q factor of the second resonant circuit (in a current graph);

FIG. 10 shows a plan view of a chip with a (monolithically) integrated antenna structure in accordance with various embodiments;

FIG. 11 shows a plan view of a coil in accordance with various embodiments;

FIG. 12 shows a simulation illustration of a first resonance case in the coil shown in FIG. 11;

FIG. 13 shows a simulation illustration of a second resonance case in the coil shown in FIG. 11;

FIG. 14 shows an illustration of the propagation of a standing wave along a Lecher line at different times; and

FIG. 15 shows a figurative explanation of the structure of the coil shown in FIG. 11, for which reason this structure likewise forms a Lecher line.

DESCRIPTION

The following detailed description refers to the accompanying drawings that show, by way of illustration, specific details and embodiments in which the invention may be practiced.

The word “exemplary” is used herein to mean “serving as an example, instance, or illustration”. Any embodiment or design described herein as “exemplary” is not necessarily to be construed as preferred or advantageous over other embodiments or designs.

The word “over” used with regards to a deposited material formed “over” a side or surface, may be used herein to mean that the deposited material may be formed “directly on”, e.g. in direct contact with, the implied side or surface. The word “over” used with regards to a deposited material formed “over” a side or surface, may be used herein to mean that the deposited material may be formed “indirectly on” the implied side or surface with one or more additional layers being arranged between the implied side or surface and the deposited material.

In various embodiments, it is now possible for very small communication modules and/or chips with an integrated antenna to be read in various frequency bands.

In the following detailed description, reference is made to the attached drawings, which form part of this description and in which specific embodiments are shown, for illustrative purposes, in which the invention can be implemented. In this respect, directional terminology such as “at the top”, “at the bottom”, “at the front”, “at the rear”, “front”, “rear”, etc. is used with reference to the orientation of the described figure(s). Since components from embodiments can be positioned in a number of different orientations, the directional terminology is used for illustrative purposes and is in no way restrictive. It goes without saying that other embodiments can be used and structural or logic amendments can be made without departing from the scope of protection of the present invention. It goes without saying that the features of the various exemplary embodiments described herein can be combined with one another if not specifically specified otherwise. The following detailed description should therefore not be interpreted in a restrictive sense, and the scope of protection of the present invention is defined by the attached claims.

In the context of this description, the terms “connected” and “coupled” are used to describe both a direct and an indirect connection and a direct or indirect coupling. In the figures, identical or similar elements have been provided with identical reference symbols, where expedient.

In various embodiments, a combination of one or more UHF booster antennas (UHF: ultrahigh frequency) and one or more HF booster antennas (HF: high frequency) is provided. By targeted geometric arrangement of the individual components, it is now possible to read even very small communication modules and/or chips with an integrated antenna in various frequency bands. A UHF booster antenna can be designed to transmit or receive electromag-

netic waves with a frequency in a range of approximately 0.3 GHz to approximately 3 GHz. Furthermore, an HF booster antenna can be designed to transmit or receive electromagnetic waves with a frequency in a range of approximately 0.3 kHz to approximately 30 MHz.

If a UHF chip is attached at the predetermined point (also referred to as coupling region, clearly the region in which the second electrical circuit is provided for producing inductive coupling to a chip or another object), the booster antenna clearly acts as a UHF tag. If an HF OCA (OCA: On-Chip Antenna, chip with (monolithically) integrated antenna) is used, a conventional HF transponder is produced.

In addition, in various embodiments, there is the possibility of using one or more chips with a special on-chip antenna, with the result that the system functions in a similar way to a so-called comprehensive transponder. That is to say that both the chip and the booster antenna can operate at both frequencies (or frequency ranges). This results in a comprehensive transponder system.

Clearly, in various embodiments, as also in the case of standard comprehensive antennas, an outgoing line of the dipole is combined with an HF coil in a booster antenna. In various embodiments, in the case of the comprehensive booster antenna, clearly a center tap of the secondary coupling element (i.e. the coupling element which is intended for inductive coupling to a chip) is provided. While, in various embodiments, the entire secondary coupling coil can be used for HF, for UHF, for example, only the inner part of the coil winding is used. Thus, ideal coupling for both frequency bands is possible.

Clearly, in various embodiments, a different coil feed from a UHF dipole and an HF coil is provided in a booster antenna.

In various embodiments, an HF tuned circuit (as an example of the first electrical circuit) with a large coil supplies the HF resonant circuit with a small coupling coil (as an example of the second electrical circuit). Said small coupling coil has a plurality of coil turns in order to achieve a correspondingly high inductance for HF. The UHF dipole (embodied as IFA in the figure) is only connected to the inner coil turns of this coupling coil. This results in a high inductive impedance in the rest of the coil turns with respect to the outside and the UHF path cannot be short-circuited by the required HF capacitance. Therefore, the HF antenna structure and the UHF antenna structure, i.e. on the same coupling structure, produce a magnetic field which can be used, for example, for inductive coupling to OCAs or CoMs.

FIG. 2 shows a booster antenna **200** in accordance with various embodiments.

The booster antenna **200**, which is provided, for example, for a chip arrangement, for example for a smart card, can have a carrier **202** and a first circuit **204**, which is applied on the carrier **202** and which forms a first resonant circuit. The first circuit **204** can have a first coil **206** with at least one coil turn **208**. The first electrical circuit **204** can form a coupling region for inductive coupling to a write and/or read device (not illustrated). The carrier **202** can be, for example, a film, for example a plastic film.

In another configuration, the coupling region for coupling to a write and/or read device can be formed by a conductor loop.

The size of the conductor loop or of the first coil **206** can, in various embodiments, be limited substantially by the external dimensions of a carrier substrate (in other words the carrier **202**) or else, for example, the chip arrangement, for example the smart card, itself if, for example, the carrier **202**

is integrated in the chip arrangement (for example is laminated into the smart card body). In order to obtain as large an area as possible through which the electromagnetic alternating field passes, the shape of the conductor loop or coil can be matched to the shape of the substrate or the chip arrangement, for example the smart card. In addition, in respect of the configuration of the shape and size of the conductor loop or coil, standards such as, for example, ISO 7816 can be taken into consideration, which standards define regions which need to be kept free for writing, embossing or the like on the cards of electrical components such as conductor tracks.

In one configuration, the winding direction of the coil turn(s) **208** can have the same winding sense.

In another configuration, the coupling region for coupling to a write and/or read device can be formed by an HF antenna structure.

The booster antenna **200** can also have a second circuit **210** which is applied to the carrier **202** and forms a second resonant circuit. The second circuit **210** can have a second coil **212** with at least one coil turn **214**, **216**. In various embodiments, a plurality of coil turns **214**, **216** can be provided, wherein the plurality of coil turns **214**, **216** can have at least one inner coil turn **214** and at least one outer coil turn **216** running around the inner coil turn **214**. The second electrical circuit **210** can form a coupling region **218** for inductive coupling to a chip (not illustrated).

In another configuration, the inductive coupling region **218** can be part of the second electrical circuit **210**, wherein the inductive coupling region **218** can be substantially congruent with the contactless chip module, for example the contactless smart card module.

In another configuration, the inductive coupling region **218** can be formed by a conductor loop.

In another configuration, the inductive coupling region **218** can be defined by a coil, for example by the innermost coil turn **214** of the coil **212**.

In another configuration, the inductive coupling region **218** of the booster antenna **200** for coupling to a chip can be arranged completely within the further coupling region for coupling to a write and/or read device.

In another configuration, the inductive coupling region **218** of the booster antenna **200** for coupling to a chip can be arranged completely outside the further coupling region for coupling to a write and/or read device.

The booster antenna **200** can furthermore have a third circuit **220**, which is applied to the carrier **202** and forms a third resonant circuit. The third circuit **220** can have a dipole antenna **222** or be formed thereby. The dipole antenna **222** can have two electrical (for example straight linear) lines **224**, **226**, wherein a first line **224** is electrically conductively connected with its first end, for example, to the innermost end of the inner coil turn **214** of the second coil **212** (the second end of the first line **224** is free), and wherein a second line **226** is electrically conductively connected with its first end, for example, likewise to an inner coil turn **214** of the second coil **212** (the second end of the second line **226** is free). The first line **224** and the second line **226** extend away from one another, but lie along a common straight line.

The dipole antenna **222** can, however, in alternative configurations, also have another desired or suitable shape, for example a shape such as is explained in further detail below.

FIG. 3 shows a booster antenna **300** in accordance with various embodiments.

The booster antenna **300** shown in FIG. 3 has a similar design to the booster antenna **200** shown in FIG. 2, for which reason only the differences between the two booster antennas are illustrated below.

In the case of the booster antenna **300** shown in FIG. 3, the dipole antenna is in the form of an inverted F antenna (IFA) **302**. Furthermore, the second coil **212** in this embodiment has a large number of coil turns **214**, **216**, wherein a large number of inner coil turns **214** and a large number of outer coil turns **216** are provided. As illustrated in FIG. 3, a first (uppermost) (transverse) limb **304** of the "F" of the IFA **302** is electrically conductively connected to a first inner coil turn **214** of the second coil **212** by means of a first electrically conductive line **306**. In addition, a second (central) (transverse) limb **308** of the "F" of the IFA **302** is electrically conductively connected to a second inner coil turn **214** of the second coil **212** by means of a second electrically conductive line **310**.

FIG. 4 shows an enlarged detail of the top left region of the booster antenna **300** shown in FIG. 3.

In various configurations, the first circuit can form the first resonant circuit with a first phase resonance, and the second circuit can form the second resonant circuit with a second absolute resonance.

FIG. 5 shows a smart card **500** with a booster antenna **504** in accordance with various embodiments.

It should be noted that even if various exemplary embodiments are explained with reference to a smart card **500**, alternative embodiments can also be provided in other application areas. Thus, for example, the booster antenna **504** can also be arranged on a different carrier, for example a flexible carrier, for example a textile carrier (for example a patch, for example an adhesive patch). The chip module also does not necessarily need to be implemented as a smart card module, but can be, for example, a chip module which can be implanted beneath the skin of a living organism, for example.

The booster antenna **504** shown in FIG. 5 has a similar design to the booster antenna **200** shown in FIG. 2, for which reason only the differences between the two booster antennas will be illustrated below.

The smart card **500** has a smart card body **502** and a booster antenna **504** in accordance with various embodiments. In addition, the smart card **500** has a contactless smart card module **506**, for example an on-chip antenna (OCA) or a chip on module (CoM). In various embodiments, the booster antenna **504** is integrated, for example laminated, into the smart card body **502**.

The contactless smart card module **506** can have a chip and a coil, which is electrically coupled (for example electrically conductively connected) to the chip, for example by means of a conductor track. The booster antenna **504** can be inductively coupled to the coil of the contactless smart card module **506** (also referred to as contactless smart card module) by means of the at least one inductive coupling region **218** of the booster antenna **504**, as has been described above and will also be explained in more detail below. In addition, the booster antenna **504** can have at least one further coupling region for inductive coupling to a write and/or read device.

The smart card **500** and therefore also the contactless smart card module arrangement can be designed as a purely contactless smart card module arrangement. Alternatively, the smart card **500** and therefore also the contactless smart card module arrangement can optionally additionally have a contact-based smart card interface (for example a contact array **508** including a multiplicity of electrically conductive

contacts), for example in the form of smart card contacts (for example in accordance with ISO 7816), and can therefore be designed as a dual-interface smart card module arrangement.

The booster antenna **504** can have the first electrical circuit, which forms a first resonant circuit with a first phase resonance, and the second electrical circuit, which forms a second resonant circuit with a second absolute resonance. The first electrical circuit and the second electrical circuit are coupled, for example electrically, to one another.

The booster antenna **504** can have substantially two conductor loops **510**, **512**, a large conductor loop **510** and a small conductor loop **512**. The small conductor loop **512** surrounds the CoM **506** or the OCA **506**. The large conductor loop **510** is electrically conductively connected with its ends to the ends of the small conductor loop **512** and partially surrounds the small conductor loop **512**. A second capacitor **516**, which is part of the second electrical circuit, is connected in parallel with the ends of the two conductor loops **510**, **512**. In addition, the large conductor loop **510** has, in its left-hand region, a first capacitor **514**, which is connected in series. Furthermore, a dipole antenna **518** is provided as third circuit, wherein the dipole antenna **518** is electrically conductively connected to an inner coil turn **520** of the coil **522** of the second circuit. A first inductance of the first coupling region of the first circuit and a second inductance of the second coupling region of the second circuit of the booster antenna **500** are each in the form of a conductor loop **510**, **512** (a first, large conductor loop **510** and a second, small conductor loop **512**), wherein the second conductor loop **512** of the second coupling region can be arranged eccentrically within the first conductor loop **510**. The first conductor loop **510** can be interrupted in its left-hand region, wherein the ends of the first conductor loop **510** are in the form of a T at the point of interruption and therefore form a plate capacitor, namely the first capacitor **514**. The ends of the conductor loops **510**, **512** in the right-hand region of the booster antenna **500** are electrically conductively connected to one another via lines, which run parallel to one another and extend beyond the first conductor loop **510**; the lines running parallel form in turn a plate capacitor, namely the second capacitor **516**. The capacitance of this second capacitor **516** is the capacitance of the parallel resonant circuit. The second conductor loop **512** has a coil with a plurality of, for example three (alternatively two, four, five, six, seven or more), coil turns.

Therefore, the booster antenna **500** has, in various embodiments, a separate design of two resonant circuits (a series resonant circuit (formed by the first electrical circuit) and a parallel resonant circuit (formed by the second electrical circuit)), which can have the same phase resonance and absolute resonance. If the second tuned circuit is in the form of a parallel resonant circuit, for example, a current increase takes place within the circuit. These currents in the branches of the parallel resonant circuit can be a great deal higher than the input current, corresponding to the Q factor of the circuit. In simple terms, the series resonant circuit (also referred to as series tuned circuit), in which the current is induced, supplies power to the parallel resonant circuit (also referred to as the parallel tuned circuit), in which a renewed increase in current then takes place. This increase in current can be proportional to the Q factor of the respective parallel tuned circuit.

FIG. **6** shows a real equivalent circuit diagram **600** of the booster antenna **500** shown in FIG. **5**.

Furthermore, FIG. **6** shows a write/read apparatus **602**, which is coupled inductively to the smart card **500** (by means of a first inductive coupling **620**) and is therefore

coupled, by means of the booster antenna **500**, in turn inductively, to the contactless smart card module **506** (by means of a second inductive coupling **622**).

The real equivalent circuit diagram **600** of the booster antenna **500** shown in FIG. **5** has, on the coupling side with respect to the write/read apparatus **602**, a first inductance (L_{large}) **604**, a first capacitor (C_{large}) **606**, a first ohmic resistance (R_{large}) **608** and a (negligible) first parasitic capacitance (C_{large_para}) **610** of the large conductor loop, and a second inductance (L_{small}) **612**, a second capacitor (C_{small}) **614**, a second ohmic resistance (R_{small}) **616** and a (negligible) second parasitic capacitance (C_{small_para}) **618** of the small conductor loop.

Disregarding the parasitic components gives the simplified equivalent circuit diagram **700** shown in FIG. **7**.

The simplified equivalent circuit diagram **700** now only has the first inductance (L_{large}) **604**, the first capacitor (C_{large}) **606**, the first ohmic resistance (R_{large}) **608** of the large conductor loop, and the second inductance (L_{small}) **612**, the second capacitor (C_{small}) **614**, and the second ohmic resistance (R_{small}) **616** of the small conductor loop.

As can be seen from the simplified equivalent circuit diagram **700**, the components in the large conductor loop form a series resonant circuit (in other words the first electrical circuit), and the components in the small conductor loop form a parallel resonant circuit (in other words the second electrical circuit); the series resonant circuit **702** is in this case connected in series with the capacitance of the parallel resonant circuit **704**. The first inductive coupling (k) **620** to the write and/or read device (reader) **602** is performed via the first inductance **604** of the large conductor loop; the coupling to the CoM or the OCA, generally the contactless smart card module **506**, is performed via the second inductance **612** of the small conductor loop.

The phase resonances of the tuned circuits **702**, **704** can be determined using the following formulae:

$$f_{r_{small}} = \frac{1}{2 \cdot \pi \cdot i} \cdot \sqrt{\frac{1}{L_{k_{small}} C_{small}} - \frac{R_{small}^2}{L_{k_{small}}^2}} \quad (1)$$

$$f_{r_{large}} = \frac{1}{2 \cdot \pi \cdot i \cdot \sqrt{L_{large} C_{large}}} \quad (2)$$

In the present case, the two resonant circuits **702**, **704** can be dimensioned such that the phase resonance for the series resonant circuit **702** and the absolute resonance for the parallel resonant circuit **704** are 13.56 MHz.

FIG. **8A** and FIG. **8B** show the associated locus curves in a locus curve graph **800**, and the profile of the absolute value (in an absolute value graph **801**) with different Q factors of the second tuned circuit. It can be seen that, above a specific Q factor of the second tuned circuit, up to three phase resonances (first phase resonance **801**, second phase resonance **802** and third phase resonance **803**) of the overall system are possible. This is also illustrated by means of extreme points of two peaks **804** and **805** in an absolute value graph **806**.

The figures show that, in the second resonance case (first phase resonance **803** and associated absolute value minimum **805**), the impedance now only has the real component. These points correspond to the operating frequency of the booster antenna. If the Q factor of the first series tuned circuit were to be changed, the curves illustrated in the locus curve graph **800** would shift along the x axis.

FIG. 9 shows a current graph 900. Here, the ratio of the currents 901 which flow in the second circuit (IL and IC) to the current which is induced in the first circuit is illustrated given a corresponding Q factor of the second resonant circuit.

FIG. 9 illustrates how the current in the coupling structure of the small inductance (second circuit) is markedly increased in comparison with the current in the large inductance (first circuit). The markedly increased current in the small conductor loop then brings about an intensified magnetic field, as a result of which the coupling to the contactless smart card module 506 is significantly improved.

The higher the Q factor of the second tuned circuit, the less the current maxima 902 are shifted with respect to the operating frequency. The ratio of the current rise 902 to the input current approximately corresponds to the Q factor of the second resonant circuit.

As has been described above, in general the first electrical circuit and the second electrical circuit can be designed such that the first phase resonance (i.e. the phase resonance of the first electrical circuit) and the second absolute resonance (i.e. the absolute resonance of the second electrical circuit) are identical. The first electrical circuit and the second electrical circuit can be designed (in other words dimensioned) such that the first phase resonance and/or the second absolute resonance is/are approximately 13.56 MHz.

The booster antenna in accordance with various configurations can be designed and dimensioned such that the smart card can be operated in the HF frequency range (for example by means of the first electrical circuit) or in the UHF frequency range (for example by means of the third electrical circuit).

The combined booster antenna, i.e. a booster antenna which, in accordance with various embodiments, supports a plurality of frequency bands, can now be used with HF-OCAs and/or UHF-OCAs.

By virtue of the use of a so-called comprehensive OCA, a comprehensive transponder which operates both at UHF and at HF is produced.

Various embodiments can be used, for example, in the following exemplary application:

A passive sensor device (OCA chip with one or more sensors) which is implanted under the skin of a living organism, for example a human, can be provided for reading biosignals such as temperature, glucose or the like.

This chip is supplied, for example, with energy via HF (the coupling structure produces sufficient energy for maintaining the operation of the chip). This HF energy comes from the direct vicinity; a base station or an energy harvester, which is implemented on the patch (on which the booster antenna can also be located). The measured sensor data are transmitted via UHF in various embodiments, however. This considerably increases the range. Patients in a hospital room can thus easily be monitored via a method which is simple to realize and not damaging to health.

A further exemplary application can be considered to be in a combination of trademark protection and logistics application, wherein UHF can be used for the logistics sector (EPC, evolved packet core, clearly communication via a 3GPP communications network), and wherein HF can be used for communication with the user as near-field communication (NFC).

By virtue of the use of one or more comprehensive booster antennas, the advantages of both frequency bands are combined. UHF provides a wide read/write range and is used universally in logistics. Packages can thus be localized and monitored easily.

The NFC application is of significance, for example, for the end consumer. In this case, detailed information on the product are called up from the direct vicinity, for example, by means of a mobile radio communications terminal with NFC capability.

FIG. 10 shows a plan view of a chip 1000 with a carrier 1002, for example including silicon (or another suitable semiconductor material or another suitable composite semiconductor material), and with an antenna structure 1004 (monolithically) integrated in the carrier 1002.

At least one circuit (not illustrated), for example a logic circuit and/or a memory circuit, is contained in the carrier 1002.

The chip 1000 therefore clearly represents an on-chip antenna (OCA).

As will be explained in more detail below, the chip 1000 represents a comprehensive antenna, which supports both HF and UHF.

By means of this design, the antenna described below can be operated at a plurality of different frequencies (or frequency ranges).

For example in applications with on-chip antennas, this variant enables a multifrequency band function which can be realized very easily.

By virtue of the specially shaped coil of the antenna structure 1004 described below of the chip 1000, a plurality of resonance cases result, which occur in different frequency bands, depending on the geometry.

This makes it possible to use the antenna structure 1004, owing to its small design, as a comprehensive on-chip antenna.

This (for example) RFID chip 1000 can therefore be operated at different frequencies.

The antenna structure 1004 can have a coil antenna having a plurality of coil turns, wherein the antenna structure is designed such that, in the case of a predetermined operating frequency of an antenna signal, a standing wave of the antenna signal is formed on said antenna structure. The antenna structure 1004 can have a Lecher line structure, as will be explained in more detail below.

This can be achieved, for example, by providing a special geometric structure of the coil.

Thus, the coil 1100 can have a structure as illustrated in plan view in FIG. 11, for example.

The coil 1100 can have two coil turns 1102, 1104, wherein a first coil turn 1102 runs substantially completely within a second coil turn 1104. A first coil connection 1106 and a second coil connection 1108 are provided at the respective ends of the coil 1100, to be precise, for example, at the outer second coil turn 1104. The corresponding potential difference of the antenna signal needs to be provided at the two coil connections 1106, 1108. Over the course of the two coil turns 1102, 1104, the two coil turns intersect one another, with the result that a respective connection 1110, 1112 of the first coil turn 1102 is connected (i.e. electrically conductively connected) in pairs to a respective connection 1114, 1116 of the second coil turn 1104. Expressed more precisely, this means that a first connection 1110 of the first coil turn 1102 is electrically conductively connected to a first connection 1114 of the second coil turn 1104 by means of a first connecting line 1118, and that a second connection 1112 of the first coil turn 1102 is electrically conductively connected to a second connection 1116 of the second coil turn 1104 by means of a second connecting line 1120, wherein the first connecting line 1118 and the second connecting line 1120 intersect one another, wherein the two connecting lines 1118, 1120 run one on top of the other and are electrically

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insulated from one another, for example by means of an oxide (for example silicon oxide) and/or by means of a nitride (for example silicon nitride) or one or more other insulating materials or insulating layers.

The coil **1100** has, for example, a rectangular (for example square) shape or a round shape (for example elliptical or circular shape). FIG. **11** shows the coil with a substantially square shape, wherein the coil has a first side **1122** (on which the coil connections **1106**, **1108** are provided), a second side **1124** (on which the connecting lines **1118**, **1120** are provided) opposite the first side, and a third side **1126**, which electrically conductively connects the lines of the coil turns **1102**, **1104** of the first side **1122** to the lines of the coil turns **1102**, **1104** of the second side **1124** at their first ends, and a fourth side **1128**, which electrically conductively connects the lines of the coil turns **1102**, **1104** of the first side **1122** to the lines of the coil turns **1102**, **1104** of the second side **1124** at their second ends.

This structure can be provided so as to be repeated as often as desired in the antenna structure **1004**, with the result that, for example, the antenna structure **1004** illustrated in FIG. **10** is produced.

A first resonant frequency results in the case of the antenna structure **1004** as in a conventional coil. In this case, the inductances and the parasitic chip capacitances rise and a resonance case arises, as is illustrated in a first simulation illustration **1200** in FIG. **12** for the coil **1100**. As illustrated in FIG. **12**, the strongest magnetic field forms in the coil **1200** in the first resonance case on the left-hand side, i.e. clearly approximately in the center **1202** of the lines of the coil turns **1102**, **1104** on the third side **1126**.

At relatively high frequencies, the wave propagation on the lines can be visualized as being in the case of a Lecher line. When the structure is selected such that a lambda (or a multiple) (i.e. a wavelength or a multiple of the wavelength of the antenna signal) propagates on the line, therefore, a second resonance case arises, as is illustrated in a second simulation illustration **1300** in FIG. **13** for the coil **1100**. As illustrated in FIG. **13**, in the second resonance case the strongest magnetic field forms in the coil **1200** both on the left-hand side, i.e. clearly approximately in the center **1202** of the lines of the coil turns **1102**, **1104** on the third side **1126**, and on the right-hand side, i.e. clearly approximately in the center **1302** of the lines of the coil turns **1102**, **1104** on the fourth side **1128**.

FIG. **14** shows an illustration **1400** of the propagation of a standing wave along a Lecher line **1402** at different times. Thus, at a time $t=0$, a sinusoidal electromagnetic wave **1404** with a wavelength λ and a maximal amplitude up is illustrated in a first graph **1406**. Furthermore, FIG. **14** shows, at the respective times $t=0$, $t=T/4$, $t=T/2$, and $t=3T/4$, the propagation of the magnetic field **1404** between the elements of the Lecher line **1402**.

FIG. **15** shows a graphical explanation of the structure of the coil shown in FIG. **11**, for which reason this structure likewise forms a Lecher line.

First, FIG. **15** shows, in a first illustration **1500**, a conventional Lecher line **1502**, which has a U-shaped profile. The Lecher line **1502** has two mutually opposite, parallel lines **1504**, **1506**, which are electrically insulated from one another at their first ends **1508**, **1510** and are electrically conductively connected to one another at their second ends **1512**, **1514** by means of an electrically conductive connecting element **1516**.

Furthermore, FIG. **15** shows, in a second illustration **1518**, that the Lecher line **1502** from the first illustration **1500** is firstly folded and secondly rotated through 180° . The

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corresponding end points of the Lecher line **1502** from the first illustration **1500** are correspondingly indicated in the second illustration **1518**.

If the Lecher line **1502** from the second illustration **1518** still with the same dimensions in respect of the wave propagation is brought into a square form, the Lecher line structure **1522** as indicated in a third illustration **1520** results. This Lecher line structure **1522** corresponds to the structure of the coil **1100** as illustrated in FIG. **11** and as has been explained correspondingly above.

In various embodiments, a booster antenna for a chip arrangement, for example for a smart card, is provided, wherein the booster antenna includes: a first circuit, which forms a first resonant circuit; a second circuit, which forms a second resonant circuit, wherein the first circuit is electrically conductively connected to the second circuit; and a third circuit, which forms a third resonant circuit, wherein the third circuit is electrically conductively connected to the second circuit.

In one configuration, the first circuit can form the first resonant circuit with a first phase resonance; wherein the second circuit can form the second resonant circuit with a second absolute resonance.

In another configuration, the first electrical circuit and the second electrical circuit can be designed such that the first phase resonance and/or the second absolute resonance is/are approximately 13.56 MHz.

In another configuration, the third circuit can form the third resonant circuit with a third phase resonance.

In another configuration, the third electrical circuit can be designed such that the third phase resonance is greater than the first phase resonance.

In another configuration, the third electrical circuit can be designed such that the third phase resonance is in a range of approximately 0.3 GHz to approximately 3 GHz.

In another configuration, the third electrical circuit can be designed such that the third phase resonance is approximately 868 MHz.

In another configuration, the third circuit can have a dipole antenna.

In another configuration, the dipole antenna may include an inverted F antenna (IFA) or can be in the form of such an antenna.

In another configuration, the second electrical circuit can have an inductive coupling structure.

In another configuration, the first electrical circuit can be connected in series with the second electrical circuit.

In another configuration, the first resonant circuit and the second resonant circuit can be designed such that a first current in the first resonant circuit effects an increased second current, in comparison with the first current, in the second resonant circuit.

In another configuration, the first resonant circuit can be a series resonant circuit.

In another configuration, the second resonant circuit can be a parallel resonant circuit.

In another configuration, the second circuit can have at least one coil turn.

In another configuration, the second circuit can have a plurality of coil turns.

In another configuration, the second circuit can have an outer coil turn and a plurality of inner coil turns.

In another configuration, the third circuit can be electrically conductively connected only to the inner coil turns.

In another configuration, the booster antenna may furthermore include a flexible carrier, for example a patch;

wherein the first electrical circuit, the second electrical circuit and the third electrical circuit can be arranged on the flexible carrier.

In various embodiments, a contactless chip arrangement is provided, for example a contactless smart card module arrangement, including: a booster antenna, as has been described above and will be explained in more detail below; and a contactless chip module, for example a contactless smart card module, which includes: a chip; and a coil, which is electrically coupled to the chip; wherein the booster antenna is inductively coupled to the coil of the contactless chip module, for example the contactless smart card module, by means of at least one inductive coupling region of the booster antenna.

The chip arrangement can be any desired arrangement which has a chip, for example a portable arrangement with a chip. The booster antenna can be arranged, for example, on a flexible carrier as well, for example on a textile carrier, for example on a patch (for example on an adhesive patch).

By corresponding dimensioning and design of the individual components of the first electrical circuit and/or the second electrical circuit, a multiplicity of possible application cases is provided. Both the first and the second resonant circuit can be adjusted very easily to a specific phase resonance or absolute resonance by corresponding dimensioning of the circuit components. By virtue of the separate design, in addition the parameterization and verification of the booster antenna are considerably simplified.

In one configuration, the contactless chip module, for example contactless smart card module, can be a module with an integrated coil (coil on module, CoM) or a module with an integrated antenna (on-chip antenna, OCA).

In yet another configuration, the contactless chip module with an integrated coil (coil on module, CoM) or a module with an integrated antenna (on-chip antenna, OCA) can have a predetermined, for example predefined, specific distance from the coupling element of the booster antenna.

In yet another configuration, the contactless chip module with an integrated coil (coil on module, CoM) or a module with an integrated antenna (on-chip antenna, OCA) can be located in a different matter (for example can be implanted in a muscle or in the body of a living organism).

In one configuration, the booster antenna can have at least one further coupling region for coupling to a write and/or read device.

In yet another configuration, the first electrical circuit can form the further coupling region for coupling to a write and/or read device.

In yet another configuration, the inductive coupling region can be part of the second electrical circuit; wherein the inductive coupling region can be arranged substantially congruently with the contactless chip module, for example the contactless smart card module.

In yet another configuration, the further coupling region for coupling to a write and/or read device can be formed by a dipole.

In yet another configuration, the inductive coupling region of the booster antenna for coupling to a chip can be arranged completely within the further coupling region for coupling to a write and/or read device.

In yet another configuration, the inductive coupling region of the booster antenna for coupling to a chip can be arranged completely outside the further coupling region for coupling to a write and/or read device.

In yet another configuration, the contactless chip module, for example the contactless smart card module, can also have chip contacts, for example smart card contacts, which

can be designed to provide a contact-based chip interface, for example smart card interface.

In yet another configuration, the contactless chip arrangement, for example contactless smart card module arrangement, can be designed as a dual-interface chip module arrangement, for example as a dual-interface smart card module arrangement.

In various embodiments, a contactless chip arrangement is provided, for example a smart card, including: a chip module arrangement, for example a contactless smart card module arrangement, as has been described above and will be explained in more detail below.

It is thus possible, for example, to design and dimension the components of the circuits in such a way that it is possible to cause the first tuned circuit (in other words the first resonant circuit) to oscillate with an external, weak electromagnetic field, for example to set it to phase resonance or absolute resonance. The latter case would result in the magnitude of the impedance of the first series resonant circuit being at a minimum and the current induced in the first resonant circuit being at a maximum. The second circuit can likewise be excited by the first circuit being coupled to the second circuit. If the second tuned circuit is in the form of a parallel resonant circuit, for example, an increase in current occurs within the circuit. These currents in the branches of the parallel resonant circuit can be a great deal higher than the excitation current corresponding to the Q factor of the circuit.

As a result, in addition to the conventional geometric booster effect, an electromagnetic property which results in an electrical booster effect is also utilized.

In one configuration, at least part of the second electrical circuit of the booster antenna forms an inductive coupling region for coupling to an antenna of a chip module, for example a smart card module. The inductive coupling region can be provided, for example, by the formation of a conductor loop or a coil. For example, the shape of the conductor loop or the coil of the inductive coupling region of the booster antenna can correspond to or approximate the shape of the antenna of the contactless chip module, for example the contactless smart card module. Furthermore, provision can be made for the dimensions, in other words the size dimensions, of the conductor loop or the coil of the inductive coupling region of the booster antenna to also correspond to or at least approximate the shape of the antenna of the contactless chip module, for example the contactless smart card module. An improvement in the coupling between the booster antenna and the contactless chip module, for example the contactless smart card module, can also be achieved if the conductor loop or the coil of the inductive coupling region of the booster antenna tightly surrounds or is arranged congruently above or beneath the antenna of the contactless chip module, for example the contactless smart card module, with the result that a magnetic field produced by the coil or the conductor loop passes through the coil of the contactless chip module, for example the contactless smart card module, as efficiently as possible.

The first electrical circuit of the booster antenna can be, for example, an HF tuned circuit or form such an HF tuned circuit. The third electrical circuit of the booster antenna can be, for example, a UHF tuned circuit (for example a UHF dipole) or form such a UHF tuned circuit.

The second electrical circuit may include a plurality of coil turns and therefore at least one inner coil turn and at least one outer coil turn. The third electrical circuit and

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therefore, for example, the UHF dipole can, in various embodiments, only be electrically conductively connected to the inner coil turn(s).

As a result, a high inductive impedance of the remaining coil turns can be produced on the outside, and the UHF path cannot be short-circuited by the required HF capacitance.

It would appear that the first electrical circuit and the third electrical circuit are designed and electrically conductively connected or coupled to one another and to the second electrical circuit in such a way that the first electrical circuit and the third electrical circuit (i.e., for example, the HF tuned circuit and the UHF tuned circuit) produce a magnetic field on the same coupling structure (as an example of the second electrical circuit), which can be used for inductive coupling to an antenna on a chip or to an antenna on another object.

In various embodiments, an antenna structure is provided including a coil antenna including a plurality of coil turns, wherein the antenna structure is designed such that, at a predetermined operating frequency of an antenna signal, a standing wave of the antenna signal forms on said antenna structure.

In one configuration, the antenna structure can have a Lecher line structure or be formed by such a Lecher line structure.

In various embodiments, a chip arrangement is provided, including: at least one chip; and an antenna structure coupled to the chip, as has been described above and will be explained in more detail below.

In one configuration, the chip and the antenna structure can be applied to a common carrier.

In another configuration, the chip and the antenna structure can be applied in monolithically integrated fashion to a common carrier.

Embodiments of the invention are illustrated in the figures and will be explained in more detail below.

While the invention has been particularly shown and described with reference to specific embodiments, it should be understood by those skilled in the art that various changes in form and detail may be made therein without departing from the spirit and scope of the invention as defined by the appended claims. The scope of the invention is thus indicated by the appended claims and all changes which come within the meaning and range of equivalency of the claims are therefore intended to be embraced.

What is claimed is:

1. A booster antenna for a chip arrangement, the booster antenna comprising:

a first circuit, which forms a first resonant circuit with a first phase resonance;

a second circuit, which forms a second resonant circuit, wherein the first circuit is electrically conductively connected to the second circuit;

a third circuit, which forms a third resonant circuit with a third phase resonance, wherein the third circuit forms a dipole antenna, wherein the dipole antenna is not short-circuited; and wherein the dipole antenna comprises an inverted F antenna; and

wherein the second circuit comprises a coil comprising at least one coil turn where an end of an innermost coil turn is directly connected to an end of an electrical line of the dipole antenna.

2. The booster antenna of claim 1, wherein the second circuit forms the second resonant circuit with a second absolute resonance.

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3. The booster antenna of claim 2, wherein the first electrical circuit and the second electrical circuit are designed such that at least one of the first phase resonance or the second absolute resonance is or are approximately 13.56 MHz.

4. The booster antenna of claim 1, wherein the third electrical circuit is designed such that the third phase resonance is greater than the first phase resonance.

5. The booster antenna of claim 1, wherein the third electrical circuit is designed such that the third phase resonance is in a range of approximately 0.3 GHz to approximately 3 GHz.

6. The booster antenna of claim 1, wherein the second electrical circuit has an inductive coupling structure.

7. The booster antenna of claim 1, wherein the first electrical circuit is connected in series with the second electrical circuit.

8. The booster antenna of claim 1, wherein the first resonant circuit is a series resonant circuit.

9. The booster antenna of claim 1, wherein the second resonant circuit is a parallel resonant circuit.

10. The booster antenna of claim 1, further comprising: a flexible carrier; wherein the first electrical circuit, the second electrical circuit and the third electrical circuit are arranged on the flexible carrier.

11. A contactless chip arrangement, comprising: a booster antenna comprising:

a first circuit, which forms a first resonant circuit with a first phase resonance;

a second circuit, which forms a second resonant circuit, wherein the first circuit is electrically conductively connected to the second circuit;

a third circuit, which forms a third resonant circuit with a third phase resonance, wherein the third circuit forms a dipole antenna, wherein the dipole antenna is not short-circuited; wherein the dipole antenna comprises an inverted F antenna; and

wherein the second circuit comprises a coil comprising at least one coil turn where an end of an innermost coil turn is directly connected to an end of an electrical line of the dipole antenna;

a contactless chip module, which comprises:

a chip; and

a coil, which is electrically coupled to the chip; wherein the booster antenna is inductively coupled to the coil of the contactless chip module, by means of at least one inductive coupling region of the booster antenna.

12. The contactless chip arrangement of claim 11, wherein the booster antenna has at least one further coupling region for coupling to a write and/or read device.

13. The contactless chip arrangement of claim 12, wherein the first electrical circuit forms the further coupling region for coupling to at least one of a write device or read device.

14. The contactless chip arrangement of claim 12, wherein the further coupling region for coupling to at least one of a write device or read device is formed by a dipole.

- 15.** The contactless chip arrangement of claim **12**,
wherein the inductive coupling region of the booster
antenna for coupling to a chip is arranged completely
within the further coupling region for coupling to at
least one of a write device or read device. 5
- 16.** The contactless chip arrangement of claim **12**,
wherein the inductive coupling region of the booster
antenna for coupling to a chip is arranged completely
outside the further coupling region for coupling to a at
least one of a write device or read device. 10
- 17.** The contactless chip arrangement of claim **11**,
wherein the inductive coupling region is part of the
second electrical circuit; and
wherein the inductive coupling region is arranged sub-
stantially congruently with the contactless chip module. 15
- 18.** The contactless chip arrangement of claim **11**,
wherein the contactless chip module further has chip
contacts, which are designed to provide a contact-based
chip interface.
- 19.** The contactless chip arrangement of claim **11**, 20
designed as a dual-interface chip module arrangement.

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