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(54) FLUID CONTROL DEVICE

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- (58) Field of Classification Search CPC F04B 43/046; F04B 45/047

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USPC 417/413.2, 413.3, 480 See application file for complete search history.

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(57) ABSTRACT

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A fluid control device includes a vibrating plate unit, a driver, and a flexible plate. The vibrating plate unit includes a vibrating plate with first and second main surfaces, a frame plate surrounding the vibrating plate, and a link portion linking the vibrating plate and the frame plate and elastically supporting the vibrating plate against the frame plate. The driver is on the first main surface of the vibrating plate, and vibrates the vibrating plate. The flexible plate having a hole faces the second main surface of the vibrating plate, being fixed to the frame plate. At least a portion of the vibrating plate and the link portion are thinner than the thickness of the frame plate so that the surface of the portion of the vibrating plate and the link portion, on the side of the flexible plate, can separate from the flexible plate.

9 Claims, 7 Drawing Sheets



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FIG.4















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FLUID CONTROL DEVICE

CROSS REFERENCE

This non-provisional application claims priority under 35 5 U.S.C. §119(a) to Patent Application No. 2011-194427 filed in Japan on Sep. 6, 2011, the entire contents of which are hereby incorporated by reference.

BACKGROUND OF THE INVENTION

1. Field of the Invention

The present invention relates to a fluid control device which performs fluid control.

2. Description of the Related Art

International Publication No. 2008/069264 discloses a conventional fluid pump (see FIGS. 1A to 1E). FIG. 1A to FIG. 1E show operations of the conventional fluid pump in a tertiary mode. The fluid pump, as shown in FIG. 1A, includes a pump body 10; a vibrating plate 20 in which the 20 outer peripheral portion thereof is attached to the pump body 10; a piezoelectric element 23 attached to the central portion of the vibrating plate 20; a first opening 11 formed on a portion of the pump body 10 that faces the approximately central portion of the vibrating plate 20; and a second 25 opening 12 formed on either one of a region intermediate between the central portion and the outer peripheral portion of the vibrating plate 20 or a portion of the pump body 10 that faces the intermediate region.

The vibrating plate **20** is made of metal. The piezoelectric 30 element **23** has a size so as to cover the first opening **11** and a size so as not to reach the second opening **12**.

In the above mentioned fluid pump, by applying voltage having a predetermined frequency to the piezoelectric element 23, a portion of the vibrating plate 20 that faces the first 35 opening 11 and a portion of the vibrating plate 20 that faces the second opening 12 are bent and deformed in opposite directions, as shown in FIG. 1A to FIG. 1E. This causes the fluid pump to draw fluid from one of the first opening 11 and the second opening 12 and to discharge the fluid from the 40 other opening.

The above mentioned fluid pump, as is shown in FIG. 1A with a conventional structure, has a simple structure, and thus the thickness of the fluid pump can be made thinner. Such a fluid pump is used, for example, as an air transport 45 pump of a fuel cell system.

At the same time, electronic equipment and apparatuses into which the fluid pump is incorporated have tended to be miniaturized. Therefore, it is necessary to further miniaturize the fluid pump without reducing the pump performance 50 (the discharge flow rate and the discharge pressure) of the fluid pump.

However, the performance of the fluid pump decreases as the fluid pump becomes smaller. Therefore, there are limitations to miniaturizing the fluid pump having the conven-55 tional structure while maintaining the pump performance.

Accordingly, the inventors of the present invention have devised a fluid pump having a structure shown in FIG. 2.

FIG. 2 is a sectional view showing a configuration of a main portion of the fluid pump. The fluid pump **901** is 60 provided with a flexible plate **35**, a vibrating plate unit **38**, and a piezoelectric element **32**, and is provided with a structure in which the components are layered in that order.

The vibrating plate unit **38** includes a vibrating plate **31**, a frame plate **33**, and a link portion **34**. The vibrating plate **65** unit **38** is formed of metal. In addition, the piezoelectric element **32** and the vibrating plate **31** bonded to the piezo-

electric element 32 constitute an actuator 30. The vibrating plate 31 has the frame plate 33 provided therearound. The vibrating plate 31 is linked to the frame plate 33 by the link portion 34. A ventilation hole 35A is formed in the center of 5 the flexible plate 35. Moreover, the frame plate 33 is fixed to the end of the flexible plate 35 by an adhesive agent layer 37. For this reason, the vibrating plate 31 and the link portion 34 are supported by the frame plate 33 in a position spaced away from the flexible plate 35 by a distance equal 10 to the thickness of the adhesive agent layer 37. The link portion 34 has an elastic structure having the elasticity of a small spring constant.

Therefore, the vibrating plate **31** is flexibly and elastically supported at two points against the frame plate **33** by two link portions **34**. For this reason, the bending vibration of the vibrating plate **31** generated by expansion and contraction of the piezoelectric element **32** cannot be blocked at all. In other words, the fluid pump **901** has a structure in which the peripheral portion of the actuator **30** is not substantially fixed. Accordingly, there will be a reduction in the loss caused by the bending vibration of the actuator **30**.

Consequently, since the flexible plate **35** vibrates with driving of the actuator **30**, the amplitude of vibration of the fluid pump **901** is effectively increased. This allows the fluid pump **901** to produce a high discharge pressure and a large discharge flow rate despite the small size and low profile design thereof.

However, in the fluid pump **901**, when the frame plate **33** and the flexible plate **35** are fixed by an adhesive agent, an excess amount of the adhesive agent may possibly flow into a gap between the link portion **34** and the flexible plate **35** from the adhesive agent layer **37**. Due to this, there is a possibility that the link portion **34** and the flexible plate **35** adhere to each other and block the vibration of the actuator **30**.

In addition, although a distance between the vibrating plate **31** and the flexible plate **35** is determined by a thickness of the adhesive agent layer **37**, it is extremely difficult to accurately and consistently achieve an exact distance determined by the applied amount of the adhesive agent. For this reason, in the fluid pump **901**, a distance between the vibrating plate **31** and the flexible plate **35** that affects the pressure-flow rate characteristics of the fluid pump **901** cannot be accurately and consistently defined. Thus, the fluid pump **901** has a problem that the pressure-flow rate characteristics of the fluid pump **901** fluctuate with each fluid pump **901**.

SUMMARY OF THE INVENTION

To overcome the problems described above, preferred embodiments of the present invention provide a fluid control device that prevents vibration of a vibrating plate from being blocked by an adhesive agent as well as prevents fluctuations in pressure-flow rate characteristics.

A fluid control device according to a preferred embodiment of the present invention includes a vibrating plate unit, a driver, and a flexible plate. The vibrating plate unit includes a vibrating plate including a first main surface and a second main surface, a frame plate that surrounds the vibrating plate, and a link portion that links the vibrating plate and the frame plate and elastically supports the vibrating plate against the frame plate. The driver is provided on the first main surface of the vibrating plate, and vibrates the vibrating plate. The flexible plate has a hole, faces the second main surface of the vibrating plate, and is fixed to the frame plate. At least a portion of the vibrating plate and the link portion are thinner than a thickness of the frame plate so that surfaces of the portion of the vibrating plate and the link portion, on the side of the flexible plate, separate from the flexible plate.

With this configuration, the surface of the link portion, on the side of the flexible plate, is spaced away from the flexible plate. Thus, even if an excess of the adhesive agent flows into a gap between the link portion and the flexible plate, the fluid control device can prevent the link portion from 10 adhering to the flexible plate.

Similarly, with this configuration, the surface of a portion of the vibrating plate on the side of the flexible plate is separated from the flexible plate. Thus, even if an excess of the adhesive agent flows into a gap between a portion of the 15 vibrating plate and the flexible plate, the fluid control device can prevent the portion of the vibrating plate and the flexible plate from adhering to each other.

Therefore, the fluid control device can prevent the portion of the vibrating plate and the link portion, and the flexible 20 plate from adhering to each other as well as blocking the vibration of the vibrating plate.

In addition, with this configuration, the difference between the thickness of a portion of the vibrating plate and the thickness of the frame plate is equivalent to the distance 25 between the portion of the vibrating plate and the flexible plate. In other words, in the fluid control device, the distance that affects the pressure-flow rate characteristics is determined accurately by partially varying the thickness of the vibrating plate unit on the side of the flexible plate. As such, 30 the fluid control device can prevent the pressure-flow rate characteristics from fluctuating with each fluid control device.

Thus, the fluid control device can prevent the vibration of the vibrating plate from being blocked through an inflow of 35 the adhesive agent as well as preventing the fluctuations in pressure-flow rate characteristics.

The vibrating plate unit preferably defines an integral unit.

With this configuration, the distance that affects the pressure-flow rate characteristics is determined accurately by partially varying the thickness of the integrally provided vibrating plate unit on the side of the flexible plate. As such, the fluid control device can prevent the pressure-flow rate characteristics from fluctuating with each fluid control 45 device.

In addition, at least a portion of the vibrating plate and the link portion are made thinner than the thickness of the frame plate by etching, for example.

With this configuration, the surface of the portion of the 50 vibrating plate and the link portion, on the side of the flexible plate, is etched. For this reason, with this configuration, the distance between the portion of the vibrating plate and the link portion, and the flexible plate is accurately determined by the etching depth. 55

Thus, the fluid control device can further prevent the pressure-flow rate characteristics from fluctuating with each fluid control device.

A portion of the vibrating plate is preferred to be an end of the vibrating plate, of the whole of the vibrating plate, 60 nearest to an adhesion portion between the flexible plate and the frame plate.

With this configuration, the surface of the end of the vibrating plate on the side of the flexible plate is separated from the flexible plate. For this reason, even though an 65 excess of the adhesive agent flows into the gap between the end of the vibrating plate and the flexible plate, the fluid

control device prevents the end of the vibrating plate and the flexible plate from adhering to each other. Thus, the fluid control device prevents the end of the vibrating plate and the flexible plate from adhering to each other as well as blocking the vibration of the vibrating plate.

Moreover, preferably, a hole portion is formed in a region of the flexible plate facing the link portion.

With this configuration, when the frame plate and the flexible plate are fixed by the adhesive agent, an excess of the adhesive agent flows into the hole portion. For this reason, the fluid control device can further prevent the vibrating plate and the link portion, and the flexible plate from adhering to each other. In another words, the fluid control device can further prevent the vibration of the vibrating plate from being blocked by the adhesive agent.

Additionally, the vibrating plate and the driver constitute an actuator and, the actuator is preferred to be disc shaped.

With this configuration, the actuator vibrates in a rotationally symmetric pattern (a concentric circular pattern). For this reason, an unnecessary gap is not generated between the actuator and the flexible plate. Therefore, the fluid control device enhances operational efficiency as a pump.

Preferably, the flexible plate includes a movable portion that is positioned in the center or near the center of the region of the flexible plate on a side facing the vibrating plate and can bend and vibrate; and a fixing portion that is positioned outside the movable portion in the region and is substantially fixed.

According to this configuration, the movable portion vibrates with vibration of the actuator. For this reason, in the fluid control device, the amplitude of vibration is effectively increased. Thus, the fluid control device can achieve a higher discharge pressure and a larger discharge flow rate despite the small size and low profile design thereof.

The above and other elements, features, steps, characteristics and advantages of the present invention will become more apparent from the following detailed description of the preferred embodiments with reference to the attached drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1A to FIG. 1E are cross-sectional views of a main portion of a conventional fluid pump.

FIG. 2 is a cross-sectional view of a main portion of a fluid pump **901** according to a comparative example of the present invention.

FIG. 3 is an external perspective view of a piezoelectric pump 101 according to a first preferred embodiment of the present invention.

FIG. 4 is an exploded perspective view of the piezoelectric pump 101 as shown in FIG. 3.

FIG. **5** is a cross-sectional view of the piezoelectric pump **101** as shown in FIG. **3** taken along line T-T.

FIG. 6 is an external perspective view of a vibrating plate unit 160 as shown in FIG. 4.

FIG. 7 is a plan view of a bonding body of the vibrating plate unit 160 and a flexible plate 151 as shown in FIG. 4.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

Hereinafter, a piezoelectric pump **101** will be described according to a first preferred embodiment of the present invention.

FIG. **3** is an external perspective view of the piezoelectric pump **101** according to the first preferred embodiment of the

present invention. FIG. **4** is an exploded perspective view of the piezoelectric pump **101** as shown in FIG. **3**. FIG. **5** is a cross-sectional view of the piezoelectric pump **101** as shown in FIG. **3** taken along line T-T. FIG. **6** is an external perspective view of a vibrating plate unit **160** as shown in 5 FIG. **4** as viewed from a flexible plate **151**.

As shown in FIG. 3 to FIG. 5, the piezoelectric pump 101 preferably includes a cover plate 195, a base plate 191, a flexible plate 151, a vibrating plate unit 160, a piezoelectric element 142, a spacer 135, an electrode conducting plate 10 170, a spacer 130, and a lid portion 110. The piezoelectric pump 101 is provided with a structure in which the above components are layered in that order.

A vibrating plate **141** includes an upper surface facing the lid portion **110**, and a lower surface facing the flexible plate 15 **151**.

The piezoelectric element 142 is adhesively fixed to the upper surface of the vibrating plate 141. The upper surface of the vibrating plate 141 is equivalent to the "first main surface" according to a preferred embodiment of the present 20 invention. Both the vibrating plate 141 and the piezoelectric element 142 preferably are disc shaped. In addition, the vibrating plate 141 and the piezoelectric element 142 define a disc shaped actuator 140. The vibrating plate unit 160 that includes the vibrating plate 141 is preferably formed of a 25 metal material which has a coefficient of linear expansion greater than the coefficient of linear expansion of the piezoelectric element 142. By applying heat to cure the vibrating plate 141 and the piezoelectric element 142 at time of adhesion, an appropriate compressive stress can be left on 30 the piezoelectric element 142 which allows the vibrating plate 141 to bend and form a convex curve on the side of the piezoelectric element 142. This compressive stress can prevent the piezoelectric element 142 from cracking. For example, it is preferred for the vibrating plate unit 160 to be 35 formed of SUS430. For example, the piezoelectric element 142 may be made of lead titanate zirconate-based ceramics. The coefficient of linear expansion for the piezoelectric element 142 is nearly zero, and the coefficient of linear expansion for SUS430 is about $10.4 \times 10^{-6} \text{ K}^{-1}$.

It should be noted that the piezoelectric element **142** is equivalent to the "driver" according to a preferred embodiment of the present invention.

The thickness of the spacer **135** may preferably be the same as, or slightly thicker than, the thickness of the 45 piezoelectric element **142**.

The vibrating plate unit 160, as shown in FIG. 4 to FIG. 6, preferably includes the vibrating plate 141, the frame plate 161, and a link portion 162. The vibrating plate unit 160 is preferably integrally formed by etching a metal plate, 50 for example. The vibrating plate 141 has the frame plate 161 provided therearound. The vibrating plate 141 is linked to the frame plate 161 by the link portion 162. Additionally, the frame plate 161 is fixed to the flexible plate 151 preferably by the adhesive agent. 55

As shown in FIG. 5 and FIG. 6, the vibrating plate 141 and the link portion 162 preferably have a thickness that is thinner than the thickness of the frame plate 161 so that surfaces at the flexible plate 151 side of the vibrating plate 141 and the link portion 162 may separate from the flexible 60 plate 151. The vibrating plate 141 and the link portion 162 are preferably made thinner than the thickness of the frame plate 161 by half etching the surface of the vibrating plate 141 and of the link portion 162 on the side of the flexible plate 151. Accordingly, a distance between the vibrating 65 plate 141 and the link portion 162, and the flexible plate 151 is accurately determined to a predetermined size (15 µm, for 6

example) by the depth of the half etching. The link portion **162** has an elastic structure having the elasticity of a small spring constant.

Therefore, the vibrating plate 141 is flexibly and elastically supported preferably at three points against the frame plate 161 by three link portions 162, for example. For this reason, the bending vibration of the vibrating plate 141 cannot be blocked at all. In other words, the piezoelectric pump 101 has a structure in which the peripheral portion of the actuator 140 (as well as the central part) is not substantially fixed.

It is to be noted that the flexible plate 151, an adhesive agent layer 120, the frame plate 161, the spacer 135, the electrode conducting plate 170, the spacer 130, and the lid portion 110 constitute a pump housing 180. Additionally, the interior space of the pump housing 180 is equivalent to a pump chamber 145.

The spacer 135 is adhesively fixed to an upper surface of the frame plate 161. The spacer 135 is preferably made of resin. The thickness of the spacer 135 is the same as or slightly thicker than the thickness of the piezoelectric element 142. Additionally, the spacer 135 constitutes a portion of the pump housing 180. Moreover the spacer 135 electrically insulates the electrode conducting plate 170, described below, with the vibrating plate unit 160.

The electrode conducting plate **170** is adhesively fixed to an upper surface of the spacer **135**. The electrode conducting plate **170** is preferably made of metal. The electrode conducting plate **170** includes a frame portion **171** which is a nearly circular opening, an inner terminal **173** which projects into the opening, and an external terminal **172** which projects to the outside.

The leading edge of the inner terminal **173** is soldered to the surface of the piezoelectric element **142**. The vibration of the inner terminal **173** can be significantly reduced and prevented by setting a soldering position to a position equivalent to a node of the bending vibration of the actuator **140**.

The spacer 130 is adhesively fixed to an upper surface of 40 the electrode conducting plate 170. The spacer 130 preferably is made of resin. The spacer 130 is a spacer that prevents the soldered portion of the inner terminal 173 from contacting the lid portion 110 when the actuator 140 vibrates. The spacer also prevents the surface of the piezo-45 electric element 142 from coming too close to the lid portion 110, thus preventing the amplitude of vibration from reducing due to air resistance. For this reason, the thickness of the spacer 130 may be equivalent to the thickness of the piezoelectric element 142.

The lid portion **110** with a discharge hole **111** formed thereon is bonded to an upper surface of the spacer **130**. The lid portion **110** covers the upper portion of the actuator **140**. Therefore, air sucked through a ventilation hole **152**, to be described below, of the flexible plate **151** is discharged from the discharge hole **111**.

Here, the discharge hole **111** is a discharge hole which releases positive pressure in the pump housing **180** which includes the lid portion **110**. Therefore, the discharge hole **111** need not necessarily be provided in the center of lid portion **110**.

An external terminal **153** is arranged on the flexible plate **151** to connect electrically. In addition, a ventilation hole **152** is formed in the center of the flexible plate **151**.

On a lower surface of the flexible plate **151**, the base plate **191** is attached preferably by the adhesive agent. A cylindrical opening **192** is formed in the center of the base plate **191**. A portion of the flexible plate **151** is exposed to the base

plate 191 at the opening 192 of the base plate 191. The circularly exposed portion of the flexible plate 151 can vibrate at a frequency substantially the same as a frequency of the actuator 140 through the fluctuation of air pressure accompanying the vibration of the actuator 140. In another 5 words, by the configuration of the flexible plate 151 and the base plate 191, a portion of the flexible plate 151 facing the opening 192 serves as the circular movable portion 154 capable of bending and vibrating. The movable portion 154 corresponds to a portion in the center or near the center of 10 the region facing the actuator 140 of the flexible plate 151. Furthermore, a portion positioned outside the movable portion 154 of the flexible plate 151 serves as the fixing portion 155 that is fixed to the base plate 191. The characteristic frequency of the movable portion 154 is designed to be the 15 same as or slightly lower than the driving frequency of the actuator 140.

Accordingly, in response to the vibration of the actuator **140**, the movable portion **154** of the flexible plate **151** also vibrates with large amplitude, centering on the ventilation 20 hole **152**. If the vibration phase of the flexible plate **151** is a vibration phase delayed (for example, 90 degrees delayed) from the vibration of the actuator **140**, the thickness variation of a gap between the flexible plate **151** and the actuator **140** increases substantially. As a result, the piezoelectric 25 pump **101** improves pump performance (the discharge pressure and the discharge flow rate).

The cover plate 195 is bonded to a lower surface of the base plate 191. Three suction holes 197 are provided in the cover plate 195. The suction holes 197 communicate with 30 the opening 192 through a passage 193 formed in the base plate 191.

The flexible plate 151, the base plate 191, and the cover plate 195 are preferably made of a material having a coefficient of linear expansion greater than a coefficient of 35 linear expansion of the vibrating plate unit 160. In addition, the flexible plate 151, the base plate 191, and the cover plate 195 are preferably made of a material having approximately the same coefficient of linear expansion. For example, it is preferable to have the flexible plate 151 that is made of 40 substances such as beryllium copper. It is preferable to have the base plate 191 that is made of substances such as phosphor bronze. It is preferable to have the cover plate 195 that is made of substances such as copper. These coefficients of linear expansion are approximately 17×10⁻⁶ K⁻¹. More- 45 over, it is preferable to have the vibrating plate unit 160 that is made of SUS430. The coefficient of linear expansion of SUS430 is about $10.4 \times 10^{-6} \text{ K}^{-1}$.

In this case, due to the differences in the coefficients of linear expansion of the flexible plate 151, the base plate 191, 50 and the cover plate 195 in relation to the frame plate 161, by applying heat to cure the flexible plate 151 at time of adhesion, a tension which makes the flexible plate 151 bend and form a convex curve on the side of the piezoelectric element 142, is applied to the flexible plate 151. Thus, a 55 tension which makes the movable portion capable of bending and vibrating is adjusted on the movable portion 154. Furthermore, the vibration of the movable portion 154 is not blocked due to any slack on the movable portion 154. It is to be understood that since the beryllium copper which 60 constitutes the flexible plate 151 is a spring material, even if the circular movable portion 154 vibrates with large amplitude, there will be no permanent set-in fatigue or similar symptoms. In another words, beryllium copper has excellent durability.

In the above structure, when a driving voltage is applied to the external terminals **153**, **172**, the actuator **140** of the

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piezoelectric pump 101 concentrically bends and vibrates. Furthermore, in the piezoelectric pump 101, the movable portion 154 of the flexible plate 151 vibrates from the vibration of the vibrating plate 141. Thus, the piezoelectric pump 101 sucks air from the suction hole 197 to the pump chamber 145 through the ventilation hole 152. Then, the piezoelectric pump 101 discharges the air in the pump chamber 145 from the discharge hole 111. In this state of the piezoelectric pump 101, the peripheral portion of the vibrating plate 141 is not substantially fixed. For that reason, the piezoelectric pump 101 has less loss caused by the vibration of the vibrating plate 141, while being small and low profile, and can obtain a high discharge pressure and a large discharge flow rate.

In addition, in the piezoelectric pump **101**, the surface of the link portion **162** on the side of the flexible plate **151** is separated from the flexible plate **151**. Therefore, the piezoelectric pump **101** can prevent the link portion **162** and the flexible plate **151** from adhering to each other even if the excess of the adhesive agent flows into a gap between the link portion **162** and the flexible plate **151**.

Similarly, in the piezoelectric pump 101, the lower surface of the vibrating plate 141 on the side of the flexible plate 151 is separated from flexible plate 151. For that reason, the piezoelectric pump 101 can prevent the vibrating plate 141 and the flexible plate 151 from adhering to each other even if the excess of the adhesive agent flows into a gap between the vibrating plate 141 and the flexible plate 151. Here, the lower surface of the vibrating plate 141 is equivalent to the "second main surface" according to a preferred embodiment of the present invention.

Thus, the piezoelectric pump 101 can prevent the vibrating plate 141 and the link portion 162 and the flexible plate 151 from adhering to each other and blocking the vibration of the vibrating plate 141.

Additionally, in the piezoelectric pump **101**, a difference between the thickness of the vibrating plate **141** and the thickness of the frame plate **161** is equivalent to a distance between the vibrating plate **141** and the flexible plate **151**. In another words, in the piezoelectric pump **101**, the distance that affects the pressure-flow rate characteristics is determined by the depth of the half etching to the vibrating plate **141**.

It is possible for precise setting of the depth of this half etching. Thus, the piezoelectric pump **101** prevents the pressure-flow rate characteristics from varying with each piezoelectric pump **101**.

As described above, the piezoelectric pump 101 prevents vibration of the vibrating plate 141 from being blocked by the adhesive agent and prevents fluctuations in the pressure-flow rate characteristics.

Both the actuator 140 and the flexible plate 151 bend and form convex curves on the side of the piezoelectric element 142 at normal temperature by approximately the same amount. Here, when a temperature of the piezoelectric pump 101 rises by generation of heat at the time of driving the piezoelectric pump 101, or when an environmental temperature rises, a warp of the actuator 140 and the flexible plate 151 decreases, and both the actuator 140 and the flexible plate 151 deform in parallel by approximately the same amount. In another words, a distance between the vibrating plate 141 and the flexible plate 151 does not change in temperature. Additionally, the distance is determined by the depth of the half etching to the vibrating plate 141 as mentioned above.

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Consequently, the piezoelectric pump **101** can maintain proper pressure-flow rate characteristics of a pump over a wide temperature range.

FIG. 7 is a plan view of a bonding body of the vibrating plate unit 160 and the flexible plate 151 as shown in FIG. 4. 5

As shown in FIG. 4 to FIG. 7, it is preferable that a hole portion **198** is provided in the region facing the link portion **162** in the flexible plate **151** and the base plate **191**. Thus, when the frame plate **161** and the flexible plate **151** are fixed preferably by the adhesive agent, the excess of the adhesive 10 agent flows into the hole portion **198**.

Thus, the piezoelectric pump 101 prevents the vibrating plate 141 and the link portion 162 and the flexible plate 151 from adhering to each other and blocking the vibration of the vibrating plate 141.

Other Preferred Embodiments

While the actuator **140** having a unimorph type structure and undergoing bending vibration was provided in the above mentioned preferred embodiments, the structure is not limited thereto. For example, it is possible to attach a piezo- 20 electric element **142** on both sides of the vibrating plate **141** so as to have a bimorph type structure and undergo bending vibration.

Moreover, in the above described preferred embodiments, while the actuator **140** which undergoes bending vibration 25 due to expansion and contraction of the piezoelectric element **142** was provided, the method is not limited thereto. For example, an actuator which electromagnetically undergoes bending vibration may be provided.

In the preferred embodiments of the present invention 30 described above, while the piezoelectric element **142** is preferably made of lead titanate zirconate-based ceramics, the material is not limited thereto. For example, an actuator may be made of a piezoelectric material of non-lead based piezoelectric ceramics such as potassium-sodium niobate 35 based or alkali niobate based ceramics.

Additionally, while the above described preferred embodiments of the present invention showed an example in which the piezoelectric element **142** and the vibrating plate **141** preferably have roughly the same size, there are no 40 limitations to the size. For example, the vibrating plate **141** may be larger than the piezoelectric element **142**.

Moreover, although the disc shaped piezoelectric element **142** and the disc shaped vibrating plate **141** were preferably used in the above mentioned preferred embodiments, there 45 are no limitations to the shape. For example, either of the piezoelectric element **142** or the vibrating plate **141** can be a rectangle or a polygon.

In addition, while a thickness of the entire vibrating plate **141** is preferably thinner than the thickness of the frame 50 plate **161**, there are no limitations to the thickness. For example, the thickness of at least a portion of the vibrating plate **141** may be thinner than the thickness of the frame plate **161**. However, a portion of the vibrating plate **141** is preferred to be an end of the vibrating plate, of the entire 55 vibrating plate **141**, nearest to an adhesion portion between the flexible plate **151** and the frame plate **161**.

Additionally, in the above described preferred embodiments, while the link portion **162** is preferably provided at three spots, the number of places is not limited thereto. For 60 example, the link portion **162** may be provided at only two spots or the link portion **162** may be provided at four or more spots. Although the link portion **162** does not block vibration of the actuator **140**, the link portion **162** does more or less affect the vibration of the actuator **140**. Therefore, the 65 actuator **140** can be held naturally by linking (holding) the actuator at three spots, for example, and the position of the

actuator **140** is held accurately. The piezoelectric element **142** can also be prevented from cracking.

In addition, the actuator **140** may be driven in an audible frequency band in various preferred embodiments of the present invention if it is used in an application in which the generation of audible sounds does not cause problems.

Moreover, while the above described preferred embodiments show an example in which one ventilation hole **152** is preferably disposed at the center of a region facing the actuator **140** of the flexible plate **151**, there are no limitations to the number of holes. For example, a plurality of holes may be disposed near the center of the region facing the actuator **140**.

Further, while the frequency of driving voltage in the above mentioned preferred embodiments is determined so as to make the actuator **140** vibrate in a primary mode, there are no limitations to the mode. For example, the driving voltage frequency may be determined so as to vibrate the actuator **140** in other modes such as a tertiary mode.

In addition, while air is preferably used as fluid in the above mentioned preferred embodiments, the fluid is not limited thereto. For example, any kind of fluid such as liquids, gas-liquid mixture, solid-liquid mixture, and solidgas mixture can be applied to the above preferred embodiments.

Finally, the above described preferred embodiments are to be considered in all respects as illustrative and not restrictive. The scope of the present invention is defined not by above described preferred embodiments but by the claims. Further, the scope of the present invention is intended to include all modifications that come within the meaning and scope of the claims and any equivalents thereof.

What is claimed is:

1. A fluid control device comprising:

- a vibrating plate unit including:
 - a vibrating plate that includes a first main surface and a second main surface;
 - a frame plate that surrounds the vibrating plate with a gap between the frame plate and the vibrating plate; and
 - a link portion that links the vibrating plate and the frame plate and connects a portion of the vibrating plate and the frame plate;
- a driver that is provided on the first main surface, and vibrates the vibrating plate; and
- a flexible plate that includes a hole portion formed in a region in which the flexible plate faces the link portion, faces the second main surface of the vibrating plate, and is fixed to the frame plate.

2. The fluid control device according to claim **1**, wherein at least a portion of the vibrating plate and the link portion are thinner than a thickness of the frame plate so that the portion of the vibrating plate and the link portion are separate from the flexible plate.

3. The fluid control device according to claim **1**, wherein the vibrating plate unit is an integral unit.

4. The fluid control device according to claim **1**, wherein at least the portion of the vibrating plate and the link portion are made thinner than the frame plate.

5. The fluid control device according to claim **1**, wherein the portion of the vibrating plate is formed in an end of the vibrating plate nearest to an adhesion portion between the flexible plate and the frame plate.

6. The fluid control device according to claim 1, wherein the vibrating plate and the driver constitute an actuator and the actuator is disc shaped.

7. The fluid control device according to claim 1, wherein the flexible plate comprises:

- a movable portion that is positioned in a center or in an area of the center of a region in which the flexible plate faces the vibrating plate and is arranged to bend and 5 vibrate; and
- a fixing portion that is positioned in an area outside the movable portion of the flexible plate and is substantially fixed.

8. The fluid control device according to claim **1**, further 10 comprising a plurality of link portions.

9. The fluid control device according to claim **1**, wherein the link portion comprises:

- an extending portion that extends along the gap;
- a first linking portion that links the extending portion and 15 the vibrating plate; and
- a second linking portion that links the extending portion and the frame plate, and
- a position in which the first linking portion and the vibrating plate are connected to each other is different 20 from a position in which the second linking portion and the frame plate are connected to each other, in a direction in which the extending portion extends.

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