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#### (54) MULTI-FUNCTIONED OPTICAL USPC .................................. 356/491,495, 503, 511 MEASUREMENT DEVICE AND METHOD FOR OPTICALLY MEASURING A PLURALITY OF PARAMETERS

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#### (57) ABSTRACT

The conventional white-light interferometer, confocal micro scope, and ellipsometer are integrated as one device set in a functional sense, and the geometrical parameters convention ally measured may be deduced on the integrated device. Thus, the advantages and efficacies of equipment cost saving, on line measuring, rapid monitoring, reduced manufacturing time, and reduced possibility of object damage during the manufacturing process may be secured, compared with the prior art.

#### 16 Claims, 5 Drawing Sheets











FIG. 3B



FIG. 3C

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## MULT-FUNCTIONED OPTICAL MEASUREMENT DEVICE AND METHOD FOR OPTICALLY MEASURING A PLURALITY OF PARAMETERS

#### BACKGROUND OF RELATED ART

#### 1. Technical Field

The present invention relates to an optically measurement device and an optically measuring method, and particularly to a multi-functioned optically measurement device for measur ing a plurality of parameters of an object and a method for optically measuring a plurality of parameters of an object, the parameters may be a surface profile, a gray-level image and a <sub>15</sub> full focal colorful image, and a thin-film thickness.

2. Related Art

With rapid improvement of various micro-level manufac turing technologies in the industry, there is an increasing demand on measurement of such micro-level devices. The 20 various 3D contour measuring technologies used in the prior art can not satisfy with the general requirement any more.

In the semiconductor, flat displays, and micro-electrome chanical devices and electronic package fields, since there is a crucial effect of the precision and mechanical property of 25 the surface profile of the micro-structure surface on the prod uct's efficacy and lifetime, the quality presented on the manu facturing process has to be monitored. Hence, there is quite a need to accurately measure the surface profile of the microstructure, and which is typically done by some optical instru- 30 ments together with some optical technologies.

How the interferometry, confocal microscopy and ellip sometry functions are performed by the white-light interfer ometer, microscope, and ellipsometer have been readily known by those persons skilled in the art. They may each 35 deduce a corresponding parameter of a measured object by its optical measurement for monitoring the on-line manufac tured semiconductor products.

The interferometer for surface profile measurement of the object is implemented into an optical path. There are three 40 type of interferometers: Mirau, Linnik, and Michelson. For the Mirau and Michelson types, their reference surface is integrated into an object lens and not adjustable. On the other hand, the optical architecture of the Linnik type enables its reference optical-path and optical system to be adjustable and 45 flexible, and which may be manual operated by the user.

A typical commercial confocal microscope may be used to first vertically scanning the measured object and assembling the Scanned images together with an image processing, to 50 obtain a high frequency information for each of the pixels in the scanned image, so that a depth-of-focus gray level of each of the pixels is deduced and thus the whole-field information is secured.

erally adopted, in which a linear polarized light is first formed by polarizing a light source, and then adjusted for its phase through a compensation plate. Then, the formed light is inci dent onto an object having a thin film thereon and then reflected back onto a second polarization plate, an analyzer, 60 and compensated therein. And, a detector is used to record the reflected light and analyze the associated Stokes parameter, and the amplitude and the phase of the reflected light, thereby reversely deducing a thickness information of the thin film. To measure a thin-film thickness, the ellipsometer is gen- 55

However, the currently available interferometer, confocal 65 microscope and ellipsometer each only have one single mea surement function. And, so far, the efforts on these instru-

ments have been mostly only made for enhanced precision and stability of their measurement algorithms.

In measuring a bulk dimension, a public US patent application, US2013/0033698 A1, disclosed such a method by reflecting two light beams from the front and rare surface of the measured object, detecting a spectrum of the light beams reflected from the front and rare surface of the measured object, respectively, and utilizing a processor to analyze a thickness value between the two faces.

A public US patent application, US2012/0218561 A1, dis closed a method for deducing a bulk dimension by measuring a time difference between light beams are reflected from the using a spectrometer or a light detector, i.e. the time difference between the time when a surface reflected light and an interface reflected light are respectively received, and then deducing the bulk dimension by using a computer.

U.S. Pat. No. 8,416.491 B2, disclosed a method capable of employing the confocal microscopy principle, where a series of strip structured light beams are propagating from a light source to explore a depth response curve, so as to secure a depth distribution within a measuring range of the object and thus the surface profile of the measured object may be reversely deduced.

U.S. Pat. No. 8,416,399 B2, disclosed a method for mea suring the surface profile and the thickness of the measured object by using a white-light interferometry method and a reverse measurement method.

TW patent, TW096147071, disclosed a method for obtaining a three dimensional contour of a measured object by receiving R, G and B interference signal spectra by using an off-axis digital full color method, and finally calculating three colors, R, G and B, information and phases by using a com puter calculation.

However, since the semiconductor industry has a trend to seek a higher integration solution for its manufacturing to achieve a reduced manufacturing time and systematic perfor mance, to further save its manufacturing cost and simplified process flow, the currently used optical measurement devices<br>have a need to be further reduced in its cost and processing time when parameters measurement of the measured object is considered. Moreover, the object stands some possibility of damage when it is moved for the parameters measurement Therefore, how may the optical measurement achieves in an on-line performance becomes an issue to be overcome in the micro-level industries. Such as the semiconductor industry.

In view of the above prior arts, it may be known that the optical measurement instruments has a need to get more on-line measuring, rapid monitoring, reduced manufacturing time, and reduced possibility of object damage during the product manufacturing process may be achieved to facilitate industry improvement.

#### **SUMMARY**

It is, therefore, an object of the present invention to provide a multi-functioned optical measurement device for measur ing a plurality of parameters of an object and a method for measuring a plurality of parameters to provide a multi-param eter measurement.

In accordance with the present invention, the multi-func tioned optical measurement device for measuring a plurality of parameters of an object comprises a light source unit, comprising an external light Source; a collimation unit, cou pling the external light source to provide a collimated refer  $\mathcal{L}_{\mathcal{L}}$ 

ence light and a collimated subject light; and a polarizer unit, polarizing the collimated reference light and the collimated ized subject light, the polarized reference light propagating on a propagating path; an aperture unit, comprising a refer ence light aperture, controlling a light flux of the polarized reference light, having an open and close states, and closing the propagating path of the polarized reference light when the close State is acted; an incident light aperture, controlling a light flux of the polarized subject light; and a measured light 10 aperture; a light splitting unit, diving the polarized light into the reference light and the polarized subject light and cou pling the reference light and the polarized subject light onto a first path and a second path, respectively; a measured end unit, locating on the second path, receiving and focusing the 15 polarized subject light to the measured object, the measured object reflecting the polarized subject light passing the light splitting unit to generate a measured light, the measured light being reflected onto a third path reverse to the second path; a reference light processing unit, locating on the first path, and reflecting the polarized reference light to generate a colli mated effect reference light onto the third path when the reference light aperture is at the open state and the optical measurement device is on an interferometer mode and the jointly generate an interference image through the light-splitting unit, and generating a guided measured image on the third path when the reference light aperture is at the close state and the optical measurement device is on a microscope mode; a spectrum obtaining/image acquiring unit, comprising a 30 polarized light splitting unit, guiding the interference image on the interferometer mode and guiding the measured image<br>on the microscope mode to obtain a first to-be-analyzed image and a second to-be-analyzed image; a spectrum obtaining unit, receiving the first to-be-analyzed image to generate 35 a spectrum data; and an image acquiring unit, receiving the second to-be-analyzed image; and a control-processing unit, performing steps of controlling the measured object to move along a vertical direction on the interferometer mode, and analyzing the second to-be-analyzed image, thereby securing 40 a zero optical path difference for each of a plurality of pixels in the second to-be-analyzed image and recording the Zero optical path difference for each of the plurality of pixels in the second to-be-analyzed image, thereby enabling the spectrum obtaining unit to obtain the spectrum data, thereby calculating 45 a surface topography of the measured object according to at least one of the spectrum data and the second to-be-analyzed image; closing the reference light aperture to enable the optical measurement device to enter the microscope mode, cal measurement device to enter the microscope mode, enabling the spectrum obtaining unit to obtain the spectrum 50 data when the Zero optical path difference exists, activating the measured object to move along the vertical direction, analyzing a focal information of each of the plurality of pixels in the second to-be-analyzed image to obtain a full focal colorful image and a full focal gray-level image, and estab 55 lishing a depth response curve; activating the measured object<br>to move laterally, to obtain a large-range surface profile according to the spectrum data, the depth response curve and an axial dispersion extent; and deducing a thin-film thickness and an another surface profile according to the spectrum data 60 when the zero optical path difference face exists, when the measured object is a substrate having a coating layer thereon, wherein the surface profile is the another surface profile and the control-processing unit selects to only calculate and present one of the surface profile and the another surface 65 profile. In accordance with the present invention, the method for optically measuring a plurality of parameters of an object measured light and the collimated effect reference light 25

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comprises steps of (a) providing a collimated reference light and a collimated subject light; (b) polarizing the collimated reference light and the collimated Subject light, to obtain a polarized reference light and a polarized Subject light, the polarized reference light having a propagating path; (c) con trolling a light flux of the polarized reference light, having an open and close states, and closing the propagating path of the polarized reference light when the close state is acted; (d) controlling a light flux of the polarized subject light;  $(e)$ diving the polarized light into the reference light and the polarized subject light and coupling the reference light and<br>the polarized subject light onto a first path and a second path, respectively; (f) receiving and focusing the polarized subject light to the measured object, the measured object reflecting the polarized subject light passing the light-splitting unit to generate a measured light, the measured light being reflected onto a third path reverse to the second path; (g) reflecting the polarized reference light to generate a collimated effect ref erence light onto the third path when the reference light aperture is at the open state and the optical measurement device is on an interferometer mode and the measured light and the collimated effect reference light jointly generate an interference image and generating a guided measured image on the third path when the reference light aperture is at the close state and the optical measurement device is on a micro scope mode; (h) guiding the interference image on the interferometer mode and guiding the measured image on the microscope mode to obtain a first to-be-analyzed image and a second to-be-analyzed image: (i) receiving the first to-be analyzed image to generate a spectrum data and receiving the second to-be-analyzed image: (i) controlling the measured object to move along avertical direction on the interferometer mode, and analyzing the second to-be-analyzed image, thereby securing a zero optical path difference for each of a plurality of pixels in the second to-be-analyzed image and recording the Zero optical path difference for each of the plurality of pixels in the second to-be-analyzed image, thereby enabling the spectrum obtaining unit to obtain the spectrum data, thereby calculating a surface topography of the measured object according to at least one of the spectrum data and the second to-be-analyzed image; (k) closing the reference light aperture to enable the optical measurement device to enter the microscope mode, enabling the spectrum obtaining unit to obtain the spectrum data when the Zero optical path difference exists; (1) activating the measured object to move along the vertical direction, analyzing a focal information of each of the plurality of pixels in the second to-be-analyzed image to obtain a full focal colorful image and a full focal gray-level image, and establishing a depth response curve; (m) activating the measured object to move laterally, to obtain a large-range surface profile according to the spectrum data, the depth response curve and an axial dispersion extent; and (n) deducing a thin-film thickness and an another surface profile according to the spectrum data when the Zero optical path difference face exists, when the measured object is a substrate having a coating layer thereon, wherein the surface profile is the another surface profile and the control-processing unit selects to only calculate and present one of the surface profile and the another surface profile.

By means of the optical measurement device and method of the present invention, since the traditional white-light interferometer, confocal microscope, and ellipsometer are integrated as one device set in a functional sense, the advan tages and efficacies of equipment cost saving, on-line mea

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suring, rapid monitoring, reduced manufacturing time, and reduced possibility of object damage during the manufactur ing process may be secured.

#### BRIEF DESCRIPTION OF THE DRAWINGS

The present invention will be better understood from the following detailed descriptions of the preferred embodiments according to the present invention, taken in conjunction with the accompanying drawings, in which:

FIG. 1 is a schematic block diagram of multi-functioned optical measurement device for measuring a plurality of parameters of an object according to the present invention;

FIG. 2 is a schematic diagram of a further detailed archi tecture of the multi-functioned optical measurement device for measuring a plurality of parameters of an object according to the present invention; and

FIGS. 3A, 3B and 3C are jointly a flowchart of the method for optically measuring a plurality of parameters of an object  $_{20}$ according to the present invention.

#### DETAILED DESCRIPTION

The present invention will be apparent from the following  $25$ detailed description, which proceeds with reference to the accompanying drawings, wherein the same references relate to the same elements.

The present invention sets forth a multi-functioned optical measurement device for a plurality of parameters of an object 30 and a method for optically measuring a plurality of param eters of an object. At first, FIG. 1 and FIG. 2 are used to described the optical measurement device part of the present invention, in which FIG. 1 is a schematic block diagram of a of parameters of an object according to the present invention, and FIG. 2 is a schematic diagram of a further detailed archi tecture of the multi-functioned optical measurement device for a plurality of parameters of an object according to the present invention. multi-functioned optical measurement device for a plurality 35 40

As shown, the optical measurement device 100 comprises a light source unit 101, an aperture unit 120, a beam splitting unit 103, a measured object unit 104, a reference light processing unit 105, a polarization and splitting unit 106, a spectrum obtaining/image acquiring unit  $107$ , and a signal pro-  $45$ cessing unit 107. The optical measurement device 100 is used to measure geometrical parameters of a measured object A, where the measured object A is an object having a substrate with a coating layer thereon, and typically a micro-device such as a semiconductor device.

The light source unit 101 comprises an external light source 101*a*, a collimation unit 101*b*, and a polarization unit 101c. The external light source 101 may be a white-light halogen lamp or an infrared lamp, and has a Gaussian inten sity distribution. The polarization unit  $101c$  receives the 55 external light source  $101a$  for providing a collimated reference light R1 and a collimated subject light I1. The polariza tion unit  $101c$  is used to polarize the collimated reference light R1 and the collimated subject light I1, to obtain a polarized reference light R2 and a polarized subject light I2.

The aperture unit 102 comprises a reference light aperture 102 $a$ , an incident light aperture 102 $b$ , and a measured light aperture  $102c$ . The reference light aperture  $102a$  controls a passing amount of the polarized reference light R2 and has an open and close states. Further, when the close state exists, the 65 reference light aperture 102a closes the propagating path of the polarized reference light R2.

The incident light aperture  $102b$  controls a passing amount of the polarized subject light I2. In addition, the measured light aperture  $102c$  will be explained in the following.

The light splitting unit 103 guides the polarized reference light R2 and the polarized subject light I2 onto a first path P1 and a second path P2.<br>The measured end unit 104 is located on the second path

P2, and receives and focuses the polarized subject light I2 passing the light splitting unit 103 to the measured object A.<br>Then, the measured object A reflects the polarized subject light I2 passing the light-splitting unit 103 to generate a measured light M1, wherein the measured light M1 is reflected onto a third path P3 reverse to the second path P2.

The reference light processing unit 105 is located on the first path P1, and when the reference light aperture  $102a$  is at the open state and the optical measurement device 100 is on an interference mode, it reflects the polarized reference light R2 to generate a collimated effect reference light R3 onto the third path P3. The measured light M1 and the collimated effect reference light R3 jointly generate an interference image through the light-splitting unit 103. The interferometer mode refers to a state when the optical measurement device 100 operates at this time. When the reference light aperture  $102a$  is at the close state and the optical measurement device 100 is on a microscope mode, a guided measured image M2 is generated on the third path P3.

The spectrum obtaining/image acquiring unit 106 com prises a polarized light splitting unit  $106a$ , a spectrum obtaining unit 106a and an image acquiring unit 106.

On the interference mode, the polarized light splitting unit 106a receives the interference image and; on the other hand, receives the measured image on the microscope mode to obtain a first to-be-analyzed image and a second to-be-ana lyzed image. The spectrum obtaining unit 106a receives the first to-be-analyzed image to generate a spectrum message. The image acquiring unit 106*b* receives the second to-beanalyzed image for use of subsequent analysis processing, so that a relationship between the second-to-be-analyzed image and the measured object A may be used to deduce some geometrical parameters of the measured object A.

The signal processing unit 107 is used to analyze and calculate several geometrical parameters of the measured object A. On the interference mode, the signal processing unit 107 controls the measured object A to move along a vertical direction V, and analyzes the second to-be-analyzed image, thereby securing a zero optical path difference for each of a plurality of pixels in the second to-be-analyzed image and rality of pixels in the second to-be-analyzed image, thereby enabling the spectrum obtaining unit  $106a$  to obtain the spectrum message, thereby calculating a Surface topography of the measured object A according to the spectrum message or the second to-be-analyzed image.

60 focal information of each of the plurality of pixels in the Further, the signal processing unit 107 closes the reference light aperture  $102a$  to enable the optical measurement device 100 to enter the microscope mode, enabling the spectrum obtaining unit  $106a$  to obtain a spectrum message when the Zero optical path difference exists, activates the measured object A to move along the vertical direction V, analyzes a second to-be-analyzed image to obtain a full focal colorful image and a full focal gray-level image, and establishing a depth response curve.

Thereafter, the signal processing unit 107 further activates the measured object A to move laterally, to obtain a large range surface profile according to the spectrum message, the depth response curve and a axial dispersion phenomenon.

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Finally, when the Zero optical path difference face exists, a bulk dimension and an another Surface profile are deduced according to the spectrum message, wherein the Surface pro file is the another surface profile and the signal processing unit 107 selects to only calculate and present one of the <sup>5</sup> surface profile and the another surface profile.

In the following, the optical measurement device 100 will be described for its more details in some preferred embodi ments.

The reference light processing unit 104 further comprises an optical path difference precision shift mechanism 104a and a reference light reflector precision shift mechanism 104*b*. The mechanism 104*a* adjusts the collimated effect reference light to have a zero optical path difference with respect  $_{15}$ to the measured light, while the mechanism 104b adjusts a contrast of a plurality of interference strips in the interference image.

The polarized light splitting unit  $106a$  further comprises an adjustment splitting angle rotational platform (not shown), for adjusting an image definition of the plurality of strips in the interference image.

The optical measurement device 100 of the present inven tion further comprises a measure object Supporting mecha nism 108, which comprises a piezoelectric activator 108a and 25 an precision shift platform 108b, used for supporting the piezoelectric activator  $108a$ . In the mechanism 10, the piezo-electric activator  $108a$  is controlled by the signal processing unit 107 to move the measured object A along the vertical direction V on the interference mode, while the precision shift 30 platform 108b is used to support the piezoelectric activator 108a.

The signal processing unit 1207 activates the measured object A to move along the vertical direction V on the micro Scope mode, analyzes a high frequency information of each of 35 the plurality of pixels in the second measured image, match ing a depth of field gray value of each of the plurality of pixels, restoring an image out-focal information to form the full focal colorful image and the full focal gray-level image, and estab lishing the depth response curve.

The signal processing unit 107 restores the image out-focal information to deduce the full focal gray-level image by using an image contrast filtering method and analyzed high fre quency information of each of the plurality of pixels in the second measured image. Furthermore, the to-be-analyzed 45 image is divided into three colors R, G and B images, and the three colors R, G and B images are then analyzed and over lapped to restore the full focal colorful image.

On the microscope mode, the spectrum obtaining unit 106 acquires a spectrum message of an upper surface of the sub- 50 strate and an upper face of the coating layer, respectively, and reversely deduces a distance between the upper surface of the substrate and the upper face of the coating layer of the measured object A and serving the distance as a thickness of the coating layer.

The image acquiring unit  $106b$  and the spectrum obtaining unit  $106b$  are capable of detecting a visible light or a non-visible light.

The signal processing unit 107 applies a phase shift algorithm onto the plurality of interference stripes and analyzes a 60 maximum strength of the plurality of interference stripes, so as to establish a surface profile information to acquire a surface profile of the measured object A.

Now, referring to FIG. 2, by which each of the units of the optical measurement device of the present invention is described with its further detailed elements accompanying with FIG. 1.

As shown, the light source unit 101 comprises a collimated light module 10 and a polarization plate 14. The collimated light module 10 comprises a doublet 11, a pinhole 12, and a focal lens 13. The polarization plate 14 comprises a polariza tion plate rotational platform 15. The reference light process ing unit 104 comprises a reference light reflector 16 and an infinite calibration object lens 17. On a midway of the mea sured light M1 to the measured object supporting unit 108 (not shown in FIG. 2, but the one comprises the piezoelectric element activation unit  $108a$  and the measured object supporting platform  $108b$ ), an infinite calibration unit 18 and a focal lens 19 are provided.

On a path between the polarized light splitting unit 106a to the spectrum obtaining unit 106b, a pinhole 20 and a focal lens 21 are provided. The polarized light splitting unit 106a further comprises a polarized light splitting unit rotational unit (not shown). On a path between the polarized light split ting unit 106*a* to the image acquiring unit 106*c*, a focal lens 22 is further comprised. Persons of the skilled arts may readily know how the detailed optical elements operate, and thus omitted herein for clarity.

By means of the above description, it may be known that the present invention is established by taking the Linnik inter ferometer as a basis, and integrating the functions provided by the conventional interferometer, microscope and ellipsom eter. Namely, the surface profile measurement of the conven analysis of the microscope, and the layer thick measurement of the ellipsometer are totally integrated in function, and thus the three dimensional geometrical parameters such as the surface profile, full focal colorful and gray-level images, large-range surface profile, and bulk dimension.

AS Such, the advantages and efficacies of equipment cost saving, on-line measuring, rapid monitoring, reduced manu facturing time, and reduced possibility of object damage dur ing the manufacturing process may be secured by the optical measurement device in the present invention, compared with the prior art.

40 explain a flowchart of the method for optically measuring a In the following, FIGS. 3A, 3B and 3C are jointly used to plurality of parameters of an object according to the present invention.

55 ence light and the polarized subject light are coupled onto a In the method of the present invention, a collimated refer ence light and a collimated subject light are first provided (S301). Next, the collimated reference light and the colli mated Subject light are used to obtain a polarized reference light and a polarized subject light (S302), wherein the polarized reference light has a propagating path. Thereafter, a light flux of the polarized reference light, having an open and close states, is controlled and the propagating path of the polarized reference light is closed when the close state is acted (S303). Subsequently, a light flux of the polarized subject light is controlled (S304). Then, the polarized light into the reference light and the polarized subject light are dived and the refer first path and a second path, respectively (S305). Next, the polarized subject light is received and focused to the measured object, wherein the measured object reflects the polarized subject light passing the light-splitting unit to generate a measured light, and the measured light is reflected onto a third path reverse to the second path; (S306). Then, the polarized reference light is reflected to generate a collimated effect reference light onto the third path when the reference light aperture is at the open state and the optical measurement device is on an interferometer mode and the measured light and the collimated effect reference light jointly generate an interference image and a guided measured image is generated

on the third path when the reference light aperture is at the close state and the optical measurement device is on a micro scope mode (S307). Thereafter, the interference image is guided on the interferometer mode and the measured image is guided on the microscope mode to obtain a first to-be-ana lyzed image and a second to-be-analyzed image (S308). Thereafter, the first to-be-analyzed image is received to gen erate a spectrum data and the second to-be-analyzed image is received (S309). Then, the measured object is controlled to and the second to-be-analyzed image is analyzed, thereby securing a zero optical path difference for each of a plurality of pixels in the second to-be-analyzed image and recording the Zero optical path difference for each of the plurality of pixels in the second to-be-analyzed image, thereby enabling 15 the spectrum obtaining unit to obtain the spectrum data, thereby calculating a surface topography of the measured object according to at least one of the spectrum data and the second to-be-analyzed image (S310). Thereafter, the refer ence light aperture is closed to enable the optical measure- 20 ment device to enter the microscope mode, enabling the spec trum obtaining unit to obtain the spectrum data when the Zero optical path difference exists (S311). Next, the measured object is activated to move along the vertical direction, a focal information of each of the plurality of pixels in the second 25 to-be-analyzed image is analyzed to obtain a full focal color ful image and a full focal gray-level image, and establishing a depth response curve (S312). Thereafter, the measured object is activated to move laterally, to obtain a large-range object is activated to move laterally, to obtain a large-range surface profile according to the spectrum data, the depth 30 response curve and an axial dispersion extent (S313). Finally, a thin-film thickness and an another surface profile are deduced according to the spectrum data when the Zero optical path difference face exists, when the measured object is a substrate having a coating layer thereon, wherein the surface 35 profile is the another surface profile and the control-process ing unit selects to only calculate and present one of the Surface profile and the another surface profile (S314). move along a vertical direction on the interferometer mode, 10

For the further detailed description for the optical measure ment method of the present invention, it may be referred to the 40 corresponding part in the above description for the optical measurement device of the present invention, and omitted herein for clarity.

As compared to the prior art methods, the optical measure ment method has its advantages and efficacies, which are 45 similar to what are described for the optical measurement device of the present invention and may be known by directly referring to the related description in the above and omitted herein for clarity.

Although the invention has been described with reference 50 to specific embodiments, this description is not meant to be construed in a limiting sense. Various modifications of the disclosed embodiments, as well as alternative embodiments, will be apparent to persons skilled in the art. It is, therefore, contemplated that the appended claims will cover all modifi- 55 cations that fall within the true scope of the invention.

#### What is claimed is:

1. An optically measurement device for measuring a plurality of parameters, comprising: 60

a light source unit, comprising:

- an external light source;
- a collimation unit, coupling the external light source to provide a collimated reference light and a collimated subject light; and 65
- a polarizer unit, polarizing the collimated reference light and the collimated Subject light, to obtain a polarized

reference light and a polarized subject light, the polar ized reference light propagating on a propagating path;

- an aperture unit, comprising a reference light aperture, controlling a light flux of the polarized reference light, having an open and close states, and closing the propa gating path of the polarized reference light when the close state is acted;
- an incident light aperture, controlling a light flux of the polarized subject light; and a measured light aperture;
- a light splitting unit, diving the polarized light into the reference light and the polarized subject light and cou pling the reference light and the polarized subject light onto a first path and a second path, respectively;
- a measured end unit, locating on the second path, receiving and focusing the polarized subject light to the measured object, the measured object reflecting the polarized sub ject light passing the light-splitting unit to generate a measured light, the measured light being reflected onto a third path reverse to the second path;
- a reference light processing unit, locating on the first path, and reflecting the polarized reference light to generate a collimated effect reference light onto the third path when the reference light aperture is at the open state and the optical measurement device is on an interferometer mode and the measured light and the collimated effect reference light jointly generate an interference image through the light-splitting unit, and generating a guided measured image on the third path when the reference light aperture is at the close state and the optical mea surement device is on a microscope mode;
- a spectrum obtaining/image acquiring unit, comprising a polarized light splitting unit, guiding the interference image on the interferometer mode and guiding the mea sured image on the microscope mode to obtain a first to-be-analyzed image and a second to-be-analyzed image;
- a spectrum obtaining unit, receiving the first to-be-ana lyzed image to generate a spectrum data; and an image acquiring unit, receiving the second to-be-analyzed image; and
- a control-processing unit, performing steps of
	- controlling the measured object to move along a vertical the second to-be-analyzed image, thereby securing a Zero optical path difference for each of a plurality of pixels in the second to-be-analyzed image and record ing the zero optical path difference for each of the plurality of pixels in the second to-be-analyzed image, thereby enabling the spectrum obtaining unit to obtain the spectrum data, thereby calculating a surface topography of the measured object according to at least one of the spectrum data and the second to-be-analyzed image:
	- closing the reference light aperture to enable the optical measurement device to enter the microscope mode, enabling the spectrum obtaining unit to obtain the spectrum data when the Zero optical path difference exists;
	- activating the measured object to move along the vertical direction, analyzing a focal information of each of the plurality of pixels in the second to-be-analyzed image to obtain a full focal colorful image and a full focal gray-level image, and establishing a depth response curve;

- activating the measured object to move laterally, to obtain a large-range Surface profile according to the spectrum data, the depth response curve and an axial dispersion extent; and
- deducing a thin-film thickness and an another Surface 5 profile according to the spectrum data when the Zero optical path difference face exists, when the measured object is a substrate having a coating layer thereon,
- wherein the surface profile is the another surface profile and the control-processing unit selects to only calculate and present one of the surface profile and the another surface profile. 10

2. The optically measurement device as claimed in claim 1, wherein:

the reference light processing unit further comprises: an optical path difference precision shift mechanism, used for adjusting the collimated effect reference light, so that the collimated effect reference light has a zero path difference with respect to the measured<br>light: and<br>20 light; and

- a reference light reflector precision shift mechanism, used for adjusting a contrast of a plurality of interfer
- the polarized light splitting unit further comprises a splitter angle adjustment rotation platform, used for adjusting 25 an image definition of the plurality of interference stripes in the interference image; and
- the optical measurement device further comprises a mea sured object supporting mechanism, comprising:
	- a piezoelectric activator, being controlled by the signal 30 processing unit to move the measured object along the vertical direction on the interference mode; and an precision shift platform, used for Supporting the piezoelectric activator.

3. The optically measurement device as claimed in claim 1, 35 wherein the signal processing unit activates the measured object to move along the vertical direction on the microscope mode, analyzing a high frequency information of each of the plurality of pixels in the second measured image, matching a depth of field gray value of each of the plurality of pixels, 40 restoring an image out-focal information to form the full focal colorful image and the full focal gray-level image, and estab lishing the depth response curve.<br>4. The optically measurement device as claimed in claim 3,

4. The optically measurement device as claimed in claim 3, wherein the signal processing unit restores the image outfocal information to deduce the full focal gray-level image by using an image contrast filtering method and analyzed high frequency information of each of the plurality of pixels in the second measured image.

wherein the spectrum obtaining unit acquires a spectrum message of an upper surface of the substrate and an upper face of the coating layer, respectively, and reversely deduces a distance between the upper surface of the substrate and the upper face of the coating layer of the measured object and 55 serving the distance as a thickness of the coating layer. 5. The optically measurement device as claimed in claim 1, 50

6. The optically measurement device as claimed in claim 1, wherein the external light source is one of a white-light halo gen lamp and an infrared lamp and has a Gaussian distributed 60

intensity.<br>
7. The optically measurement device as claimed in claim 1, wherein the image acquiring unit is capable of detecting one of a visible light and a non-visible light.<br>8. The optically measurement device as claimed in claim 1,

wherein the signal processing unit applies a phase shift algorithm onto the plurality of interference stripes and analyzes a maximum strength of the plurality of interference stripes, so 65

as to establish a surface profile information to acquire a surface profile of the measured object.

9. A method for optically measuring a plurality of param eters of an object, comprising steps of:

- (a) providing a collimated reference light and a collimated subject light;
- (b) polarizing the collimated reference light and the colli mated Subject light, to obtain a polarized reference light and a polarized subject light, the polarized reference light having a propagating path;
- (c) controlling a light flux of the polarized reference light, having an open and close states, and closing the propa gating path of the polarized reference light when the close state is acted;
- (d) controlling a light flux of the polarized subject light;
- (e) diving the polarized light into the reference light and the polarized subject light and coupling the reference light and the polarized subject light onto a first path and a second path, respectively;
- (f) receiving and focusing the polarized subject light to the measured object, the measured object reflecting the polarized subject light passing the light-splitting unit to generate a measured light, the measured light being
- $(g)$  reflecting the polarized reference light to generate a collimated effect reference light onto the third path when the reference light aperture is at the open state and the optical measurement device is on an interferometer mode and the measured light and the collimated effect reference light jointly generate an interference image, and generating a guided measured image on the third path when the reference light aperture is at the close state and the optical measurement device is on a microscope mode;
- (h) guiding the interference image on the interferometer mode and guiding the measured image on the micro scope mode to obtain a first to-be-analyzed image and a second to-be-analyzed image;
- (i) receiving the first to-be-analyzed image to generate a spectrum data, and receiving the second to-be-analyzed image;
- (i) controlling the measured object to move along a vertical direction on the interferometer mode, and analyzing the second to-be-analyzed image, thereby securing a Zero optical path difference for each of a plurality of pixels in the second to-be-analyzed image and recording the zero optical path difference for each of the plurality of pixels in the second to-be-analyzed image, thereby enabling the spectrum obtaining unit to obtain the spectrum data, thereby calculating a surface topography of the mea sured object according to at least one of the spectrum data and the second to-be-analyzed image;
- (k) closing the reference light aperture to enable the optical enabling the spectrum obtaining unit to obtain the spectrum data when the Zero optical path difference exists:
- (l) activating the measured object to move along the verti cal direction, analyzing a focal information of each of the plurality of pixels in the second to-be-analyzed image to obtain a full focal colorful image and a full focal gray-level image, and establishing a depth response curve;
- (m) activating the measured object to move laterally, to obtain a large-range surface profile according to the spectrum data, the depth response curve and an axial dispersion extent; and

(n) deducing a thin-film thickness and an another surface  $12$ . The method as claimed in claim 11, wherein the step profile according to the spectrum data when the zero (11) further comprises a step of:<br>optical path diffe wherein the surface profile is the another surface profile  $5$ and the control-processing unit selects to only calculate and present one of the surface profile and the another surface profile.

10. The optically measurement device as claimed in claim 9, wherein: extent the step (c) further comprises a step of:  $10$ 

- (c1) adjusting the collimated effect reference light, so that difference with respect to the measured light; the step (e) further comprises steps of:
- - (e1) adjusting a contrast of a plurality of interference 15 stripes in the interference image; and
	- (e2) adjusting an image definition of the plurality of inter ference stripes in the interference image; and

the method further comprises a step prior to the step (a) of:

(a1) supporting the piezoelectric activator and controlling  $20$ the measured object to move along the vertical direction on the interference mode.

11. The method as claimed in claim 9, wherein the step (1) further comprises a step of:

(11) analyzing a high frequency information of each of the  $_{25}$ plurality of pixels in the second measured image, match ing a depth of field gray value of each of the plurality of pixels, restoring an image out-focal information to form the full focal colorful image and the full focal gray-level image, and establishing the depth response curve.  $* * * * *$ 

optical path difference face exists, when the measured (12) restoring the image out-focal information to deduce the full focal gray-level image by using an image con-<br>the full focal gray-level image by using an image contrast filtering method and analyzed high frequency infor mation of each of the plurality of pixels in the second measured image.

13. The method as claimed in claim  $9$ , wherein the step  $(n)$ further comprises a step of:

(n1) acquiring a spectrum message of an upper surface of respectively, and reversely deduces a distance between the upper surface of the substrate and the upper face of the coating layer of the measured object and serving the distance as a thickness of the coating layer.

14. The method as claimed in claim 9, wherein the colli mated reference light is one of a white-light halogen lamp and

an infrared lamp and has a Gaussian distributed intensity.<br>15. The method as claimed in claim 9, wherein the image acquiring unit is capable of detecting one of a visible light and a non-visible light.

16. The method as claimed in claim 9, wherein the step (k) further comprises a step of:

(k1) applying a phase shift algorithm onto the plurality of interference stripes and analyzes a maximum strength of the plurality of interference stripes, so as to establish a surface profile information to acquire a surface profile of the measured object.